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**EXPANDED FORTRAN IV PROGRAM
FOR ELASTIC SCATTERING ANALYSES**

by Margaret M. Smith and Charles C. Giamati

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16. Abstract SCATLE is a FORTRAN IV nuclear optical model program which is a revision and extension of program SCAT4 (published by a UCLA group in 1962). This report describes program SCATLE and serves as a user's guide. SCATLE calculates elastic scattering cross sections, polarizations, phase shifts, and triple scattering values. An automatic search varies the nuclear parameters to improve agreement between calculated and experimental cross sections and polarizations. Several nuclear potential forms are available.			
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EXPANDED FORTRAN IV PROGRAM FOR ELASTIC SCATTERING ANALYSES

by Margaret M. Smith and Charles C. Giamati

Lewis Research Center

SUMMARY

SCATLE is a FORTRAN IV program which uses the nuclear optical model to calculate elastic scattering cross sections and polarizations. The version presented herein was written for an IBM 7094 II/7044 direct couple system at Lewis. This report describes program SCATLE and serves as a user's guide. SCATLE contains several options for calculating the central nuclear potential. Some options allow the real central, imaginary central, and spin-orbit potentials to have independent parameters. The parameters of the nuclear potential can be varied by a search option to improve the agreement between calculated and experimental values of cross sections and polarizations. Any one of the several chi-square functions calculated by SCATLE can be minimized by the search option. Plots of cross sections and polarizations as a function of scattering angle are furnished as part of the program output. Calculations of nuclear phase shifts and triple scattering values are available. The input description includes a listing of seven example input cases. Selected output from these examples is presented.

INTRODUCTION

Program SCATLE is the result of extensive revisions and additions made to the program SCAT4 (ref. 1).

Both SCAT4 and SCATLE solve the Schrodinger wave equation, using a given scattering energy and nuclear interaction potential. The solutions to the wave equation are used to calculate scattering cross sections and polarizations as a function of scattering angle. These calculated values are compared to experimentally measured values. A chi-square function is evaluated to furnish a numerical basis for the comparison. The calculated values depend on the chosen form of the nuclear interaction potential, which is a function of several parameters. SCATLE contains an automatic search option which minimizes chi-square by varying these parameters. SCATLE also provides an increased number of options for choosing the nuclear interaction potential.

In SCAT4, a nuclear potential is defined by specifying real and imaginary strength parameters (which represent the depths of the attractive potential wells) and real shape parameters (which define the nuclear size and surface diffuseness). When a Woods-Saxon form is used for the central potential, both the real and imaginary terms of the central nuclear potential are functions of the same two shape parameters. When a Gaussian form is chosen for the imaginary potential well, it is a function of two additional shape parameters. The nuclear potential can also have a spin-orbit term which is multiplied by real and imaginary strength parameters representing the depths of the spin-orbit potential wells. The shape parameters for the spin-orbit term are those used for the real central potential. These parameters can be incremented in uniform steps to provide a grid of points in the parameter space. Program SCAT4 then calculates scattering cross sections, polarizations, and chi-squares at each grid point.

The program SCATLE is basically an extension of SCAT4. All the SCAT4 calculations are included in SCATLE, although some of them have been revised. Several new calculations have been added, and some of the old calculations have been used in new ways. For example, one section of SCATLE is a merger of the basic SCAT4 calculations with a search program (ref. 2) from Argonne National Laboratory. SCATLE is arranged so that the parameter values at each grid point are input to the search program. The parameters are changed to give better agreement (in a least-squares sense) between calculated and experimental values for cross section and polarization. This process continues until a local minimum of the chi-square function is reached.

New options are also available for calculating the central-nuclear-potential form factors. The real central potential is always of the Woods-Saxon form, but can have different parameters than the imaginary potential (the decoupled case). The imaginary term may be a derivative of Woods-Saxon form, a Gaussian plus Woods-Saxon form, or a derivative of Woods-Saxon plus Woods-Saxon form.

SCATLE also has options to calculate phase shifts and triple scattering parameters. Additional output is available in printed and plotted forms.

The primary purpose of this report is to document SCATLE. The sections of this report which describes data preparation and available options will serve as a user's guide. The SCATLE calculations, input, and output are explained in detail. Some calculations are essentially unchanged from the original SCAT4 calculations. In these cases, the appropriate references will be made to the UCLA report (ref. 1).

MATHEMATICAL DESCRIPTION

The program SCATLE contains several calculations and options which are not available in SCAT4. These are described in detail in the following sections. SCATLE

also contains calculations which are essentially the same as the corresponding ones in SCAT4. Because those calculations are presented in reference 1, they are not discussed in this report.

Nuclear Potential Options

The Schrodinger equation solved by SCATLE can be written as

$$\left[\frac{-\hbar^2}{2\mu} \nabla^2 + V_1(r) + V_2(r) \bar{\mathbf{S}} \cdot \bar{\mathbf{L}} \right] \psi = E\psi \quad (1)$$

using the symbols of reference 1. (All symbols are defined in appendix A.) The interactions represented in equation (1) by $V_1(r)$ and $V_2(r)$ can be rewritten as

$$V_1(r) + V_2(r) \bar{\mathbf{S}} \cdot \bar{\mathbf{L}} = V_{\text{CN}} + V_{\text{coul}} + V_{\text{SO}} + V_{\text{coul,SO}} \quad (2)$$

where V_{CN} is the nuclear central potential, V_{coul} is the coulomb potential, V_{SO} is the nuclear spin-orbit potential, and $V_{\text{coul,SO}}$ is the coulomb spin-orbit potential.

Although equation (1) is expressed in terms of the variable r , it is convenient to represent the potentials in terms of the dimensionless variable ρ where

$$\rho = kr \quad (3)$$

The wave number k is given by

$$k = \sqrt{\frac{2\mu E}{\hbar^2}} = 0.218739 \sqrt{\mu E} \text{ fm}^{-1} \quad (4)$$

The constant factor in equation (4) is slightly different from the constant factor in equation (8) of reference 1. A similar difference occurs in the definition of the coulomb parameter η , where

$$\eta = \frac{\mu(ZZ')e^2}{\hbar^2 k} = 0.157481 ZZ' \sqrt{\frac{m_i}{E_{\text{LAB}}}} \quad (5)$$

corresponds to equation (43) of reference 1. The constants used in equations (4) and (5)

were computed using values of the fundamental constants \hbar and e from reference 3. The reduced mass μ is given by

$$\mu = \frac{m_i \cdot m_b}{m_i + m_b} \quad (6)$$

Options for computing spin-orbit potential. - The standard form for the spin-orbit term in equation (2) uses the strength parameters VS and WS, and the shape parameters AS and RS. The spin-orbit scattering potential V_{SO} is then given by

$$V_{SO} = \frac{2}{M_\pi^2 c^2} \left\{ \frac{k^2}{\rho} \frac{d}{d\rho} \left[\frac{-VS - i \cdot WS}{1 + \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)} \right] \right\} \bar{S} \cdot \bar{L} \quad \text{KL}(1) \neq 2 \quad (7)$$

where

$$\rho_S = k \cdot RS \cdot (m_b)^{1/3} \quad (8)$$

In equation (8), m_b represents the mass number of the target nucleus. When the square-well form is chosen for the real central potential, VS and WS must be set to zero (KL(1) = 2).

There are also several special options available for computing V_{SO} . These are described on pages 20 through 24 of reference 1 as form A and form B. They are obtained by setting KL(9) \neq 0 or KL(10) \neq 0. SCATLE provides an option for introducing a space-exchange form for the real spin-orbit potential. In that option, VS is the strength of the real spin-orbit term when the angular momentum number l is an even number, and VSODD is the strength when l is odd (KX(6) = 1).

Options for computing central nuclear potential. - SCATLE contains several options for computing the central nuclear potential which is represented as V_{CN} in equation (2); V_{CN} can be expressed as a function of ρ by

$$V_{CN}(\rho) = V_{CN,R} + i \cdot V_{CN,I} \quad (9)$$

where $V_{CN,R}$ is the real part of V_{CN} and $V_{CN,I}$ is the imaginary part.

There are two primary options for computing the real central potential $V_{CN,R}$ in

SCATLE. Both options use a Woods-Saxon form with strength parameter VO. The first option uses the shape parameters AS and RS, which are identical to those in the spin-orbit term (coupled spin-orbit case). Then $V_{\text{CN},\mathcal{R}}$ is given by

$$V_{\text{CN},\mathcal{R}} = -VO \frac{1}{1 + \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)} \quad \text{KX}(7) = 1 \quad (10)$$

This option is also available in SCAT4. The second option uses the shape parameters AO and RO. These are independent of the shape parameters in the spin-orbit term (decoupled spin-orbit case). Then $V_{\text{CN},\mathcal{R}}$ is given by

$$V_{\text{CN},\mathcal{R}} = -VO \frac{1}{1 + \exp\left(\frac{\rho - \rho_O}{k \cdot a_O}\right)} \quad \text{KX}(7) = 2 \quad (11)$$

where

$$\rho_O = k \cdot RO \cdot (m_b)^{1/3} \quad (12)$$

SCATLE contains five primary options for computing the imaginary part of the central potential $V_{\text{CN},\mathcal{I}}$:

(1) Standard Woods-Saxon

$$V_{\text{CN},\mathcal{I}} = -WI \frac{1}{1 + \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)} \quad \text{KL}(1) = 0 \quad (13)$$

(2) Gaussian absorption

$$V_{\text{CN},\mathcal{I}} = -WI \cdot \exp\left[-\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)^2\right] \quad \begin{array}{l} \text{KL}(1) = 1, \\ \text{KX}(1) = 0 \end{array} \quad (14)$$

where

$$\rho_I = k \cdot RI \cdot (m_b)^{1/3} \quad (15)$$

(Options (1) and (2) are also available in SCAT4.)

(3) Derivative of Woods-Saxon

$$V_{CN,\mathcal{D}} = -WI \frac{4 \cdot \exp\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)}{\left[1 + \exp\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)\right]^2} \quad \begin{array}{l} KL(1) = 1, \\ KX(1) = 1 \end{array} \quad (16)$$

(4) Gaussian plus Woods-Saxon

$$V_{CN,\mathcal{D}} = -WI \cdot \exp\left[-\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)^2\right] - WVI \frac{1}{1 + \exp\left(\frac{\rho - \rho_I}{0.69 k \cdot a_I}\right)} \quad \begin{array}{l} KL(1) = 1, \\ KX(1) = 2 \end{array} \quad (17)$$

(5) Derivative of Woods-Saxon plus Woods-Saxon

$$V_{CN,\mathcal{D}} = -WI \frac{4 \cdot \exp\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)}{\left[1 + \exp\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)\right]^2} - WVI \frac{1}{1 + \exp\left(\frac{\rho - \rho_I}{k \cdot a_I}\right)} \quad \begin{array}{l} KL(1) = 1, \\ KX(1) = 3 \end{array} \quad (18)$$

There are 10 ways to combine the two primary options for $V_{CN,\mathcal{R}}$ and the five primary options for $V_{CN,\mathcal{D}}$ to calculate $V_{CN}(\rho)$ by equation (9). Table I shows how these combinations are formed and lists the parameters used for $V_{CN,\mathcal{R}}$, $V_{CN,\mathcal{D}}$, and V_{SO} .

TABLE I. - SHAPE PARAMETERS FOR REAL CENTRAL
NUCLEAR, IMAGINARY CENTRAL NUCLEAR, AND
SPIN-ORBIT POTENTIALS

Real central nuclear potential, $V_{\text{CN},\mathcal{R}}$	Imaginary central nuclear potential, $V_{\text{CN},\mathcal{I}}$	Spin-orbit potential, V_{SO}
Shape parameters		
AS, RS (eq. (10))	AS, RS (eq. (13))	AS, RS
AS, RS (eq. (10))	AI, RI (eqs. (14), (16), (17), (18))	AS, RS
AO, RO (eq. (11))	AS, RS (eq. (13))	AS, RS
AO, RO (eq. (11))	AI, RI (eqs. (14), (16), (17), (18))	AS, RS

The square well form of V_{CN} is given by

$$V_{\text{CN},\mathcal{R}} = V_{\text{CN},\mathcal{I}} = 1 \quad \text{for } \rho \leq \rho_{\text{S}} \quad (19a)$$

and

$$\text{KL}(1) = 2$$

$$V_{\text{CN},\mathcal{R}} = V_{\text{CN},\mathcal{I}} = 0 \quad \text{for } \rho > \rho_{\text{S}} \quad (19b)$$

There are several options available which vary the shape of the Woods-Saxon form of V_{CN} by including a dip or bump at the origin, or by varying the shape of the knee or tail of the potential curve. These options are described on pages 18 through 20 of reference 1 as form A and form B. They are obtained by setting $\text{KL}(7) \neq 0$ or $\text{KL}(8) \neq 0$.

Grid and Search Procedures

The nuclear potential calculations depend on the following 12 parameters: VS, WS, AS, RS, VO, AO, RO, WI, WVI, AI, RI, and VSODD. Determining good values for these parameters requires three steps. The first step is to make initial guesses for the parameters. The next step is to vary the parameters in some systematic manner. The final step is to compare the results of calculations which are based on different sets of parameter values.

In SCATLE, the initial guesses are the input values of the parameters. The calculations are compared on the basis of a chi-square function associated with each set of parameter values. This chi-square function measures the deviation (in a least-squares sense) of the calculated values from the experimental values for cross section and po-

larization. There are several variations for calculating the chi-square function. These are described in a later section.

SCATLE provides three options for the systematic variation of the parameters. The grid option ($KT(1) = 2$) calculates results at several predetermined sets of parameter values. The search option ($KT(1) = 4$) begins from a single set of parameter values and automatically varies these parameters to give successively smaller values of chi-square. Each parameter set in the grid option can also be used as the starting point for a search ($KT(1) = 3$).

Each set of parameter values can be considered as defining a point in an n -dimensional parameter space. The points used in the grid option are defined as grid points. The initial grid point consists of the input values of the 12 parameters listed previously. Each parameter selected for the grid variation is then incremented for a specified number of uniform steps. The remaining grid points are then formed by taking all possible combinations of the generated parameter values. Cross sections and polarizations are calculated at each grid point. Chi-square functions are then calculated and written out at each grid point, along with the parameter values. The variable names of the grid increments and of the number of grid steps corresponding to each parameter are found in table IV. (Tables II through V are grouped at the end of the section Input requirements.)

SCATLE contains an automatic search option which utilizes the subroutines described in reference 2. For any given search, the parameters to be varied are defined as search parameters. These n search parameters can be any selected subset of the 12 parameters listed previously. Each search begins from the point in the n -dimensional parameter space which is defined by the input values of the search parameters. A specified chi-square function is then calculated at this point. The partial derivatives of the chi-square function with respect to each of the search parameters are also calculated, and they define the gradient of the function at this point. Increments for the search parameters are then calculated by using the gradient and a matrix (H-matrix) which is used as a metric in the parameter space. The search parameters are varied simultaneously and in such a way that the next iteration produces a smaller chi-square value. These calculations are repeated until a local minimum of the chi-square function is determined.

The number of iterations required to locate a minimum depends on how accurately the H-matrix at each point describes the gradient at that point. A search converges faster with a good approximation for the initial H-matrix than with a poor approximation. There are three ways to set up the initial H-matrix in SCATLE. These options are described in table III. A standard diagonal matrix can be constructed by using the elements found in column 5 of table IV. Experience has shown that these values are appropriate.

The normal search output for each iteration includes the current values of the search parameters, the partial derivatives of chi-square with respect to each of the

search parameters, and the value of the chi-square function to be minimized. At the end of a search, the final H-matrix is written out and the final values of the search parameters are used to generate the output for a SCATLE single case.

When the grid and search options are combined, each grid point becomes the starting point for a search. The initial H-matrix for the first grid point is specified according to the options described in table III. The initial H-matrix for any subsequent grid point is set equal to the final H-matrix from the previous grid point. This procedure generally leads to a more rapid convergence than occurs when a standard or arbitrary initial H-matrix is used.

Additional Calculations

The program SCATLE computes and outputs several quantities which were not computed in SCAT4. This section presents a brief description of the mathematical expressions for these calculations.

Double and triple scattering calculations. - The quantities $\delta_{l,R}^+$, $\delta_{l,S}^+$, $\delta_{l,R}^-$, $\delta_{l,S}^-$, η_l^+ , and η_l^- are computed and written out in subroutine OUTPT4. These quantities are also plotted in the subroutine PTETDL. The absorption coefficients η_l^+ and η_l^- are expressed in terms of the imaginary parts of the complex phase shifts δ_l^+ and δ_l^- by

$$\eta_l^+ = \exp \left(-2\delta_{l,S}^+ \right) \quad (20a)$$

$$\eta_l^- = \exp \left(-2\delta_{l,S}^- \right) \quad (20b)$$

The phase shifts are related to the complex coefficients C_l^+ and C_l^- by the following equation (see eq. (57) of ref. 1):

$$C_{l,R}^\pm + iC_{l,S}^\pm = \frac{1}{2i} \left\{ \exp \left[2i \left(\delta_{l,R}^\pm + i\delta_{l,S}^\pm \right) \right] - 1 \right\} \quad (21)$$

C_l^+ and C_l^- are related to the scattering amplitudes $A(\theta)$ and $B(\theta)$. The spin-independent amplitude $A(\theta)$ is given by

$$A(\theta) = f_c(\theta) + \frac{1}{k} \sum_{l=0}^{\infty} \exp(2i\sigma_l) \left[(l+1) C_l^+ + l C_l^- \right] P_l(\cos \theta) \quad (22a)$$

The spin-dependent scattering amplitude is

$$B(\theta) = \frac{-i}{k} \sum_{l=0}^{\infty} \exp(2i\sigma_l) (C_l^+ - C_l^-) P_l^1(\cos \theta) \quad (22b)$$

Equation (22) appears as equation (60) in reference 1. The coulomb scattering amplitude $f_c(\theta)$ appearing in equation (22a) is given by (see eq. (47) of ref. 1)

$$f_c(\theta) = \frac{-\eta}{2k \sin^2\left(\frac{\theta}{2}\right)} \exp \left\{ -i\eta \ln \left[\sin^2\left(\frac{\theta}{2}\right) \right] + 2i\sigma_0 \right\} \quad (23)$$

The coulomb phase shift σ_l is defined by (see eq. (49) of ref. 1)

$$\sigma_l = \arg \Gamma(l + 1 - i\eta) \quad (24)$$

Calculations and output for the triple scattering parameters R , β , and $-R'$ are provided in subroutine TRIPS. The rotation angle β is defined in terms of the scattering amplitudes, cross section, and polarization by

$$\cos \beta = \frac{|A(\theta)|^2 - |B(\theta)|^2}{\sigma(\theta) [1 - P^2(\theta)]^{1/2}} \quad (25a)$$

$$\sin \beta = \frac{A(\theta)B^*(\theta) - A^*(\theta)B(\theta)}{\sigma(\theta) [1 - P^2(\theta)]^{1/2}} \quad (25b)$$

For an unpolarized incident beam, the cross section and polarization are given in terms of the scattering amplitudes $A(\theta)$ and $B(\theta)$ as follows:

$$\sigma(\theta) = |A(\theta)|^2 + |B(\theta)|^2 \quad (26)$$

$$\overline{P}(\theta) = \frac{A^*(\theta)B(\theta) + A(\theta)B^*(\theta)}{\sigma(\theta)} \quad (27)$$

The rotation parameter R is defined by

$$R = \left[1 - P^2(\theta) \right]^{1/2} \cos(\beta - \theta_{\text{LAB}}) \quad (28)$$

The parameter $-R'$, often denoted in the literature by the symbol A , is given as

$$-R' = \left[1 - P^2(\theta) \right]^{1/2} \sin(\beta - \theta_{\text{LAB}}) \quad (29)$$

The output from subroutine TRIPS includes a table of θ , $\tan \beta$, β , θ_{LAB} , R , and $-R'$ values along with a plot of R and $-R'$ as a function of θ .

The polarization $\bar{P}(\theta)$ is usually obtained from a double scattering experiment. When the incident beam is unpolarized, the polarization $\bar{P}(\theta)$ of the scattered beam is along the direction of the unit vector \bar{n}_1 of equation (30) and figure 1.

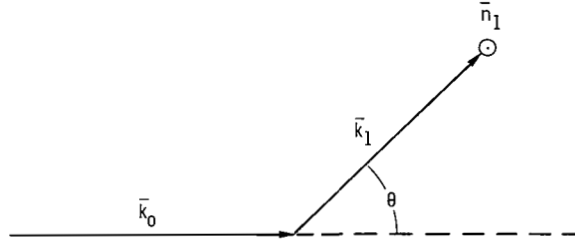


Figure 1. - Polarization direction in double scattering.

$$\bar{n}_1 = \frac{\bar{k}_0 \times \bar{k}_1}{|\bar{k}_0 \times \bar{k}_1|} \quad (30)$$

Consider a triple scattering experiment with a 100-percent-polarized beam of spin $1/2$ particles. Let the polarization vector be normal to the incident beam in the plane of scattering, as shown in figure 2.

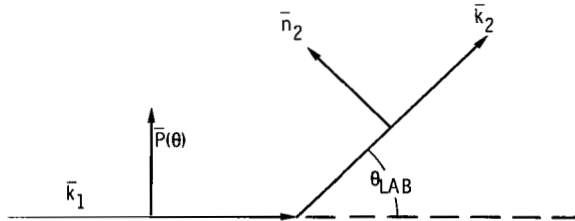


Figure 2. - Polarization directions in triple scattering.

The rotation of polarization R can be defined as

$$R = \frac{2}{\hbar} \langle \bar{S} \rangle \cdot \bar{n}_2 \quad (31)$$

where the direction of \bar{n}_2 is given by

$$\bar{n}_2 = \frac{(\bar{k}_1 \times \bar{k}_2) \times \bar{k}_2}{|(\bar{k}_1 \times \bar{k}_2) \times \bar{k}_2|} \quad (32)$$

The direction of n_2 defines the sign convention used to define R , β , and $-R'$.

Chi-square calculations. - The various chi-square functions computed in subroutine CHISQ are presented in this section. The function minimized by the search subroutines can be selected from any of the chi-square functions given by equations (33) and (34) or by equations (37) through (42). (See explanation of KX(3) in table III.) The search subroutines will also minimize the sum $\chi_\sigma^2 + \chi_P^2$ over any one of the restricted angular ranges. (See explanation of KX(12) in table III.)

The value of the chi-square deviation for the polarization is computed just as in SCAT4 (eq. (139) of ref. 1)

$$\chi_P^2 = \sum_{\theta} \chi_P^2(\theta) = \sum_{\theta} \left[\frac{P^{th}(\theta) - P^{ex}(\theta)}{\Delta P^{ex}(\theta)} \right]^2 \quad (33)$$

The total chi-square is (eq. (137) of ref. 1)

$$\chi_T^2 = \chi_\sigma^2 + \chi_P^2 \quad (34)$$

where χ_σ^2 is computed from the cross-section calculations and data.

The absolute normalization of the experimental cross-section data is usually uncertain. When fitting calculated cross sections, the experimental data can be normalized by a constant N , as described in reference 4. The equation for χ_σ^2 then becomes

$$\chi_\sigma^2 = \sum_{\theta} \chi_\sigma^2(\theta) = \sum_{\theta} \left[\frac{\sigma^{th}(\theta) - N \cdot \sigma^{ex}(\theta)}{N \cdot \Delta \sigma^{ex}(\theta)} \right]^2 \quad (35)$$

In SCATLE, there are three options for choosing the value of N. When KX(5) = 0, N is set equal to 1 so that χ_{σ}^2 is computed just as in SCAT4. In this case, $\sigma^{\text{ex}}(\theta)$ and $\Delta\sigma^{\text{ex}}(\theta)$ are not normalized in the χ_{σ}^2 calculation. When KX(5) = 1, N is set equal to the input variable XNORM. Finally, when KX(5) = 2, N is set equal to N_E which is given by

$$N_E = \frac{\sum_{\theta} \left[\frac{\sigma^{\text{th}}(\theta)}{\Delta\sigma^{\text{ex}}(\theta)} \right]^2}{\sum_{\theta} \frac{\sigma^{\text{th}}(\theta)\sigma^{\text{ex}}(\theta)}{[\Delta\sigma^{\text{ex}}(\theta)]^2}} \quad (36)$$

In this case, N is recomputed for each set of $\sigma^{\text{th}}(\theta)$ values and is such that the corresponding χ_{σ}^2 value is as small as possible. The value of N_E is always printed out along with values of the various chi-square functions.

The coulomb cross section $\sigma_{\text{coul}}^{\text{th}}(\theta)$ can be used in place of $\Delta\sigma^{\text{ex}}(\theta)$ as the weight factor in the χ_{σ}^2 calculation. This option requires KX(3) = 1. Then χ_{σ}^2 is given by

$$\chi_{\sigma}^2 = \sum_{\theta} \left[\frac{\sigma^{\text{th}}(\theta) - \sigma^{\text{ex}}(\theta)}{\sigma_{\text{coul}}^{\text{th}}(\theta)} \right]^2 \quad (37)$$

In addition, it is possible to compute a chi-square function over restricted angular ranges. This is useful when trying to fit a particular portion of an experimental curve. The ranges of angles are controlled by input controls KT(4) through KT(14) which correspond to the indices NF, NR, N1, IN1, N2, IN2, N3, IN3, N4, IN4 as used in equations (38) through (42).

The computations using NF and NR are

$$\chi_{\sigma, F}^2 = \sum_{j=1}^{NF} \chi_{\sigma}^2(\theta_j) \quad (38a)$$

$$\chi_{P, F}^2 = \sum_{j=1}^{NF} \chi_P^2(\theta_j) \quad (38b)$$

$$\chi_{\sigma, M}^2 = \sum_{j=NF+1}^{NR} \chi_{\sigma}^2(\theta_j) \quad (39a)$$

$$\chi_{P, M}^2 = \sum_{j=NF+1}^{NR} \chi_P^2(\theta_j) \quad (39b)$$

$$\chi_{\sigma, R}^2 = \sum_{j=NR+1}^{JMAX} \chi_{\sigma}^2(\theta_j) \quad (40a)$$

$$\chi_{P, R}^2 = \sum_{j=NR+1}^{JMAX} \chi_P^2(\theta_j) \quad (40b)$$

where J_{\max} is the index of the last angle of the set.

If we let K equal 1, 2, 3, and 4, the values of chi-square are computed for NK and INK as follows:

$$\chi_{\sigma, K}^2 = \sum_{j=NK}^{NK+INK} \chi_{\sigma}^2(\theta_j) \quad (41a)$$

$$\chi_{P, K}^2 = \sum_{j=NK}^{NK+INK} \chi_P^2(\theta_j) \quad (41b)$$

For K equal to 3 and 4, the following chi-squares can be computed:

$$\chi_{\sigma, 34}^2 = \chi_{\sigma, 3}^2 + \chi_{\sigma, 4}^2 \quad (42a)$$

$$\chi_{P, 34}^2 = \chi_{P, 3}^2 + \chi_{P, 4}^2 \quad (42b)$$

Adjusted chi-square values are also calculated to furnish additional output. These adjusted values are the chi-square functions just described divided by the factor $JMAX - NP$, where $JMAX$ is the number of experimental data points and NP is an input variable.

Effective potential calculations. - The effective potential for a given l -value is computed and plotted in subroutine PTFRFRI. The effective potential V_{EFF} is given by

$$V_{\text{EFF}} = -\frac{V_{\text{CN},R}}{E} + \frac{V_{\text{coul}}}{E} + \frac{l(l+1)}{\rho^2} \quad (43)$$

The value of l in equation (43) is equal to the input parameter KX(9). The effective potential V_{EFF} is plotted as a function of ρ for those values of ρ which lie in the range

$$(\rho_S - k \cdot l_{\text{lim}}) < \rho < (\rho_S + k \cdot l_{\text{lim}}) \quad (44)$$

This plot then presents the detailed behavior of the effective potential near the nuclear surface. The value of l_{lim} in equation (44) is set internally to be an integer in the interval $[0, 8]$, which produces a suitable plotting range.

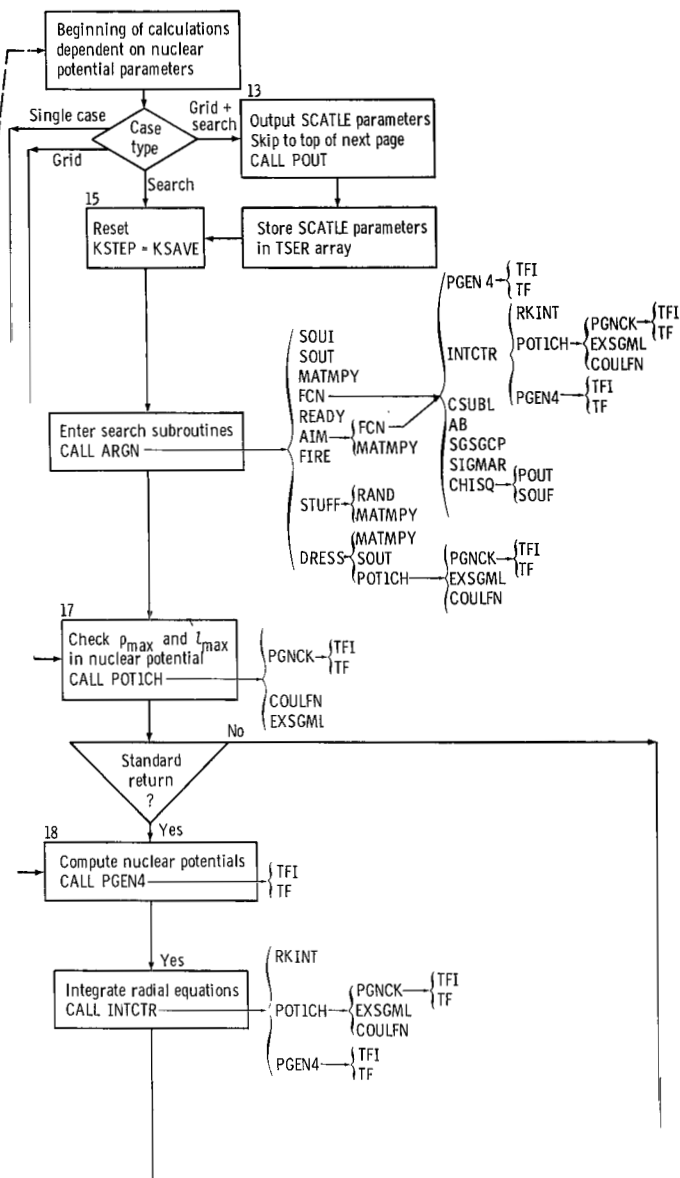
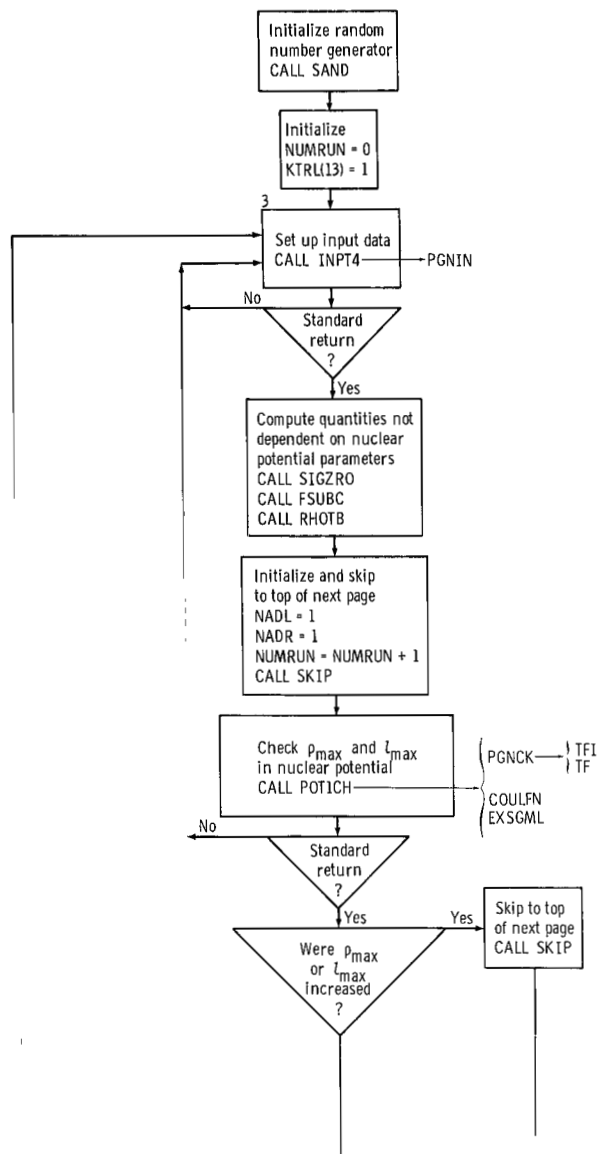
PROGRAM DESCRIPTION

General Program Organization

Each subroutine of the FORTRAN program SCATLE is assigned a subroutine number, and each card is assigned a card number. The card numbers are punched in columns 73 through 80 and appear in the FORTRAN listing at the end of this main section. The first two digits of each card number are the corresponding subroutine number. In this section of the report, the subroutine numbers are given in parentheses following each subroutine name.

Subroutines essentially unchanged from SCAT4. - The calculations in the following subroutines are essentially unchanged from SCAT4, although the common statements have been completely revised and the subroutines have been rewritten in the FORTRAN IV language:

SIGZRO (04)	EXSGML (09)
FSUBC (05)	CSUBL (16)
RHOTB (06)	SGSGCP (18)
SKIP (07)	SIGMAR (19)



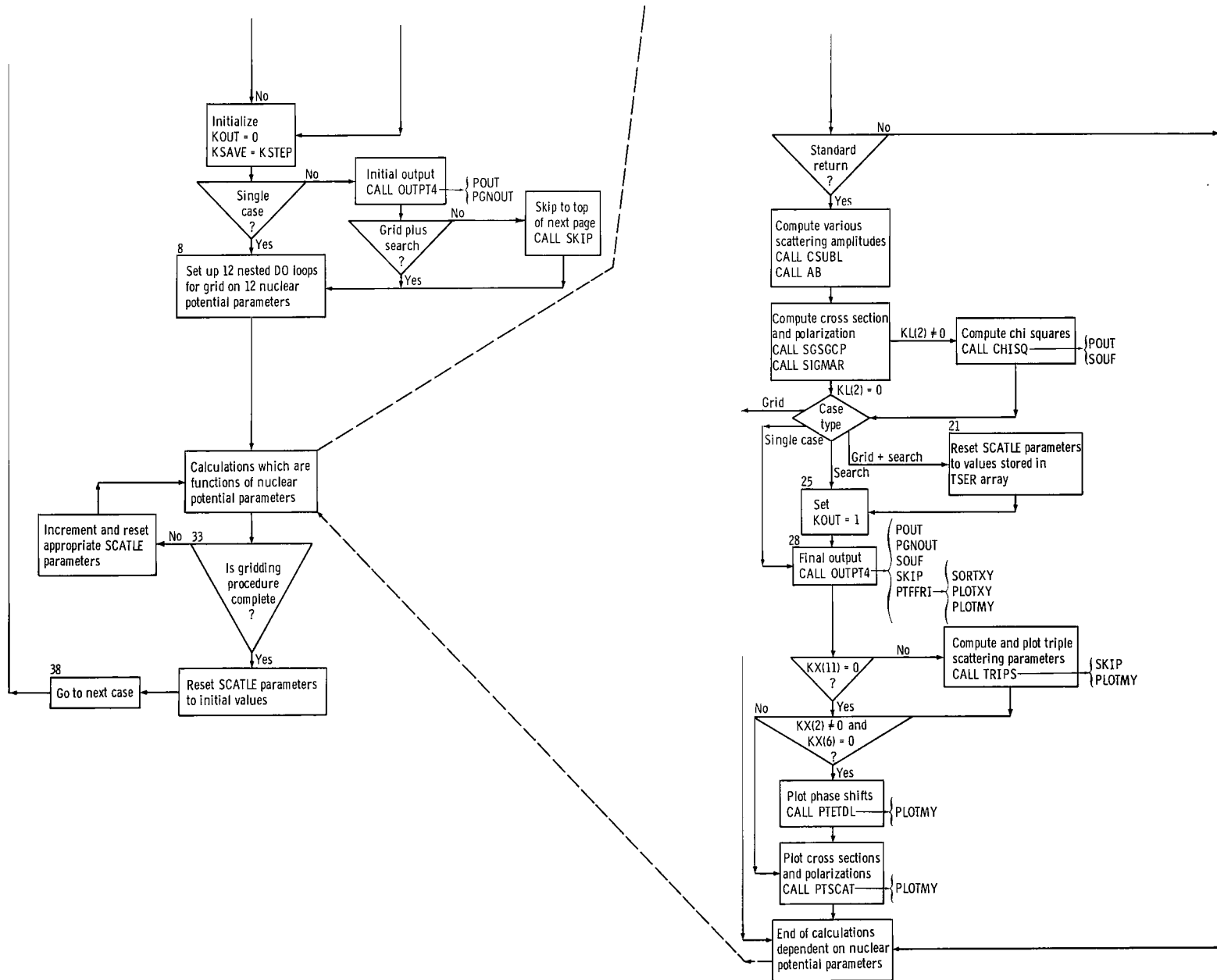


Figure 3. - Flow chart of main routine CTRL4 and overall program organization.

Subroutines modified from SCAT4. - The calculations in the following subroutines have been modified from SCAT4:

CTRL4 (01)	PGEN4 (12)
INPT4 (03)	INTCTR (14)
POT1CH (08)	RKINT (15)
COULFN (10)	AB (17)
OUTPT4 (11)	CHISQ (20)

CTRL4 (01): The main routine CTRL4 controls the flow of the program. Since the flow is different from that of SCAT4, a general flow chart is shown in figure 3.

INPT4 (03): Subroutine INPT4 controls the data input and performs several initial calculations. Standard values for the program controls and for other input variables are set automatically in INPT4. These standard values can be overwritten by means of input statements referring to NAMELIST statements. The SCATLE input is less complicated and requires fewer data cards than the corresponding SCAT4 input. A detailed description of the SCATLE input is contained in the next subsection.

POT1CH (08): The purpose of subroutine POT1CH is to make sure that l_{\max} and ρ_{\max} are sufficiently large. The value of l_{\max} must be large enough so that all the partial waves sensibly affected by the nuclear potential are included in the computation. The value of ρ_{\max} determined by this subroutine must be so large that the non-coulomb part of the potential is negligible at $\rho = \rho_{\max}$. The flow chart of POT1CH (fig. 4) outlines the details of the procedure for checking and increasing l_{\max} and ρ_{\max} . The quantities which are tested are expressed in terms of the variables TCR, TCI, TSR, and TSI, where TCR and TCI are defined by

$$\text{TCR} = - \frac{V_{\text{CN},\mathcal{R}}}{E} \quad (45a)$$

$$\text{TCI} = - \frac{V_{\text{CN},\mathcal{I}}}{E} \quad (45b)$$

Equation (6) can be rewritten as

$$V_{\text{SO}} = V_{\text{SO},\mathcal{R}} + i \cdot V_{\text{SO},\mathcal{I}} \quad (46)$$

where

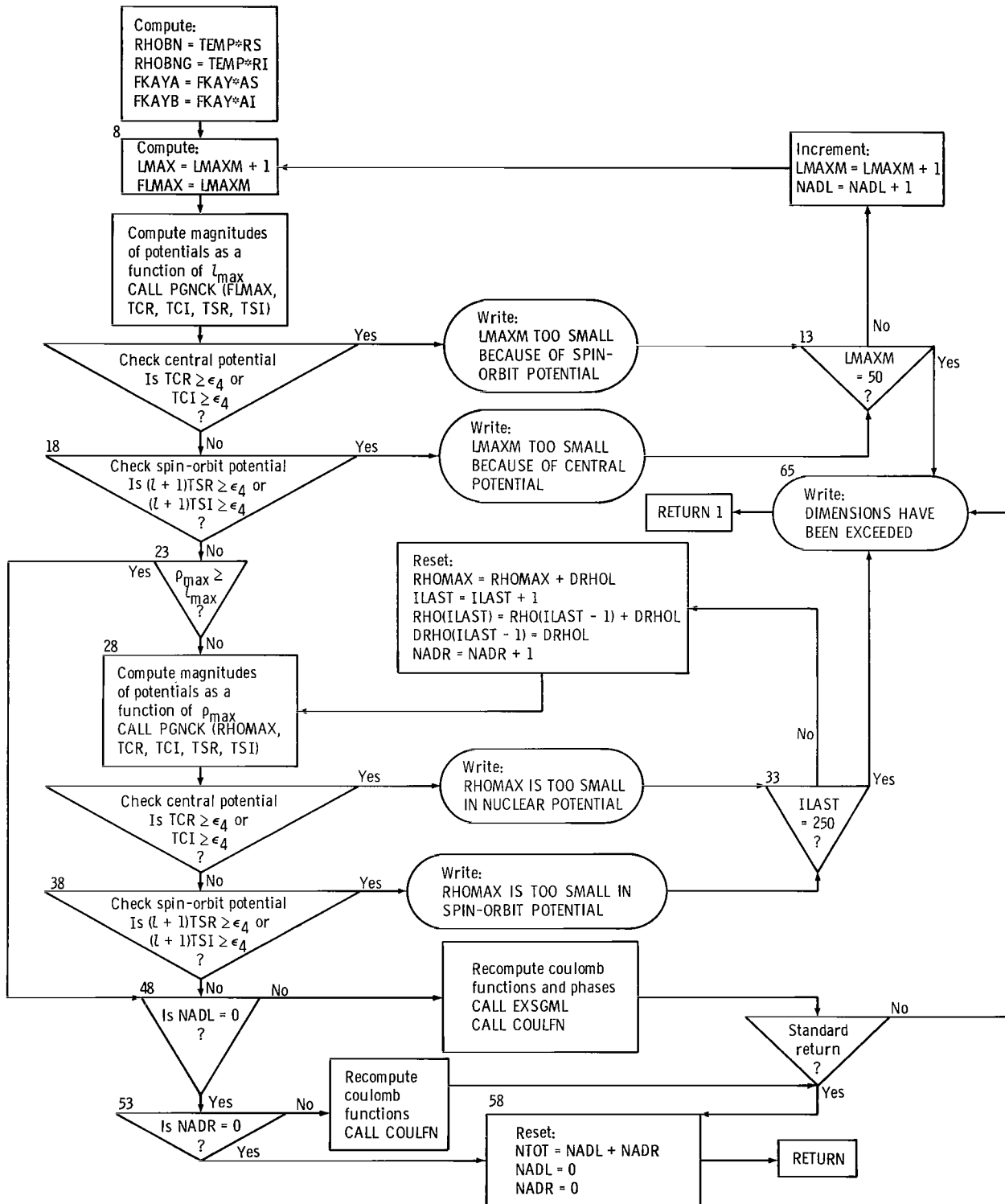


Figure 4. - Flow chart of subroutine POT1CH.

$$V_{SO,R} = -VS \frac{2 \cdot k \cdot S_l \cdot \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)}{\left[1 + \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)\right]^2} \quad (47a)$$

and

$$V_{SO,\mathcal{R}} = -WS \frac{2 \cdot k \cdot S_l \cdot \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)}{\left[1 + \exp\left(\frac{\rho - \rho_S}{k \cdot a_S}\right)\right]^2} \quad (47b)$$

and where S_l is given by

$$S_l = l \quad \text{when} \quad |\bar{S}| = \frac{\hbar}{2} \quad (48a)$$

$$S_l = -l - 1 \quad \text{when} \quad |\bar{S}| = -\frac{\hbar}{2} \quad (48b)$$

The variables TSR and TSI are defined by

$$TSR = -\frac{V_{SO,R}}{E \cdot S_l} \quad (49a)$$

$$TSI = -\frac{V_{SO,\mathcal{R}}}{E \cdot S_l} \quad (49b)$$

COULFN(10): Subroutine COULFN has been modified from the SCAT4 version by adding the calculations of the SCAT4 subroutine RMXINC. The table of ρ values is now extended directly in subroutine COULFN when necessary.

OUTPT4(11): Subroutine OUTPT4 includes the statements for SCATLE initial and final output. This subroutine also includes the calculations for $\delta_{l,R}^+$, $\delta_{l,\mathcal{R}}^+$, $\delta_{l,R}^-$, $\delta_{l,\mathcal{R}}^-$, η_l^+ , and η_l^- defined by equations (20) and (21). OUTPT4 has been expanded from the

SCAT4 version to include additional printouts and calculations. A detailed description of output options is presented in the section Typical output listings.

PGEN4 (12): The SCATLE version of subroutine PGEN4 is an extensive revision of the SCAT4 subroutine. The SCAT4 version of PGEN4 computes values for the nuclear potential at the beginning and middle of the integration mesh points. The SCATLE version of PGEN4 contains the following revisions:

(1) The potential V_{CN} can be computed using several new options as described in the section Options for computing central nuclear potential.

(2) PGEN4 is now called directly by POT1CH and furnishes values for the potential at $l = l_{\max}$ and $\rho = \rho_{\max}$.

(3) The two separate computations of the potential at the beginning and middle of an integration step interval have been combined in the coding.

(4) The computations for the knee and tail variations of the form factors as described in reference 1 are now found in the function TF.

(5) PGEN4 contains the following entry points:

(a) The normal entry point at the beginning of PGEN4 is used for calculating the nuclear potential at the beginning and middle of the integration mesh points.

(b) PGNCK is the entry point called by POT1CH.

(c) PGNIN is an entry point called from INPT4. It provides for the input of data used by function TF for the knee and tail variation calculations.

(d) PGNOUT is an entry point called from OUTPT4. It provides for the initial output of the knee and tail variation parameters.

A flow chart of subroutine PGEN4 is shown in figure 5.

INTCTR (14): This subroutine controls the Runge-Kutta integration procedure. When $KX(6) = 1$, the strength of the real spin-orbit term in the nuclear potential is VS if l is an even integer and VSODD if l is an odd integer.

RKINT (15): Subroutine RKINT carries out the numerical integration of the radial wave equation. The integration is carried out by operating with two coupled differential equations for the real and imaginary parts of the radial wave function. For convenience, this set of two equations is solved for the case $j = l + 1/2$ and $j = l - 1/2$ at the same time. When $VS = WS = 0$, these two cases are identical. In order to speed up the integration procedure, RKINT calculates only one of these cases when $VS = WS = 0$.

AB (17): Subroutine AB calculates the scattering coefficients $A(\theta)$ and $B(\theta)$. The Legendre polynomials $P_l(\cos \theta)$ and the associated Legendre polynomials $P_l^1(\cos \theta)$ are also calculated in this subroutine. To economize on computer storage space, the quantities $P_l(\cos \theta)$ and $P_l^1(\cos \theta)$ are recomputed each time $A(\theta)$ and $B(\theta)$ are computed.

CHISQ (20): Subroutine CHISQ computes the chi-square functions and the normalization constant given in equations (33) through (42). During a grid case, this subroutine provides for the output of the parameter and chi-square values.

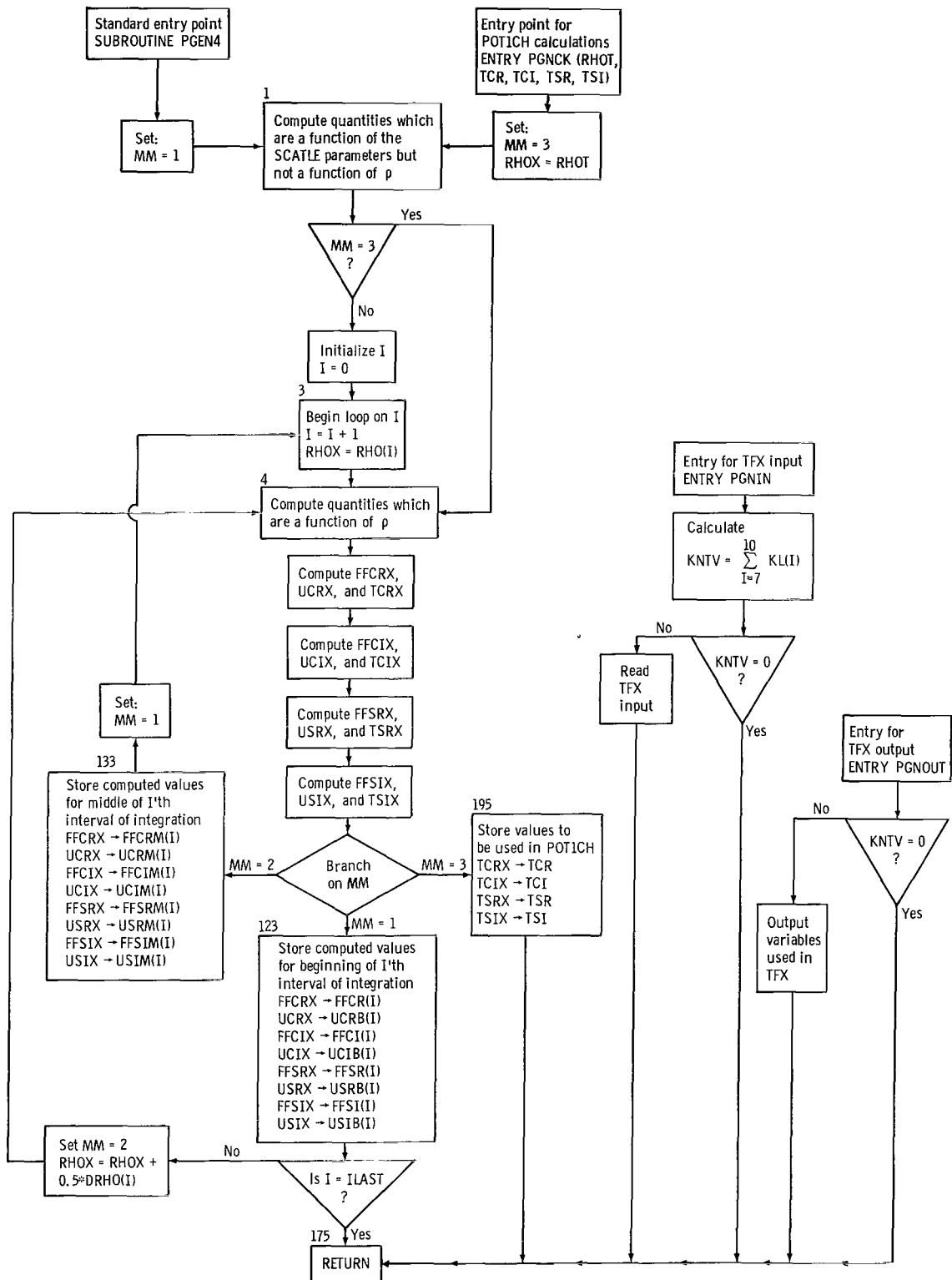


Figure 5. - Flow chart of subroutine PGEN4.

New subroutines. - The following subroutines were written for program SCATLE:

POUT(02)	PTETDL(23)
TFX(13)	PTSCAT(24)
PTFFRI(21)	SOU(26)
TRIPS(22)	SCTBD(34)

POUT(02): Subroutine POUT outputs values of the nuclear potential parameters, along with proper labels, during search and grid procedures.

TFX(13): Function TFX contains the calculations for the special variations of the potential form factors referred to as knee and tail variations in reference 1.

PTFFRI(21): Subroutine PTFFRI is called only when KL(12) = 1. It computes and plots the effective potential as a function of ρ near the nuclear surface. The potential as given by equations (43) and (44) is calculated for a single given l -value. The form factors for the real and imaginary parts of the central nuclear and spin-orbit potentials are also plotted as a function of ρ . These form factors are the coefficients of -VO, -WI, -WVI, -VS, and -WS in the equations for the nuclear potential. The spin-orbit form factors are multiplied by the factor $4 \cdot \rho_S$ before plotting, and all four form factors appear on a single plot.

TRIPS(22): Subroutine TRIPS is called when KX(11) \neq 0. When KX(11) equals 1 or 2, the triple scattering parameters R , β , and R' of equations (25), (28), and (29) are calculated. The values of θ , $\tan \beta$, β , θ_{LAB} , R , and $-R'$ are then written out in table form. Subroutine TRIPS also produces a plot of R and $-R'$ as a function of θ . When KX(11) = 2, a table of the quantities $f_c(\theta)$ and $[A(\theta) - f_c(\theta)]$ is generated in polar form. These quantities are given by equations (22a) and (23). A table of σ_l values as given by equation (24) is also written out.

PTETDL(23): Subroutine PTETDL is called when KX(2) \neq 0 and KL(6) \neq 1. This subroutine produces a plot of η_l^+ and η_l^- as a function of l (see eq. (20)). It also produces a plot of the quantities $\delta_{l,R}^\pm$, $\delta_{l,R}^\pm - \pi$, $\delta_{l,R}^\pm + \pi$, and $\delta_{l,R}^\pm + 2\pi$ as a function of l . The real phase shifts $\delta_{l,R}^\pm$ are defined in equation (21).

PTSCAT(24): This subroutine produces plots of polarization and/or cross-section data when KL(4) \neq 0. When KL(4) = 1, a plot of $P^{ex}(\theta)$ and $P^{th}(\theta)$ as a function of θ is produced. A plot of $\sigma^{ex}(\theta)$ and $\sigma^{th}(\theta)$ as a function of θ is produced when KL(4) = 2. A plot of $N \cdot \sigma^{ex}(\theta)$ and $\sigma^{th}(\theta)$ as a function of θ is also produced when the experimental cross sections are normalized in equation (35) (KX(5) \neq 0 and KL(4) = 2). When KL(4) = 3, the combined results of KL(4) = 1 and KL(4) = 2 are produced.

SOU(26): Subroutine SOU outputs and labels values of the search parameters and their partial derivatives during a search. The value of the reaction cross section and

the values of the normalization and chi-square functions given by equations (33) through (42) are also written out. Subroutine SOUI contains two nonstandard entry points which are labeled ENTRY SOUF and ENTRY SOUT.

SCTBD(34): Subroutine SCTBD is a BLOCK DATA subprogram. The convergence limits ϵ_1 , ϵ_2 , ϵ_3 , and ϵ_4 are entered into COMMON block CONV in SCTBD. The names of the SCATLE parameters are entered into COMMON block PARA.

Search subroutines. - The SCATLE search subroutines are unchanged from the corresponding subroutines of reference 2 in the sense that the searching procedure is the same. There are several new cutoff options which are controlled by the input variables NMLR, NPCT, and PCT (table III). The SCATLE search subroutines are changed from those of reference 2 in the sense that the input, output, and COMMON statements have been modified.

ARGN(25): The SCATLE subroutine ARGN corresponds to the main program of reference 2, and controls the search procedure. The SCATLE search variables are input in subroutine INPT4 by referring to NAMELIST SCHI. Table III contains a detailed description of the search input.

The following subroutines are described in reference 2:

READY(27)	DRESS(30)
AIM(28)	STUFF(31)
FIRE(29)	MATMPY(32)

FCN(33): Subroutine FCN is called by several search subroutines. It calculates the value of the chi-square function to be minimized and its gradient, given a set of values for the n search parameters. Let $f_{\chi^2}(x_1, x_2, \dots, x_n)$ be the chi-square function designated by the controls KX(4) and KX(12) (see table III). The n components of the gradient of f_{χ^2} are given by

$$G_j = \frac{\partial f_{\chi^2}}{\partial x_j} = \frac{f_{\chi^2}(x_1, \dots, x_j + \Delta x_j, \dots, x_n) - f_{\chi^2}(x_1, \dots, x_j, \dots, x_n)}{\Delta x_j} \quad (50)$$

for $j = 1$ to $j = n$, where x_1, x_2, \dots, x_n are the current values of the n search parameters. The values of Δx_j corresponding to each SCATLE parameter are found in column 6 of table IV. The value of $f_{\chi^2}(x_1, x_2, \dots, x_n)$ is the current value of the function to be minimized by the search subroutines, and the gradient of this function is defined by the n values of G_j .

Program Operating Instructions

Machine specifications. - Program SCATLE is written in FORTRAN IV programming language (version 13). It is currently being run at Lewis on an IBM 7094 II direct couple system with 32 768 core storage locations. The monitor system is a modified version of the IBM-distributed IBSYS Version 13. SCATLE utilizes several options which are not part of the IBM monitor system. Table V includes descriptions of these options and indicates where they are used in SCATLE.

Detailed description of required input. - The form of the data cards is specified by either FORMAT statements or NAMELIST statements. There are nine sets of data cards. Four sets are required for every case; the other five sets may be required depending on the options chosen. The nine input sets are listed in table II. The card number listed refers to the READ statement for that data set. The NAMELIST or FORMAT for each set is listed in the column labeled Description.

Table III lists and describes all SCATLE input variables which appear in NAMELIST statements. The standard input values also appear in table III. The glossary of FORTRAN variables (appendix B) may also be helpful in interpreting the SCATLE input variables.

Table IV lists the variable names of the grid increment and number of grid points corresponding to each SCATLE parameter. The values of the corresponding elements in the standard H-matrix are also tabulated. The values of Δx_j in column 6 are those used to calculate the partial derivatives of f_2 for the search subroutines (eq. (50)). These values are internal and cannot be read in.

The dimension specifications of the FORTRAN variables impose three limitations on the input values: JMAX must be less than or equal to 150; LMAXM must be less than or equal to 50; the RHOIN and DRHOIN arrays cannot take on values which cause the resulting RHO array to have more than 250 elements.

In general, the SCATLE user need input a NAMELIST variable only if he wants its value to differ from the value already stored in the computer. The flow diagram of figure 6 shows how a set of input values for any given case is defined.

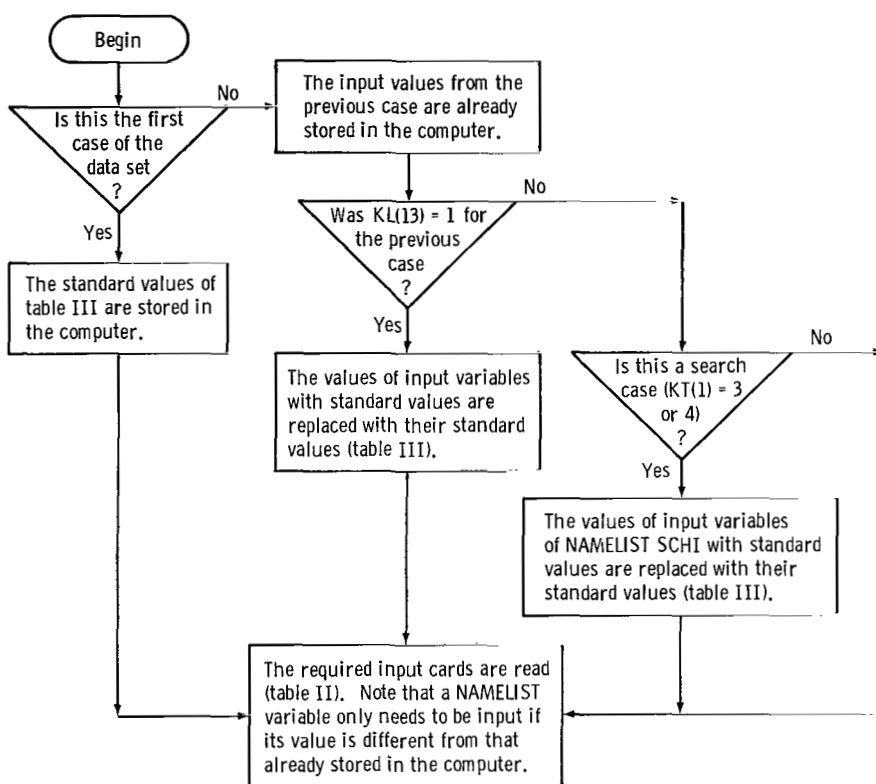


Figure 6. - Schematic flow diagram showing how a set of input values is defined.

The data cards for a single case with standard controls and with no experimental data are listed below. The potential is a Woods-Saxon real central potential, a Gaussian imaginary central potential, and a derivative of Woods-Saxon spin-orbit potential.

STANDARD POTENTIAL CASE WITHOUT EXPERIMENTAL DATA

\$KTR KL(2)=0 \$

\$PE1 FMI=1.00783,FMB=27.97693,ELAB=18.82,ZZ=14,RC=1.25,VO=60,AS=.6,RS=1.0,
WI=6,AI=.8,R1=1.2,VS=0, \$

\$RF1 \$

\$TSP DTH=5,THI=5,THF=175 \$

Card 1 is the title card. Card 2 contains the nonstandard value $KL(2) = 0$ so that chi-square values (meaningless here without experimental data) will not be computed. Card 3 and Card 4 contain the parameters describing the specific nucleus and interaction. The

first four variables are the incident and target nucleus masses, laboratory energy, and charge product. The coulomb charge radius parameter is denoted by RC; VO, AS, and RS are parameters for the real central potential; WI, AI, and RI are parameters for the imaginary central potential; and VS is the real spin-orbit potential strength. Card 5 must be read in, but since standard values are used for the integration data, the data field is left blank. Card 6 contains values needed to generate the set of center-of-mass angles at which cross sections and polarizations are calculated.

Input cards for typical data sets. - This section lists the input cards for six example cases which compute results for scattering of 18.82-MeV protons from ^{28}Si . Data set 1 consists of the input cards for examples 1 and 2. The input cards for examples 3 through 6 have been combined to form data set 2. These two data sets illustrate the input requirements described in the previous section.

Example 1 of data set 1 is a six-parameter search case with search parameters VO, WI, VS, AO, AI, and AS. The real central potential $V_{\text{CN},\text{R}}$ uses a Woods-Saxon form factor, the imaginary central potential $V_{\text{CN},\text{I}}$ uses a derivative of Woods-Saxon form factor, and the spin-orbit potential contains only a real part.

Example 2 of data set 1 is a combination grid and search case which uses the same options for V_{CN} and V_{SO} as example 1. The grid parameters are AO and AS; and each grid point is the starting point for a four-parameter search on VO, WI, VS, and AI.

DATA SET 1

EXAMPLE 1 SILICON 28 (P,P) E=18.82 SINGLE CASE SEARCH

\$KTR KL(4)=2, KX(1)=1, KX(7)=2, KT(1)=4, NP=10\$

\$PEI FMI=1.00783, FMB=27.97693, ELAB=18.82, ZZ=14., RC=1.25,
VU=60., WI=6., VS=6., AU=.8, AI=.8, AS=.5, RO=1.05, RI=1.2, RS=.95\$

\$RHI LMAXM=15, NMAX=4, RHOIN(3)=5., 15., DRHCIN(2)=.1, .2\$

\$SCHF N=6, SRCH='VU', 'WI', 'VS', 'AI', 'AS'\$

\$TSP CSIG=T, JMAX=44, JUPT=1\$

5.18	1.57 +5	1.57 +4	1.0	1.0 +30
7.77	2.35 +4	2.35 +3	1.0	1.0 +30
12.95	2623.76	262.37	1.0	1.0 +30
15.53	1350.16	135.02	-.077	.020
18.12	870.77	87.08	1.0	1.0 +30
20.71	649.43	64.94	1.0	1.0 +30
23.30	1.0	1.0 +30	-.187	.025
25.87	204.06	20.41	1.0	1.0 +30
31.03	90.89	9.09	-.266	.020
36.18	27.12	3.71	1.0	1.0 +30
38.80	1.0	1.0 +30	-.617	.028
41.33	5.47	0.55	1.0	1.0 +30
46.46	10.11	1.01	.400	.039

51.58	25.09	2.51	1.0	1.0 +30
54.10	1.0	1.0 +30	.161	.021
56.69	36.32	3.63	1.0	1.0 +30
61.79	37.42	3.74	-.118	.040
66.87	32.14	3.21	1.0	1.0 +30
69.40	1.0	1.0 +30	-.236	.022
71.94	23.06	2.31	1.0	1.0 +30
76.99	13.63	1.36	-.404	.049
82.03	7.55	0.76	1.0	1.0 +30
84.50	1.0	1.0 +30	-.451	.027
87.06	4.78	0.48	1.0	1.0 +30
92.06	4.54	0.45	-.143	.036
97.06	5.19	0.52	1.0	1.0 +30
99.50	1.0	1.0 +30	.580	.038
102.03	5.82	0.58	1.0	1.0 +30
106.99	6.07	0.61	.610	.034
111.94	5.24	0.52	1.0	1.0 +30
114.40	1.0	1.0 +30	.579	.028
116.87	4.30	0.43	1.0	1.0 +30
121.79	3.42	0.34	.340	.040
126.69	2.85	0.29	1.0	1.0 +30
129.10	1.0	1.0 +30	.080	.048
131.58	2.65	0.27	1.0	1.0 +30
136.46	2.69	0.27	-.034	.051
141.33	2.80	0.28	1.0	1.0 +30
143.80	1.0	1.0 +30	.098	.044
146.18	2.84	0.28	1.0	1.0 +30
151.03	2.91	0.29	.434	.039
155.87	2.65	0.27	.680	.050
160.71	2.53	0.25	1.0	1.0 +30
165.53	2.55	0.26	.740	.050

EXAMPLE 2 SILICON 28 (P,P) E=18.82

SEARCH WITH GRID ON AO AND AS

\$KTR NT(1)=3\$

\$PEI AU=.7\$

\$GR I NAU=2, DAU=.1, NAS=2, DAS=.05\$

\$RFI \$

\$SCH I N=4, SRCH='VU', 'WI', 'VS', 'AI'\$

Example 3, the first case of data set 2, is a single case which uses the same options for V_{CN} and V_{SO} as examples 1 and 2. The values of the SCATLE parameters are the values at the end of the search of example 1.

Example 4 is also a single case. This case is exactly the same as example 3 except that it uses the normalization N_E in the calculation of X_O^2 .

Example 5 is a grid case which uses the same computing options as example 3. The grid points of this example bracket the point in the parameter space used as input for example 3.

Example 6 is a single case where $V_{CN,R}$ uses a Woods-Saxon form factor, $V_{CN,L}$ uses a knee and tail variation form factor, and the spin-orbit potential contains only a real part. Input values for the SCATLE parameters which yield reasonable chi-square values were chosen.

Data set 1 ran on an IBM 7094 II direct couple system at Lewis with an execution time of 11.76 minutes. The execution time for data set 2 was 0.82 minute.

DATA SET 2

EXAMPLE 3 SILICON 28 (P,P) E=18.82 SINGLE CASE

\$KTR KL(4)=3, KL(6)=2, KL(12)=1, KX(1)=1, KX(7)=2, NP=10\$

\$PEI FMI=1.00783, FMB=27.97693, ELAB=18.82, ZZ=14., RC=1.25,
VO=59.78, WI=6.294, VS=0.217, AU=.7642, AI=.8455, AS=.5134, RO=1.05, RI=1.2,
KS=.95\$

\$KFI LMAXM=15, NMAX=4, KRUIN(3)=5., 15., DRUIN(2)=.1, .2\$

\$TSP CSIG=I, JMAX=44, JUPT=1\$

5.18	1.57 +5	1.57 +4	1.0	1.0 +30
7.77	2.35 +4	2.35 +3	1.0	1.0 +30
12.95	2623.76	262.37	1.0	1.0 +30
15.53	1350.16	135.02	-.077	.020
18.12	870.77	87.08	1.0	1.0 +30
20.71	649.43	64.94	1.0	1.0 +30
23.30	1.0	1.0 +30	-.187	.025
25.87	204.00	20.41	1.0	1.0 +30
28.43	90.89	9.09	-.266	.020
30.98	37.12	3.71	1.0	1.0 +30
33.53	1.0	1.0 +30	-.617	.028
36.08	5.47	0.55	1.0	1.0 +30
38.63	10.11	1.01	.400	.039
41.18	25.09	2.51	1.0	1.0 +30
43.73	1.0	1.0 +30	.161	.021
46.28	36.32	3.63	1.0	1.0 +30
48.83	37.42	3.74	-.118	.040
51.38	22.14	2.21	1.0	1.0 +30
53.93	1.0	1.0 +30	-.236	.022
56.48	23.00	2.31	1.0	1.0 +30
59.03	13.63	1.36	-.404	.049
61.58	7.55	0.76	1.0	1.0 +30
64.13	1.0	1.0 +30	-.451	.027

87.06	4.78	0.48	1.0	1.0 +30
92.06	4.54	0.45	.143	.036
97.06	5.19	0.52	1.0	1.0 +30
99.50	1.0	1.0 +30	.580	.038
102.03	5.82	0.58	1.0	1.0 +30
106.99	6.07	0.61	.610	.034
111.94	5.24	0.52	1.0	1.0 +30
114.40	1.0	1.0 +30	.579	.028
116.87	4.30	0.43	1.0	1.0 +30
121.79	3.42	0.34	.340	.040
126.69	2.85	0.29	1.0	1.0 +30
129.10	1.0	1.0 +30	.080	.048
131.58	2.69	0.27	1.0	1.0 +30
136.46	2.69	0.27	-.034	.051
141.33	2.80	0.28	1.0	1.0 +30
143.80	1.0	1.0 +30	.098	.044
146.18	2.84	0.28	1.0	1.0 +30
151.03	2.91	0.29	.434	.039
155.87	2.65	0.27	.680	.050
160.71	2.53	0.25	1.0	1.0 +30
165.53	2.55	0.26	.740	.050

EXAMPLE 4 SILICON 28 (P,P) E=18.82 SINGLE CASE, ENORM NORMALIZATION

\$KTR KX(5)=2\$

\$PEI \$

\$RHI \$

EXAMPLE 5 SILICON 28 (P,P) E=18.82 GRID ON VO, VS, AND WI

\$KTR KL(13)=1, KT(1)=2, KX(5)=0\$

\$PEI VO=50., VS=4., WI=4.\$

\$GRI NV0=2, DV0=10., Nwi=2, DWI=2., NVS=3, DVS=2.\$

\$RHI \$

EXAMPLE 6 SILICON 28 (P,P) E=18.82 SINGLE CASE, KNEE AND TAIL VCN1

\$KTR KL(1)=0, KL(4)=3, KL(6)=1, KL(8)=1, KX(7)=2, NP=11\$

\$PEI VO=51.9, WI=30.08, VS=10.37, AO=.75, AS=.85, RO=1.161, RS=.861\$

\$RHI LMAXM=15, NMAX=4, RHUIN(3)=5., 15., DRHCIN(2)=.1, .2\$

-1. 0. 1. 0. 1. 0. .7 0.

\$TSP \$

Tables describing input. - Tables II, III, and IV contain details of SCATLE input options. Table V lists the nonstandard FORTRAN IV programming options used in SCATLE.

TABLE II. - INPUT SETS

Input set	Required for -	Card number	Description
1	All cases	03--0950	Title card (FORMAT 13A6)
2	All cases	03--0970	Controls: NAMELIST/KTR/KL, KT, KX, XNORM, NP
3	All cases	03--1200	SCATLE parameters (energy, mass, and charge values): NAMELIST/PEI/FMI, FMB, ELAB, ZZ, RC, VO, AO, RO, WI, WVI, AI, RI, VS, WS, AS, RS, VSODD
4	KT(1) = 2 or KT(1) = 3	03--1330	Grid variables: NAMELIST/GRI/DRI, DRS, DVO, DWI, DAS, DVS, DWS, DAI, DWVI, DAO, DRO, DVSODD, NRI, NRS, NVO, NWI, NAS, NVS, NWS, NAI, NWVI, NAO, NRO, NVSODD
5	All cases	03--1350	Integration variables and LMAXM: NAMELIST/RHI/NMAX, LMAXM, RHOIN, DRHOIN
6	$\sum_{I=7}^{10} KL(I) \neq 0$	12--1630	Input for knee and tail variations (FORMAT 8E10.0): ^a TH(1), TH(2), TN1(1), TN1(2), TN2(1), TN2(2), PMA, PMB
7	KT(1) = 3 or KT(1) = 4	03--1520	Search variables: NAMELIST/SCHI/C, DELTA, E, FAC, H, KSTEP, N, NC, NHP, NSSW1, NMLR, NPCT, PCT, SRCH, VP
8	KL(3) \neq 0	03--1790	Experimental data: NAMELIST/TSP/CSIG, DPOLEX, DSGMEX, DTH, JMAX, JOPT, POLEX, SGMAEX, THETAD, THI, THF
9	JOPT \neq 0	03--1880 03--1890	Experimental data (FORMAT 8E10.0): ^a THETAD(J), SGMAEX(J), DSGMEX(J), POLEX(J), DPOLEX(J); one card for each J from 1 to JMAX

^aWhen data are input using E-conversion, the exponent is read as 0 whenever the characters Exx are omitted from the data card. Thus, data which are punched on cards according to the specifications for F-conversion will also be input correctly by E-conversion. (See listing of data cards for example data sets.)

TABLE III. - SCATLE INPUT VARIABLES APPEARING IN NAMELIST STATEMENTS

Namelist name	Variable name	Standard values	Description
KTR	KL(1)	1	<p>0 - $V_{CN,R}$, Woods-Saxon; $V_{CN,\ell}$, Woods-Saxon</p> <p>1 - $V_{CN,R}$, Woods-Saxon; $V_{CN,\ell}$, determined by $KX(1)$</p> <p>2 - Square well form of V_{CN} (eq. (19)): When $KL(1) = 2$, $KX(7)$ is set to 1. If $KL(1) = 2$, set $VS = WS = 0$.</p>
	KL(2)	1	<p>0 - Chi-square not computed.</p> <p>1 - Compute chi-square.</p>
	KL(3)	1	<p>0 - Use experimental values from previous case.</p> <p>1 - Read NAMELIST/TSP/. (KL(3) is set equal to 0 after Read.)</p>
	KL(4)	0	<p>0 - No plot.</p> <p>1 - Plot polarizations.</p> <p>2 - Plot sigmas.</p> <p>3 - Plot sigmas and polarizations.</p>
	KL(5)	0	Not used
	KL(6)	0	<p>0 - Normal output.</p> <p>1 - Minimum output (η_L^+, η_L^-, $\delta_{L,R}^+$, $\delta_{L,R}^-$ are not computed, printed, or plotted.)</p> <p>2 - Normal output plus AR, AI, BR, BI</p>
	KL(7)	0	<p>0 - Standard form for $V_{CN,R}$</p> <p>1 - Form A for $V_{CN,R}$ } Ref. 1</p> <p>2 - Form B for $V_{CN,R}$ }</p>
	KL(8)	0	<p>0 - Standard form for $V_{CN,\ell}$</p> <p>1 - Form A for $V_{CN,\ell}$ } Ref. 1</p> <p>2 - Form B for $V_{CN,\ell}$ }</p>
	KL(9)	0	<p>0 - Standard form for $V_{SO,R}$</p> <p>1 - Derivative of form A for $V_{SO,R}$ } Ref. 1</p> <p>2 - Form B for $V_{SO,R}$ }</p>
	KL(10)	0	<p>0 - Standard form for $V_{SO,\ell}$</p> <p>1 - Derivative of form A for $V_{SO,\ell}$ } Ref. 1</p> <p>2 - Form B for $V_{SO,\ell}$ }</p>
	KL(11)	0	<p>0 - No coulomb spin-orbit term } Eq. (2)</p> <p>1 - Includes coulomb spin-orbit }</p>
	KL(12)	0	<p>0 - Do not print and plot form factors (ref. 1)</p> <p>1 - Print and plot form factors; plot effective potential for $l = KX(9)$ (eq. (43)).</p>
	KL(13)	0	<p>0 - Save current input values for next case.</p> <p>1 - Initialize input to standard values before next case. (KL(3) is reset to 1.)</p>

TABLE III. - Continued. SCATLE INPUT VARIABLES APPEARING IN NAMELIST STATEMENTS

Namelist name	Variable name	Standard values	Description
KTR	KT(1)	1	1 - Single case, no search 2 - Grid, no search 3 - Grid, plus search 4 - Single case with search
	KT(2)	0	Not used
	KT(3)	0	Not used
	KT(4)	0	NF $\text{SUMFS} = \sum_{j=1}^{NF} \chi_{\sigma}^2(\theta_j)$; $\text{SUMFP} = \sum_{j=1}^{NF} \chi_{\text{P}}^2(\theta_j)$
	KT(5)	0	NR $\text{SUMMS} = \sum_{j=NF+1}^{NR} \chi_{\sigma}^2(\theta_j)$; $\text{SUMMP} = \sum_{j=NF+1}^{NR} \chi_{\text{P}}^2(\theta_j)$
	KT(6)	0	N1 $\text{SUMRS} = \sum_{j=NR+1}^{JMAX} \chi_{\sigma}^2(\theta_j)$; $\text{SUMRP} = \sum_{j=NR+1}^{JMAX} \chi_{\text{P}}^2(\theta_j)$
	KT(7)	0	IN1 $\text{SUM1S} = \sum_{j=N1}^{N1+IN1} \chi_{\sigma}^2(\theta_j)$; $\text{SUM1P} = \sum_{j=N1}^{N1+IN1} \chi_{\text{P}}^2(\theta_j)$
	KT(8)	0	N2 $\text{SUM2S} = \sum_{j=N2}^{N2+IN2} \chi_{\sigma}^2(\theta_j)$; $\text{SUM2P} = \sum_{j=N2}^{N2+IN2} \chi_{\text{P}}^2(\theta_j)$
	KT(9)	0	IN2
	KT(10)	0	N3 $\text{SUM3S} = \sum_{j=N3}^{N3+IN3} \chi_{\sigma}^2(\theta_j)$; $\text{SUM3P} = \sum_{j=N3}^{N3+IN3} \chi_{\text{P}}^2(\theta_j)$
	KT(11)	0	IN3
	KT(12)	0	N4 $\text{SUM4S} = \sum_{j=N4}^{N4+IN4} \chi_{\sigma}^2(\theta_j)$; $\text{SUM4P} = \sum_{j=N4}^{N4+IN4} \chi_{\text{P}}^2(\theta_j)$
	KT(13)	0	IN4 $\text{SUM34S} = \text{SUM3S} + \text{SUM4S}$ $\text{SUM34P} = \text{SUM3P} + \text{SUM4P}$
	XNORM	1	Normalization factor for $\sigma^{\text{ex}}(\theta)$ and $\Delta\sigma^{\text{ex}}(\theta)$; SNORM = XNORM when KX(5) = 1
	NP	0	All chi-square values are divided by (JMAX - NP) and printed out along with the unadjusted chi-square values.
	KX(1)	0	0 - Gaussian form for $V_{\text{CN},\sigma}$ (eq. (14)) 1 - Derivative of Woods-Saxon form for $V_{\text{CN},\sigma}$ (eq. (16)) 2 - Gaussian plus Woods-Saxon form for $V_{\text{CN},\sigma}$ (eq. (17)) 3 - Derivative of Woods-Saxon plus Woods-Saxon form for $V_{\text{CN},\sigma}$ (eq. (18))
	KX(2)	0	0 - Do not plot η_L^+ , η_L^- , $\delta_{L,R}^+$, $\delta_{L,R}^-$ (eqs. (20) and (21)). 1 - Plot η_L^+ , η_L^- , $\delta_{L,R}^+$, $\delta_{L,R}^-$ 2 - Plot and punch η_L^+ , η_L^- , $\delta_{L,R}^+$, $\delta_{L,R}^-$ } KL(6) \neq 1.

TABLE III. - Continued. SCATLE INPUT VARIABLES APPEARING IN NAMELIST STATEMENTS

Namelist name	Variable name	Standard values	Description
KTR	KX(3)	0	0 - $\Delta\sigma^{\text{ex}}(\theta)$ used in χ^2_{C} 1 - $\Delta\sigma^{\text{ex}}(\theta)$ replaced by $\sigma_{\text{coul}}^{\text{th}}(\theta)$ in χ^2_{C} ; when KX(3) = 1, KX(5) is set equal to 0.
	KX(4)	3	Determines what function will be minimized by search: 1 - CHI2ST 8 - SUM3S 15 - SUMMP 2 - CHI2PT 9 - SUM3P 16 - SUMRS 3 - CHI2T 10 - SUM4S 17 - SUMRP 4 - SUM1S 11 - SUM4P 18 - SUM34S 5 - SUM1P 12 - SUMFS 19 - SUM34P 6 - SUM2S 13 - SUMFP 7 - SUM2P 14 - SUMMS When KX(12) = 1, CHISQ(KX(4)) + CHISQ(KX(4) + 1) will be minimized.
	KX(5)	0	0 - SNORM = 1 1 - SNORM = XNORM 2 - SNORM = ENORM } KX(5) is set equal to 0 when KX(3) = 1.
	KX(6)	0	0 - Normal integration procedure 1 - Exchange potential in integration routine: If l is even, VS = VS. If l is odd, VS = VSODD.
	KX(7)	1	1 - AS and RS used to compute Woods-Saxon form of $V_{\text{CN},\text{R}}$ (eq. (10)) 2 - AO and RO used to compute Woods-Saxon form of $V_{\text{CN},\text{R}}$ (eq. (11)) } KX(7) is set equal to 1 when KL(1) = 2.
	KX(8)	0	Not used
	KX(9)	0	l -value used in angular momentum term when plotting effective potential (eq. (43)); this option is used only when KX(12) = 1.
	KX(10)	0	Not used
	KX(11)	0	0 - Do not call TRIPS 1 - Call TRIPS (standard output) 2 - Call TRIPS (standard output plus scattering amplitudes and $\sigma_{\text{coul}}^{\text{th}}(\theta)$ output)
	KX(12)	0	$\neq 1$ - Search on CHISQ(KX(4)) 1 - Search on CHISQ(KX(4)) + CHISQ(KX(4) + 1)
	KX(13)	0	Not used
PEI	FMI, FMB, ELAB, ZZ, RC	None	Mass, energy, charge product, coulomb radius
	VO, AO, RO, WI, WVI, AI, RI, VS, WS, AS, RS, VSODD	0	SCATLE parameters (nuclear potential parameters)
GRI	DVO, DAO, DRO, DWI, DWVI, DAI, DRI, DVS, DWS, DAS, DRS, DVSODD	0	Grid increments (table IV)
	NVO, NAO, NRO, NWI, NWVI, NAI, NRI, NVS, NWS, NAS, NRS, NVSODD	1	Number of grid values (table IV)

TABLE III. - Concluded. SCATLE INPUT VARIABLES APPEARING IN NAMELIST STATEMENTS

Namelist name	Variable name	Standard values	Description
RHI	LMAXM	25	t_{\max}
	NMAX	3	Number of RHOIN values (≤ 10)
	RHOIN(I) for I = 1 to 10	0.05, 0.5, 25. } 0.05, 0.5 }	$\begin{cases} \text{RHO}(1) = \text{RHOIN}(1) \\ \text{RHO}(I) = \text{RHO}(I-1) + \text{DRHOIN}(I); \text{RHO}(1) < \text{RHO}(I) \leq \text{RHOIN}(2) \\ \text{RHO}(I) = \text{RHO}(I-1) + \text{DRHOIN}(\text{NMAX}-1); \\ \text{RHOIN}(\text{NMAX}-1) < \text{RHO}(I) \leq \text{RHOIN}(\text{NMAX}) \end{cases}$
	DRHOIN(I) for I = 1 to 9		
SCHI	C(I, J) for I = 1 to 12 J = 1 to 10	0	Constraint matrix
	DELTA	None for FAC = 0 H(1, 1) · H(2, 2) · ... · H(N, N) for FAC \neq 0	Determinant of H-matrix
	E	0.1	Criteria for search cutoff
	FAC	-1	Controls input of H-matrix
	H(I, J), I = 1 to 12	FAC < 0: Diagonal matrix composed of standard elements from table IV FAC = 0: None FAC > 0: FAC × Identity matrix	Symmetric matrix used by search routines; when FAC = 0, only elements on diagonal and to right of diagonal are input.
	KSTEP	0	Number of random steps to be taken at end of search
	N	None	Number of parameters to be searched on
	NC	0	Number of constraints
	NHP	5	H-matrix is printed out every NHP iterations during search
	NSSW1	1	Output control: NSSW1 \geq 1 gives normal search output. NSSW1 < 1 gives minimum search output.
	NMLR	5	A search will be cut off after NMLR move left or move right output messages.
	NPCT	5 }	A search will terminate after NPCT iterations with less than PCT percent change.
	PCT	0.5 }	
	SRCH(I), I = 1 to 12	None	This array must contain the FORTRAN names of the N parameters to be searched on. Literal constants must be enclosed by apostrophes when read into NAMELIST (e. g., SRCH = 'VO', 'RS').
	VP	0	Factor for determining the length of random steps (card 31--0220.)
TSP	CSIG	FALSE	$\sigma^{\text{ex}}(\theta)$ and $\Delta\sigma^{\text{ex}}(\theta)$ are converted from mb/sr to fm ² /sr when CSIG = .TRUE.
	JMAX	None	Number of experimental data points.
	JOPT	0	When JOPT \neq 0, experimental data will be read with FORMAT 8E10.0 (table II).
	DTH	0 }	When DTH \neq 0, the THETAD array is generated from THI to THF in steps of DTH.
	THI	None }	
	THF	None }	
	THETAD-array	None	θ
	DPOLEX-array	None	Δp^{ex}
	DSGMEX-array	None	$\Delta\sigma^{\text{ex}}$
	POLEX-array	None	p^{ex}
	SGMAEX-array	None	σ^{ex}

TABLE IV. - SCATLE PARAMETERS - SEARCH AND GRID INFORMATION

1	2	3	4	5	6
SCAT4 parameter name	SCATLE parameter name	Grid increment	Number of grid values	Corresponding element in standard diagonal H-matrix	Increment for parameter for x_j in equation (50), Δx_j
V	VO	DVO	NVO	0.005	0.001
W	WI	DWI	NWI	.005	.001
	AO	DAO	NAO	.00001	.0001
	RO	DRO	NRO	.00001	.0001
	WVI	DWVI	NWVI	.001	.001
BG	AI	DAI	NAI	.00001	.0001
RG	RI	DRI	NRI	.00001	.0001
VS	VS	DVS	NVS	.001	.001
WS	WS	DWS	NWS	.001	.001
A	AS	DAS	NAS	.00001	.0001
RO	RS	DRS	NRS	.00001	.0001
	VSODD	DVSODD	NVSODD	.001	.001

TABLE V. - NONSTANDARD FORTRAN IV PROGRAMMING OPTIONS USED IN SCATLE

Option	Card numbers where used	Description
G-type format	02--0140 11--0940 22--0360 02--0150 11--1060 22--0520 11--0580 11--1100 22--0590 11--0620 11--1190 22--1120 11--0630 11--1360 25--0930 11--0640 11--1550 25--0940 11--0650 11--1970 26--0230 11--0670 20--0850 26--0250 11--0780 20--0860 26--0320 11--0790 20--0910 26--0330 11--0870 20--0920 26--0390 11--0880 26--0460	Output format option which causes each number to be examined to determine whether it fits I, E, or F format. If the number fits one of these formats, it is printed in that format. All other numbers are printed in O-type format.
Input of literal (BCD) constants on NAMELIST data cards	03--1520	This option permits the names of the SCATLE parameters to be entered into the SRCH-array on NAMELIST data cards. This is accomplished by enclosing the parameter names in apostrophes. Since these literal constants have less than six characters, they are left adjusted with the remaining characters set to blanks, for example, \$TSP N=3, SRCH='RI', 'VO', 'WVI' \$ will cause the SRCH-array to appear in the machine as SRCH(1) RIbbbb SRCH(2) VObbbb SRCH(3) WVIbbb
Generate random numbers	01--0290 31--0140	CALL SAND(X) initializes the procedure for generating random numbers. Each CALL RAND(Y) generates a new random number.
Printed plots	21--0740 21--1160 23--0390 24--0590 22--1080 23--0610 24--0940 21--0720	Each CALL PLOTXY(XDOWN, YACROS, KODE, P) generates a single curve plot. Each CALL PLOTMY(XDOWN, YACROS, KKK, P) generates a multiple curve plot. Each CALL SORTXY(V, W, NPTS) rearranges the NPTS of the V-array in order of increasing size. The elements of the W-array are moved to maintain the original pair-relation.

Ref. 5

Typical output listings. - The SCATLE output presented in this section is a portion of the output generated by running the standard potential case and the six example cases of the previous section. The first four pages of output from example 1 are shown. Values for the input variables and several initial calculations are listed on the first page, and the second through fourth pages contain all output from the search procedure. The last six pages of output from example 1 are not included since they correspond to the second page and to the last five pages of output from example 3.

Example 2 produces 40 pages of output. The portion presented here includes the initial page, and the initial and final parameters for each search procedure.

All 12 pages of output from example 3 are listed. The input potential parameters of this example agree to four figures with the final values of the search of example 1. Therefore, the final output values from example 1 are quite similar to the output values from example 3. The output from examples 4, 5, and 6, which consists of 21 pages, is not listed herein.

```

RUN NUMBER 1
STANDARD POTENTIAL CASE WITHOUT EXPERIMENTAL DATA

      N = 1 2 3 4 5 6 7 8 9 10 11 12 13
      KL(N)= 1 0 0 0 0 0 0 0 0 0 0 0 0
      KT(N)= 1 0 0 0 0 0 0 0 0 0 0 0 0
      KX(N)= 0 0 0 3 0 0 1 0 0 0 0 0 0

      BASIC INPUT DATA
      FMI= 1.00783      FMB= 27.97693      ELAB= 18.820      ZZ= 14.
      XNORM= 1.0000000  SNORM= 1.      JMAX= 35      NP= 0

      NUCLEAR POTENTIAL PARAMETERS
      VO= 60.000000      WI= 6.0000000      AO= 0      RD= 0
      VS= 6.0000000      WVI= 0      AI= 0.8000000      RI= 1.2000000
      VSODD= 0      WS= 0      AS= 0.6000000      RS= 1.0000000
      RC= 1.2500000

      BASIC COMPUTED QUANTITIES
      RHORO= 0      RHORI= 3.3497156      RHORS= 2.7914296      RHORC= 3.4892870
      ECM= 18.165609      K= 0.9195175      KAS= 0.5517105      KAI= 0.7356140
      ETA= 0.5101995

      INTEGRATION DATA
      RHOMAX= 25.000000      LMAXM=25      NMAX= 3
      RHOIN= 0.0500      0.5000      25.0000
      DRHOIN= 0.0500      0.5000

RUN NUMBER 1
THETA
5.0000000
10.000000
15.000000
20.000000
25.000000
30.000000
35.000000
40.000000
45.000000
50.000000
55.000000
60.000000
65.000000

SIGMATH
19502.611
1066.8035
230.55717
96.579293
50.409868
26.120771
11.937901
4.2748480
1.0820086
0.7001327
1.7489625
3.2012861
4.4103024

SIG/SIGC
0.9172991
0.7997761
0.8694993
1.1409455
1.4373500
1.5228981
1.2682216
0.7600241
0.3015014
0.2901839
1.0330060
2.5995876
4.7756708

POL TH
1.6765503E-03
1.2657248E-02
1.5116542E-02
-1.6100620E-02
-7.3879237E-02
-0.1570987
-0.2856010
-0.5127966
-0.8231835
0.2469563
0.4659013
0.3104368
0.1785101

```

70.000000	5.0628741	7.1197093	6.9308369E-02
75.000000	5.1076718	9.1140505	-2.6157600E-02
80.000000	4.6556681	10.326472	-0.1097795
85.000000	3.8846824	10.514505	-0.1769103
90.000000	2.9837244	9.6916710	-0.2157031
95.000000	2.1152926	8.1207087	-0.2042394
100.000000	1.3936460	6.2354569	-0.1051392
105.000000	0.8831912	4.5459146	0.1279789
110.000000	0.6042636	3.5349597	0.4517522
115.000000	0.5408755	3.5556094	0.5669629
120.000000	0.6502372	4.7521958	0.3688893
125.000000	0.8742473	7.0315315	0.1591130
130.000000	1.1498138	10.079298	7.4726537E-02
135.000000	1.4179195	13.421867	0.1040219
140.000000	1.6318933	16.532366	0.2156623
145.000000	1.7625985	18.946604	0.3835882
150.000000	1.8008391	20.368075	0.5825254
155.000000	1.7560279	20.728001	0.7800936
160.000000	1.6520144	20.189225	0.9302291
165.000000	1.5210953	19.095482	0.9704754
170.000000	1.3970447	17.876693	0.8344227
175.000000	1.3094758	16.948968	0.4914119

RUN NUMBER	1	STANDARD POTENTIAL CASE WITHOUT EXPERIMENTAL DATA			
	L	REAL C(L+1/2)	IMAG C(L+1/2)	REAL C(L-1/2)	IMAG C(L-1/2)
0	0.4108870	0.5872918	0.4158149	0.5329699	
1	0.1612435	0.2797029	4.7274854E-03	0.2355706	
2	-0.2608620	0.1779562	-0.4199165	0.3899489	
3	-0.2886678	0.4682251	0.1319349	0.4436573	
4	0.1623717	0.1346650	7.0444219E-02	4.4456440E-02	
5	3.0956736E-02	7.5457897E-03	1.1048209E-02	4.1612677E-03	
6	3.1027100E-03	5.1497504E-04	-7.9829085E-04	3.7459159E-04	
7	-1.9256093E-03	3.9758640E-05	-2.7292777E-03	3.6686320E-05	
8	-2.5147563E-03	8.5630705E-06	-2.6822239E-03	9.1137800E-06	
9	-2.2513660E-03	5.1906080E-06	-2.2862279E-03	5.3255428E-06	
10	-1.8607633E-03	3.4660762E-06	-1.8680033E-03	3.4963492E-06	
11	-1.4754299E-03	2.1772815E-06	-1.4769507E-03	2.1809079E-06	
12	-1.1506343E-03	1.3242082E-06	-1.1509994E-03	1.3236396E-06	
13	-8.7950244E-04	7.737465E-07	-8.7961549E-04	7.734572E-07	
14	-6.3914633E-04	4.0864590E-07	-6.3918725E-04	4.0775446E-07	
15	-4.5268404E-04	2.0605891E-07	-4.5271553E-04	2.0506866E-07	
16	-3.2030407E-04	1.0182136E-07	-3.2031742E-04	1.0288596E-07	
17	-2.0949129E-04	4.4049870E-08	-2.0949131E-04	4.4741154E-08	
18	-1.1748969E-04	1.3565904E-08	-1.1750402E-04	1.3254814E-08	
19	-6.1564481E-05	3.8641117E-09	-6.1572863E-05	3.7338010E-09	
20	-3.7483953E-05	1.0725489E-09	-3.7488161E-05	1.3687664E-09	
21	-2.5147821E-05	5.8122986E-10	-2.5166588E-05	2.6101441E-10	
22	-1.3541272E-05	3.4524781E-10	-1.3554924E-05	1.4652123E-10	
23	-3.6835778E-06	4.0009485E-11	-3.6806699E-06	2.1660470E-10	
24	1.6714246E-06	8.0880384E-11	1.6714222E-06	1.9599567E-10	
25	2.8766948E-06	8.7511669E-11	2.8766967E-06	-4.1383439E-12	

RUN NUMBER	1	STANDARD POTENTIAL CASE WITHOUT EXPERIMENTAL DATA					
	L	ETA1	ETA2	DELRI-DELPRI	DELPI	DELRI2-DELMRI	DELMRI
0	0.8401144	0.8342400	0.8900657	8.7108624E-02	0.8249604	9.0617098E-02	0.3184371
1	0.5460046	0.5289432	0.3159200	0.3025639	8.9380804E-03	7.0668893E-02	0.6242692
2	0.8288815	0.8681960	2.8011822	9.3839015E-02	2.4843516	4.0650533E-02	4.0545914E-03
3	0.5808226	0.2869239	2.4110109	0.2716549	0.5835958	3.7409572E-04	2.9240658E-05
4	0.7995855	0.9219161	0.2091128	0.1118309	7.6711250E-02	1.9222535E-06	1.1175872E-07
5	0.9868525	0.9919236	3.1389777E-02	6.6173484E-03	1.1139087E-02	1.1175871E-08	-0
6	0.9989893	0.9992521	3.1058690E-03	5.0559862E-04	3.1407938	-0	-0
7	0.9999279	0.9999415	3.1396669	3.6054659E-05	3.1388632	-0	-0
8	0.9999955	0.9999962	3.1390779	2.2426297E-06	3.1389104	-0	-0
9	0.9999997	0.9999998	3.1393413	1.2665988E-07	3.1393065	-0	-0
10	1.0000000	1.0000000	3.1397319	7.4505806E-09	3.1397247	-0	-0
11	1.0000000	1.0000000	3.1401173	3.7252903E-09	3.1401157	-0	-0
12	1.0000000	1.0000000	3.1404421	3.7252903E-09	3.1404417	-0	-0
13	1.0000000	1.0000000	3.1407132	-0	3.1407131	-0	-0
14	1.0000000	1.0000000	3.1409535	-0	3.1409535	-0	-0
15	1.0000000	1.0000000	3.1411400	3.7252903E-09	3.1411400	-0	-0
16	1.0000000	1.0000000	3.1412724	-0	3.1412724	-0	-0
17	1.0000000	1.0000000	3.1413832	-0	3.1413832	-0	-0
18	1.0000000	1.0000000	3.1414752	-0	3.1414752	-0	-0
19	1.0000000	1.0000000	3.1415311	3.7252903E-09	3.1415311	-0	-0
20	1.0000000	1.0000000	3.1415552	3.7252903E-09	3.1415552	-0	-0
21	1.0000000	1.0000000	3.1415676	3.7252903E-09	3.1415675	-0	-0
22	1.0000000	1.0000000	3.1415792	3.7252903E-09	3.1415792	-0	-0
23	1.0000000	1.0000000	3.1415890	3.7252903E-09	3.1415890	-0	-0
24	1.0000000	1.0000000	1.6714246E-06	3.7252903E-09	1.6714222E-06	-0	-0
25	1.0000000	1.0000000	2.8766948E-06	3.7252903E-09	2.8766967E-06	-0	-0

RUN NUMBER 1 EXAMPLE 1 SILICON 28 (P,P) E=18.82 SINGLE CASE SEARCH

CONTROLS

N =	1	2	3	4	5	6	7	8	9	10	11	12	13
KL(N)=	1	1	0	3	0	0	0	0	0	0	0	0	0
KT(N)=	4	0	0	0	0	0	0	0	0	0	0	0	0
KX(N)=	1	0	0	3	0	0	2	0	0	0	0	0	0

BASIC INPUT DATA

FMI= 1.00783	FMB= 27.97693	ELAB= 18.820	ZZ= 14.
XNORM= 1.0000000	SNORM= 1.	JMAX= 44	NP= 10

NUCLEAR POTENTIAL PARAMETERS

VO= 60.000000	WI= 6.0000000	AO= 0.8000000	RO= 1.0500000
VS= 6.0000000	WVI= 0	AI= 0.8000000	RI= 1.2000000
VSODD= 0	WS= 0	AS= 0.5000000	RS= 0.9500000
			RC= 1.2500000

BASIC COMPUTED QUANTITIES

RHORO= 2.9310011	RHORI= 3.3497156	RHORS= 2.6518582	RHORC= 3.4892870
ECM= 18.165609	K= 0.9195175	KAS= 0.4597588	KAI= 0.7356140
ETA= 0.5101995			

INTEGRATION DATA

RHOMAX= 15.000000	LMAXM=15	NMAX= 4
RHOIN= 0.0500	0.5000	5.0000
DRHOIN= 0.0500	0.1000	0.2000

RUN NUMBER 1 EXAMPLE 1 SILICON 28 (P,P) E=18.82 SINGLE CASE SEARCH

VARIABLE METRIC MINIMIZATION

N= 6	K= 0	E= 1.00000E-01	P= 0.	DELTA= 2.50000E-23
NHP= 5	NMLR= 5	NPCT= 5	PCT= 0.5000	
VO	WI	VS	AO	AI
60.0000	6.00000	6.00000	0.80000	0.80000

H

5.00000E-03	0.	0.	0.	0.	0.
0.	5.00000E-03	0.	0.	0.	0.
0.	0.	1.00000E-03	0.	0.	0.
0.	0.	0.	1.00000E-05	0.	0.
0.	0.	0.	0.	1.00000E-05	0.
0.	0.	0.	0.	0.	1.00000E-05

IT	0	STEP	0	F= 8.24182E 02	VS	AO	AI	AS
X=	60.0000	6.00000	6.00000	0.80000	0.80000	0.50000		
G=	52.5208	-860.764	-49.7360	6317.90	-5573.81	299.988		
ENORM=	1.34307	SIGMAR (TH)= 95.4705	CHI2T= 824.182	CHI2ST= 536.556	CHI2PT= 287.626			

IT	1	STEP	0	F= 5.00752E 02	GS= -4.43157E 03			
DELTA=	5.15794E-24							
X=	59.9574	6.69885	6.00808	0.78974	0.80905	0.49951		
G=	-0.33951	31.1241	-35.8391	2025.79	354.729	253.906		
ENORM=	1.15326	SIGMAR (TH)= 99.7806	CHI2T= 500.752	CHI2ST= 311.254	CHI2PT= 189.498			

IT	2	STEP	0	F= 4.78168E 02	GS= -4.81788E 01			
DELTA=	4.85679E-24							
X=	59.9575	6.60671	6.04225	0.77005	0.80651	0.49711		
G=	-0.45776	5.70679	-22.8806	-42.9916	-149.574	46.7300		
ENORM=	1.16026	SIGMAR (TH)= 98.2166	CHI2T= 478.168	CHI2ST= 282.282	CHI2PT= 195.886			

UNDERSHOT

IT 3 STEP 0 F= 4.76723E 02 GS= -8.96794E-01

DELTA= 9.71357E-24

VO	WI	VS	AO	AI	AS		
X= 59.9614	6.57218	6.08883	0.76997	0.80976	0.49609		
G= -0.78201	-1.23215	-12.1346	3.70026	-182.610	-13.8855		
ENORM= 1.16164	SIGMAR (TH)= 98.3731		CHI2T= 476.723		CHI2ST= 280.158	CHI2PT= 196.565	

UNDERSHOT

IT 4 STEP 0 F= 4.75603E 02 GS= -7.66493E-01

DELTA= 1.94271E-23

VO	WI	VS	AO	AI	AS		
X= 59.9719	6.53323	6.14188	0.76961	0.81487	0.49569		
G= 0.37384	-0.19836	-0.98419	14.7247	-130.577	-70.7245		
ENORM= 1.16142	SIGMAR (TH)= 98.6894		CHI2T= 475.603		CHI2ST= 277.742	CHI2PT= 197.861	

UNDERSHOT

IT 5 STEP 0 F= 4.74988E 02 GS= -3.98690E-01

DELTA= 3.88543E-23

VO	WI	VS	AO	AI	AS		
X= 59.9739	6.49360	6.17759	0.76908	0.82017	0.49669		
G= 1.52969	1.75476	4.82559	23.8037	-79.8416	-98.8770		
ENORM= 1.16131	SIGMAR (TH)= 99.0121		CHI2T= 474.988		CHI2ST= 276.564	CHI2PT= 198.423	

ERROR MATRIX

5.04116E-03	-1.65115E-04	2.80492E-04	-6.19368E-06	2.81032E-05	-1.58117E-06
-1.65115E-04	3.41031E-03	-2.06964E-03	5.26835E-05	-2.82769E-04	-8.86554E-06
2.80492E-04	-2.06964E-03	3.34332E-03	-2.73925E-05	2.48465E-04	1.20495E-06
-6.19368E-06	5.26835E-05	-2.73925E-05	9.54302E-06	-2.76653E-06	-1.74292E-07
2.81032E-05	-2.82769E-04	2.48465E-04	-2.76653E-06	3.80278E-05	1.67708E-06
-1.58117E-06	-8.86554E-06	1.20495E-06	-1.74292E-07	1.67708E-06	1.09893E-05

UNDERSHOT

IT 6 STEP 0 F= 4.74410E 02 GS= -3.42403E-01

DELTA= 7.77086E-23

VO	WI	VS	AO	AI	AS		
X= 59.9608	6.45270	6.19294	0.76825	0.82521	0.49917		
G= 3.14713	0.89264	5.29099	27.1988	-50.3159	-86.3266		
ENORM= 1.16185	SIGMAR (TH)= 99.2832		CHI2T= 474.410		CHI2ST= 276.579	CHI2PT= 197.831	

UNDERSHOT

IT 7 STEP 0 F= 4.73741E 02 GS= -3.94979E-01

DELTA= 1.55417E-22

VO	WI	VS	AO	AI	AS		
X= 59.9200	6.40765	6.19710	0.76707	0.83076	0.50301		
G= 3.28445	0.22888	2.38419	14.6866	-33.3023	-61.5692		
ENORM= 1.16227	SIGMAR (TH)= 99.5622		CHI2T= 473.741		CHI2ST= 277.513	CHI2PT= 196.227	

UNDERSHOT

IT 8 STEP 0 F= 4.73141E 02 GS= -4.24909E-01

DELTA= 3.10834E-22

VO	WI	VS	AO	AI	AS		
X= 59.8513	6.34207	6.20859	0.76545	0.83893	0.50854		
G= 2.78473	-1.94550	0.15259	7.82013	-17.6620	-30.0980		
ENORM= 1.16285	SIGMAR (TH)= 99.9777		CHI2T= 473.141		CHI2ST= 278.962	CHI2PT= 194.179	

UNDERSHOT

IT 9 STEP 0 F= 4.72937E 02 GS= -1.91945E-01

DELTA= 6.21668E-22

VO	WI	VS	AO	AI	AS		
X= 59.7770	6.29418	6.21655	0.76418	0.84546	0.51340		
G= 0.51117	-0.40817	-2.03705	-6.17981	1.71661	-10.3760		
ENORM= 1.16243	SIGMAR (TH)= 100.329		CHI2T= 472.937		CHI2ST= 280.560	CHI2PT= 192.377	

- - - - -

H

1.61791E-02	8.67207E-03	-1.20793E-03	2.20589E-04	-1.12486E-03	-8.18465E-04
8.67207E-03	1.14332E-02	-3.58654E-03	2.52970E-04	-1.31386E-03	-7.09034E-04
-1.20793E-03	-3.58654E-03	3.68662E-03	-6.39499E-05	4.42508E-04	1.26851E-04
2.20589E-04	2.52970E-04	-6.39499E-05	1.45785E-05	-2.85654E-05	-1.78690E-05
-1.12486E-03	-1.31386E-03	4.42508E-04	-2.85654E-05	1.70831E-04	9.22064E-05
-8.18465E-04	-7.09034E-04	1.26851E-04	-1.78690E-05	9.22064E-05	7.36106E-05

FINAL VALUES

ERROR MATRIX

1.61791E-02	8.67207E-03	-1.20793E-03	2.20589E-04	-1.12486E-03	-8.18465E-04
8.67207E-03	1.14332E-02	-3.58654E-03	2.52970E-04	-1.31386E-03	-7.09034E-04
-1.20793E-03	-3.58654E-03	3.68662E-03	-6.39499E-05	4.42508E-04	1.26851E-04
2.20589E-04	2.52970E-04	-6.39499E-05	1.45785E-05	-2.85654E-05	-1.78690E-05
-1.12486E-03	-1.31386E-03	4.42508E-04	-2.85654E-05	1.70831E-04	9.22064E-05
-8.18465E-04	-7.09034E-04	1.26851E-04	-1.78690E-05	9.22064E-05	7.36106E-05

DELTA= 6.21668E-22 F= 4.72937E 02 GS= -2.14612E-02

VO	WI	VS	AO	AI	AS
59.7770	6.29418	6.21655	0.76418	0.84546	0.51340
G= 0.51117	-0.40817	-2.03705	-6.17981	1.71661	-10.3760
ENORM= 1.16243	SIGMAR (TH)= 100.329	CHI2T= 472.937	CHI2ST= 280.560	CHI2PT= 192.377	
SUM OF CHI SQUARES / 34.	CHI2T= 13.9099	CHI2ST= 8.25177	CHI2PT= 5.65814		

RUN NUMBER 2 EXAMPLE 2 SILICON 28 (P,P) E=18.82 SEARCH WITH GRID ON AO AND AS

N =	CONTROLS												
	1	2	3	4	5	6	7	8	9	10	11	12	13
KL(N)=	1	1	0	3	0	0	0	0	0	0	0	0	0
KT(N)=	3	0	0	0	0	0	0	0	0	0	0	0	0
KX(N)=	1	0	0	3	0	0	2	0	0	0	0	0	0

BASIC INPUT DATA

FMI= 1.00783	FMB= 27.97693	ELAB= 18.820	ZZ= 14.
XNORM= 1.0000000	SNORM= 1.	JMAX= 44	NP= 10

NUCLEAR POTENTIAL PARAMETERS

VO= 60.000000	WI= 6.0000000	AO= 0.7000000	RO= 1.0500000
VS= 6.0000000	WVI= 0	AI= 0.8000000	RI= 1.2000000
VSODD= 0	WS= 0	AS= 0.5000000	RS= 0.9500000
			RC= 1.2500000

BASIC COMPUTED QUANTITIES

RHORQ= 2.9310011	RHORI= 3.3497156	RHORS= 2.6518582	RHORC= 3.4892870
ECM= 18.165609	K= 0.9195175	KAS= 0.4597588	KAI= 0.7356140
ETA= 0.5101995			

INTEGRATION DATA

RHOMAX= 15.000000	LMAXM=15	NMAX= 4	
RHOIN= 0.0500	0.5000	5.0000	15.0000
DRHOIN= 0.0500	0.1000	0.2000	

VO= 60.000000	WI= 6.0000000	AO= 0.7000000	RO= 1.0500000
VS= 6.0000000	WVI= 0	AI= 0.8000000	RI= 1.2000000
VSODD= 0	WS= 0	AS= 0.5000000	RS= 0.9500000

VARIABLE METRIC MINIMIZATION

N= 4	K= 0	E= 1.00000E-01	P= 0.	DELTA= 2.50000E-13
NHP= 5	NMLR= 5	NPCT= 5	PCT= 0.5000	
VO	WI	VS	AI	
X= 60.0000	6.00000	6.00000	0.80000	

```

H
      5.00000E-03   0.         0.         0.
      0.         5.00000E-03   0.         0.
      0.         0.         1.00000E-03   0.
      0.         0.         0.         1.00000E-05
IT   0 STEP   0 F=  8.39127E 02
      VO      WI      VS      AI
X=   60.0000   6.00000   6.00000   0.80000
G=   18.7988  -545.662  -6.73676  -4952.93
ENORM= 1.29809   SIGMAR (TH)= 91.3161   CHI2T=  839.127   CHI2ST=  438.634   CHI2PT=  400.492

```

UNDERSHOT

```

IT   8 STEP   0 F=  6.09582E 02 GS= -2.03440E-01
DELTA= 5.49510E-13
      VO      WI      VS      AI
X=   58.9726   5.28248   6.02324   1.00881
G=   9.15527E-02 -2.31934   5.39398  -0.45776
ENORM= 1.15287   SIGMAR (TH)= 108.857   CHI2T=  609.582   CHI2ST=  286.220   CHI2PT=  323.362

```

```

      VD= 60.000000      WI= 6.00000000      AO= 0.80000000      RO= 1.05000000
      VS= 6.00000000      WVI= 0      AI= 0.80000000      RI= 1.20000000
      VSDDD= 0      WS= 0      AS= 0.50000000      RS= 0.95000000

```

VARIABLE METRIC MINIMIZATION

```

N= 4 K= 0 E= 1.00000E-01 P= 0. DELTA= 5.49510E-13
NHP= 5 NMLR= 5 NPCT= 5 PCT= 0.5000
      VO      WI      VS      AI
X=   60.0000   6.00000   6.00000   0.80000

```

```

H
      8.46098E-03   2.22449E-03  -1.36860E-03  -5.17742E-04
      2.22449E-03   2.45093E-03  -5.73725E-04  -3.98457E-04
      -1.36860E-03  -5.73725E-04   1.88324E-03   1.67550E-04
      -5.17742E-04  -3.98457E-04   1.67550E-04   9.15804E-05
IT   0 STEP   0 F=  8.24182E 02
      VO      WI      VS      AI
X=   60.0000   6.00000   6.00000   0.80000
G=   52.5208  -860.764  -49.7360  -5570.22
ENORM= 1.34307   SIGMAR (TH)= 95.4705   CHI2T=  824.182   CHI2ST=  536.556   CHI2PT=  287.626

```

COLINEAR

```

IT   5 STEP   0 F=  5.19893E 02 GS= -5.06950E-01
DELTA= 5.58919E-13
      VO      WI      VS      AI
X=   60.2413   6.96744   6.19267   0.77580
G=  -1.57928  -2.81525  -1.43433  -31.4331
ENORM= 1.15890   SIGMAR (TH)= 98.1721   CHI2T=  519.893   CHI2ST=  307.338   CHI2PT=  212.555
      VD= 60.000000      WI= 6.00000000      AO= 0.70000000      RO= 1.05000000
      VS= 6.00000000      WVI= 0      AI= 0.80000000      RI= 1.20000000
      VSDDD= 0      WS= 0      AS= 0.55000000      RS= 0.95000000

```

VARIABLE METRIC MINIMIZATION

```

N= 4 K= 0 E= 1.00000E-01 P= 0. DELTA= 5.58919E-13
NHP= 5 NMLR= 5 NPCT= 5 PCT= 0.5000
      VO      WI      VS      AI
X=   60.0000   6.00000   6.00000   0.80000

```

```

H
      6.78425E-03   1.70795E-03  -7.69296E-04  -3.42263E-04
      1.70795E-03   5.15069E-03   4.09421E-04  -6.01555E-04

```

```

-7.69296E-04  4.09421E-04  1.72424E-03 -1.20906E-05
-3.42263E-04 -6.01555E-04 -1.20906E-05  8.48659E-05

IT   0 STEP   0 F=  8.29891E 02
    VO      WI      VS      AI
X=  60.0000  6.00000  6.00000  0.80000
G=  32.6233 -542.244 -57.2357 -4910.58
ENORM= 1.30165 SIGMAR(TH)= 91.3337 CHI2T= 829.891 CHI2ST= 448.990 CHI2PT= 380.901

```

RICOCHET

```

IT   4 STEP   0 F=  5.89731E 02 GS= -1.08734E-01

DELTA= 5.58886E-13
    VO      WI      VS      AI
X=  58.8634  5.25787  6.23021  1.01314
G= -0.64087  1.31989 -1.92261 -0.99182
ENORM= 1.15455 SIGMAR(TH)= 109.168 CHI2T= 589.731 CHI2ST= 289.685 CHI2PT= 300.047

```

```

    VO= 60.000000    WI= 6.0000000    AO= 0.8000000    RO= 1.0500000
    VS= 6.0000000    WVI= 0          AI= 0.8000000    RI= 1.2000000
    VSQDD= 0          WS= 0          AS= 0.5500000    RS= 0.9500000

```

VARIABLE METRIC MINIMIZATION

```

N= 4 K= 0 E= 1.00000E-01 P= 0. DELTA= 5.58886E-13
NHP= 5 VMLR= 5 NPCT= 5 PCT= 0.5000
    VO      WI      VS      AI
X=  60.0000  6.00000  6.00000  0.80000

```

H

```

8.67082E-03  3.27192E-03 -1.09463E-03 -6.87075E-04
3.27192E-03  4.12951E-03 -5.04715E-04 -6.34927E-04
-1.09463E-03 -5.04715E-04  1.56702E-03  1.04119E-04
-6.87075E-04 -6.34927E-04  1.04119E-04  1.18829E-04

```

```

IT   0 STEP   0 F=  8.47453E 02
    VO      WI      VS      AI
X=  60.0000  6.00000  6.00000  0.80000
G=  63.6749 -858.528 -86.1053 -5461.43
ENORM= 1.34704 SIGMAR(TH)= 95.4813 CHI2T= 847.453 CHI2ST= 551.122 CHI2PT= 296.331

```

RICOCHET

```

IT   5 STEP   0 F=  5.31088E 02 GS= -4.27264E-01

DELTA= 9.33008E-13
    VO      WI      VS      AI
X=  60.2372  7.01321  6.47004  0.76998
G= -0.69427  2.74658  3.73077 -3.96729
ENORM= 1.16036 SIGMAR(TH)= 97.8084 CHI2T= 531.088 CHI2ST= 307.648 CHI2PT= 223.440

```

RUN NUMBER 1 EXAMPLE 3 SILICON 28 (P,P) E=18.82 SINGLE CASE

N =	CONTROLS												
	1	2	3	4	5	6	7	8	9	10	11	12	13
KL(N)=	1	1	0	3	0	2	0	0	0	0	0	1	0
KT(N)=	1	0	0	0	0	0	0	0	0	0	0	0	0
KX(N)=	1	0	0	3	0	0	2	0	0	0	0	0	0

BASIC INPUT DATA

```

FMI= 1.00783      FMB= 27.97693      ELAB= 18.820      ZZ= 14.
XNORM= 1.0000000      SNORM= 1.      JMAX= 44      NP= 10

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NUCLEAR POTENTIAL PARAMETERS

VO= 59.780000	WI= 6.2940000	AO= 0.7642000	RO= 1.0500000
VS= 6.2170000	WVI= 0	AI= 0.8455000	RI= 1.2000000
VSDDD= 0	WS= 0	AS= 0.5134000	RS= 0.9500000
			RC= 1.2500000

BASIC COMPUTED QUANTITIES

RHORO= 2.9310011	RHORI= 3.3497156	RHORS= 2.6518582	RHORC= 3.4892870
ECM= 18.165609	K= 0.9195175	KAS= 0.4720803	KAI= 0.7774521
ETA= 0.5101995			

INTEGRATION DATA

RHOMAX= 15.000000	LMAX=15	NMAX= 4
RHOIN= 0.0500	0.5000	5.0000
DRHOIN= 0.0500	0.1000	0.2000

SUM OF CHI SQUARES

CHISQ SIGMA= 280.52768	CHISQ POL= 192.41044	CHISQ TOTAL= 472.93813
SUM OF CHI SQUARES / 34.		
CHISQ SIGMA= 8.2508142	CHISQ POL= 5.6591307	CHISQ TOTAL= 13.909945

REACTION CROSS SECTION AND DATA NORMALIZATION FACTOR

SIGMAR(TH)= 100.33423	ENORM= 1.1624686
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RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE		
THETA	SIGMA TH	SIGTH/SIGC	POL TH	SIGMA EX	SIGEX/SIGC	POL EX
5.180	15679.710	0.8494833	1.3878863E-03	15700.000	0.8505825	1.0000000
7.770	2666.1137	0.7299965	2.5145114E-03	2350.0000	0.6434428	1.0000000
12.950	339.09003	0.7124991	-1.2503671E-02	262.37600	0.5513068	1.0000000
15.530	193.01440	0.8356875	-3.1285520E-02	135.01600	0.5845739	-7.6999999E-02
18.120	126.24218	1.0085123	-5.2990013E-02	87.076999	0.6956330	1.0000000
20.710	86.685940	1.1756859	-7.6033229E-02	64.942999	0.8807953	1.0000000
23.300	59.235816	1.2797077	-0.1013589	0.1000000	2.1603614E-03	-0.1870000
25.870	39.155144	1.2772691	-0.1309221	20.406000	0.6656585	1.0000000
31.030	13.803928	0.9181994	-0.2197211	9.0890000	0.6045753	-0.2660000
36.180	2.7465358	0.3317344	-0.4195832	3.7120000	0.4483459	1.0000000
38.800	0.7360464	0.1164127	-0.5821097	0.1000000	1.5815947E-02	-0.6170000
41.330	0.2475967	4.9896246E-02	0.3617011	0.5470000	0.1102327	1.0000000
46.460	1.5288198	0.4807349	0.3994871	1.0110000	0.3179073	0.4000000
51.580	3.4064788	1.5858350	0.1692597	2.5090000	1.1680272	1.0000000
54.100	4.0447513	2.2477649	0.1075874	0.1000000	5.5572388E-02	0.1610000
56.690	4.4045787	2.9078532	5.6533065E-02	3.6320000	2.3978055	1.0000000
61.790	4.2878773	3.8724900	-3.0094878E-02	3.7420000	3.3794944	-0.1180000
66.870	3.4453608	4.1258313	-0.1160490	3.2140000	3.8487759	1.0000000
69.400	2.9169364	3.9804220	-0.1622959	0.1000000	0.1364590	-0.2360000
71.940	2.3880696	3.6929128	-0.2114980	2.3060000	3.5660003	1.0000000
76.990	1.4857117	2.8976247	-0.3095006	1.3630000	2.6582967	-0.4040000
82.030	0.8912685	2.1478465	-0.3556238	0.7550000	1.8194562	1.0000000
84.500	0.7130025	1.8932853	-0.3218145	0.1000000	0.2655370	-0.4510000
87.060	0.5936940	1.7356793	-0.2286860	0.4780000	1.3974448	1.0000000
92.060	0.4984139	1.7374185	7.0789014E-02	0.4540000	1.5825962	0.1430000
97.060	0.4978162	2.0389090	0.3360890	0.5190000	2.1256716	1.0000000
99.500	0.5068773	2.2347560	0.4199099	0.1000000	0.4408870	0.5800000
102.030	0.5137956	2.4370749	0.4788090	0.5820000	2.7605874	1.0000000
106.990	0.5078257	2.7543385	0.5325628	0.6070000	3.2922389	0.6100000
111.940	0.4733559	2.9011540	0.5226408	0.5240000	3.2115465	1.0000000
114.400	0.4486754	2.9101862	0.4946923	0.1000000	0.6486172	0.5790000
116.870	0.4214045	2.8857124	0.4499449	0.4300000	2.9445730	1.0000000
121.790	0.3668571	2.7778288	0.3097377	0.3420000	2.5896114	0.3400000
126.690	0.3206657	2.6580683	0.1185059	0.2850000	2.3624276	1.0000000
129.100	0.3024719	2.6125239	2.0539314E-02	0.1000000	0.8637245	8.0000000E-02
131.580	0.2869613	2.5798543	-7.0468131E-02	0.2690000	2.4183773	1.0000000
136.460	0.2648081	2.5591511	-0.1827467	0.2690000	2.5996619	-3.4000000E-02
141.330	0.2510328	2.5857115	-0.1651732	0.2800000	2.8840823	1.0000000
143.800	0.2462748	2.6119042	-0.1033306	0.1000000	1.0605648	9.8000000E-02
146.180	0.2427934	2.6433458	-1.4842476E-02	0.2840000	3.0919714	1.0000000
151.030	0.2386700	2.7250951	0.2219047	0.2910000	3.3225909	0.4340000
155.870	0.2384857	2.8337388	0.4635839	0.2650000	3.1487874	0.6800000
160.710	0.2421985	2.9726298	0.6239240	0.2530000	3.1052019	1.0000000
165.530	0.2489115	3.1322618	0.6461486	0.2550000	3.2088786	0.7400000

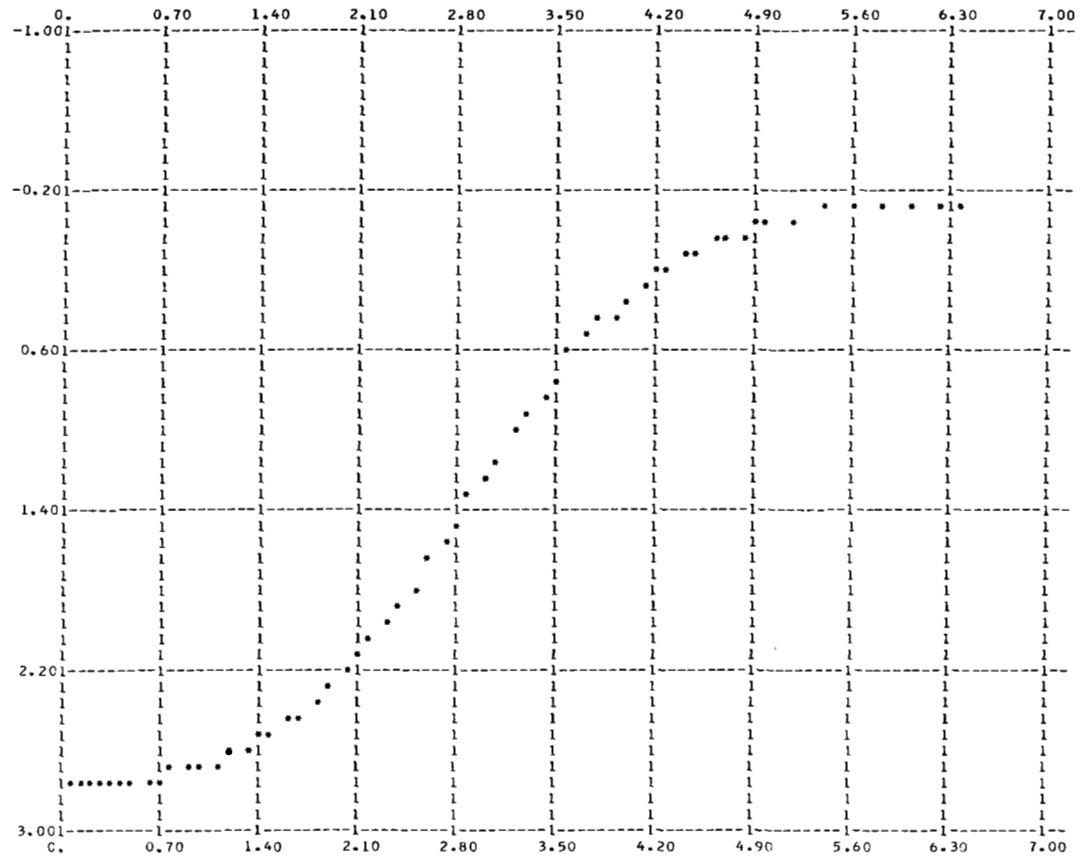
RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE
	AR	AI	BR	BI
110.89297		-58.158817	-0.1066592	-1.6281780E-02
28.684781		-42.933341	-0.1571137	-2.6897145E-02
-4.4477044		-17.867395	-0.2467559	-5.7223670E-02
-7.4116112		-11.747162	-0.2837676	-7.7985012E-02
-8.0776906		-7.8027890	-0.3145912	-0.1029910
-7.7054700		-5.2134228	-0.3382819	-0.1321368
-6.8529771		-3.4813522	-0.3541798	-0.1651236
-5.7992061		-2.3136658	-0.3617489	-0.2011009
-3.5643085		-0.9476917	-0.3510967	-0.2797219
-1.5654698		-0.2704655	-0.3060035	-0.3592358
-0.7086644		-5.6611151E-02	-0.2706070	-0.3967471
1.1170655E-03		0.1037110	-0.2292403	-0.4292881
1.0768472		0.3515894	-0.1271914	-0.4789854
1.6900079		0.5484719	-8.4916171E-03	-0.4994584
1.8419744		0.6342305	5.2941335E-02	-0.4968207
1.9092615		0.7147209	0.1162452	-0.4847271
1.8252724		0.8446249	0.2356366	-0.4328305
1.5354735		0.9236042	0.3385726	-0.3464188
1.3427649		0.9398961	0.3808843	-0.2923032
1.1308299		0.9393402	0.4160517	-0.2320222
0.6903431		0.8867367	0.4613636	-9.9899782E-02
0.2741723		0.7697713	0.4712799	3.8019395E-02
9.2433609E-02		0.6922601	0.4630767	0.1038965
-7.5164065E-02		0.6006489	0.4458346	0.1688100
-0.3322382		0.3983853	0.3886201	0.2798129
-0.4903354		0.1827994	0.3053906	0.3615360
-0.5323327		7.9092240E-02	0.2576258	0.3884231
-0.5533283		-2.4104075E-02	0.2045954	0.4064272
-0.5361774		-0.2051836	9.4762875E-02	0.4114112
-0.4591263		-0.3467726	-1.5269644E-02	0.3769279
-0.4055650		-0.3996956	-6.7573149E-02	0.3462221
-0.3454292		-0.4402976	-0.1173013	0.3073460
-0.2176284		-0.4830369	-0.2050890	0.2100211
-9.5982666E-02		-0.4768410	-0.2739569	9.4990802E-02
-4.3192271E-02		-0.4574650	-0.3001632	3.5130587E-02
4.1713044E-03		-0.4275293	-0.3216287	-2.6787462E-02
7.2572336E-02		-0.3435374	-0.3476012	-0.1438640
0.1046149		-0.2348674	-0.3530480	-0.2455258
0.1070159		-0.1735779	-0.3486922	-0.2882827
0.1010939		-0.1122627	-0.3404299	-0.3226112
6.7286364E-02		1.4721980E-02	-0.3128545	-0.3688466
1.1834987E-02		0.1368083	-0.2737513	-0.3803805
-5.4751443E-02		0.2465954	-0.2262742	-0.3566392
-0.1210144		0.3375969	-0.1734201	-0.3003678

RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE
	RHO(I)	FFCR	FFCI	FFSR
4.9999999E-02		0.9836964	5.5773134E-02	8.0154006E-02
0.1000000		0.9825150	5.9366311E-02	4.4514633E-02
0.1500000		0.9812497	6.3183208E-02	3.2959121E-02
0.2000000		0.9798948	6.7236732E-02	2.7450663E-02
0.2500000		0.9784440	7.1540345E-02	2.4384012E-02
0.3000000		0.9768911	7.6108165E-02	2.2559364E-02
0.3500000		0.9752291	8.0954888E-02	2.1464311E-02
0.4000000		0.9734508	8.6095843E-02	2.0844365E-02
0.4500000		0.9715486	9.1546956E-02	2.0559780E-02
0.5000000		0.9695143	9.7324777E-02	2.0528306E-02
0.6000000		0.9650152	0.1099296	2.1039957E-02
0.7000000		0.9598795	0.1240539	2.2155285E-02
0.8000000		0.9540258	0.1398492	2.3782535E-02
0.9000000		0.9473649	0.1574732	2.5890141E-02
1.0000000		0.9397999	0.1770871	2.8477027E-02
1.0999999		0.9312264	0.1988522	3.1557773E-02
1.1999999		0.9215340	0.2229251	3.5153228E-02
1.2999999		0.9106066	0.2494512	3.9282745E-02
1.3999999		0.8983255	0.2785579	4.3956224E-02
1.4999999		0.8845709	0.3103443	4.9165028E-02
1.5999999		0.8692265	0.3448707	5.4871450E-02
1.6999999		0.8521832	0.3821458	6.0997011E-02
1.7999999		0.8333445	0.4221124	6.7410705E-02
1.8999999		0.8126329	0.4646328	7.3919279E-02
1.9999999		0.7899958	0.5094737	8.0262785E-02
2.0999999		0.7654134	0.5562918	8.6119311E-02
2.1999999		0.7389044	0.6046230	9.1122676E-02
2.2999999		0.7105327	0.6538741	9.4894992E-02
2.3999999		0.6804115	0.7033225	9.7092385E-02
2.4999999		0.6487056	0.7521221	9.7457039E-02
2.5999998		0.6156311	0.7993198	9.5864356E-02
2.6999998		0.5814518	0.8438825	9.2352284E-02
2.7999998		0.5464722	0.8847341	8.7123209E-02
2.8999998		0.5110276	0.9208025	8.0516179E-02
2.9999998		0.4754718	0.9510731	7.2956217E-02
3.0999998		0.4401630	0.9746451	6.4893907E-02
3.1999998		0.4054494	0.9907860	5.6749653E-02
3.2999998		0.3716560	0.9989784	4.8873274E-02
3.3999998		0.3390729	0.9989549	4.1523312E-02
3.4999998		0.3079464	0.9907163	3.4864455E-02

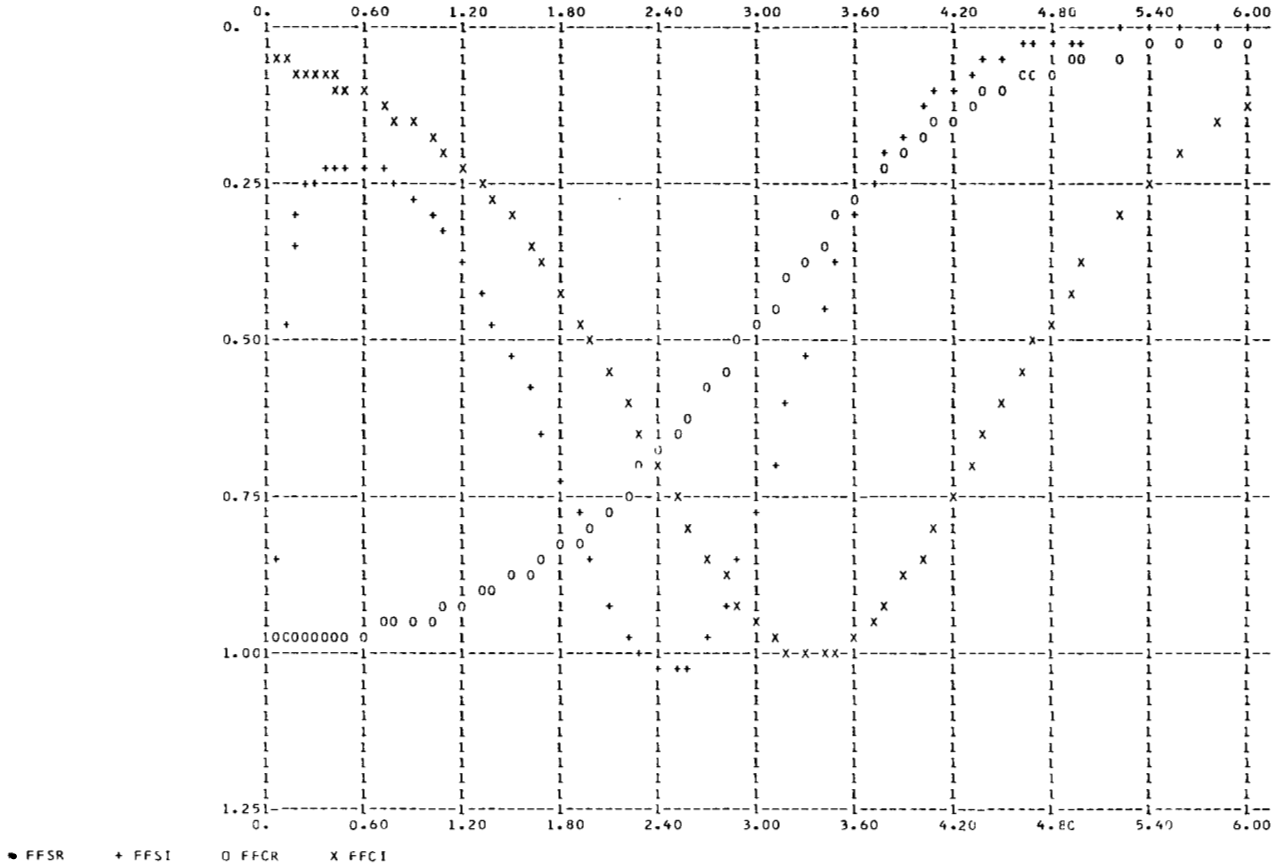
3.5999998	0.2784734	0.9745315	2.89777959E-02	2.89777959E-02
3.6999998	0.2507989	0.9509192	2.3879015E-02	2.3879015E-02
3.7999998	0.2250170	0.9206129	1.9535873E-02	1.9535873E-02
3.8999998	0.2011738	0.8845143	1.5887324E-02	1.5887324E-02
3.9999998	0.1792726	0.8436386	1.2856827E-02	1.2856827E-02
4.0999997	0.1592803	0.7990579	1.0362841E-02	1.0362841E-02
4.1999997	0.1411342	0.7518483	8.3257185E-03	8.3257185E-03
4.2999997	0.1247486	0.7030424	6.6718152E-03	6.6718152E-03
4.3999996	0.1100217	0.6535929	5.3355553E-03	5.3355553E-03
4.4999996	9.6840918E-02	0.6043451	4.2601188E-03	4.2601188E-03
4.5999995	8.5088283E-02	0.5560210	3.3972589E-03	3.3972589E-03
4.6999995	7.4644069E-02	0.5092129	2.7066355E-03	2.7066355E-03
4.7999995	6.5390212E-02	0.4643844	2.1549143E-03	2.1549143E-03
4.8999994	5.7212653E-02	0.4218779	1.7148030E-03	1.7148030E-03
4.9999994	5.0003048E-02	0.3819263	1.3641142E-03	1.3641142E-03
5.1999994	3.8089118E-02	0.3101560	8.6275637E-04	8.6275637E-04
5.3999994	2.8927412E-02	0.2492933	5.4558054E-04	5.4558054E-04
5.5999994	2.1919187E-02	0.1987222	3.4511169E-04	3.4511169E-04
5.7999994	1.6579851E-02	0.1573676	2.1842833E-04	2.1842833E-04
5.9999993	1.2524479E-02	0.1239691	1.3834852E-04	1.3834852E-04
6.1999993	9.4515034E-03	9.7257215E-02	8.7698380E-05	8.7698380E-05
6.3999993	7.1270635E-03	7.6054716E-02	5.5638407E-05	5.5638407E-05
6.5999993	5.3711812E-03	5.9324243E-02	3.5328551E-05	3.5328551E-05
6.7999993	4.0461296E-03	4.6182923E-02	2.2451173E-05	2.2451173E-05
6.9999993	3.0469625E-03	3.5897449E-02	1.4279202E-05	1.4279202E-05
7.1999993	2.2939652E-03	2.7869371E-02	9.0888244E-06	9.0888244E-06
7.3999993	1.7267341E-03	2.1616641E-02	5.7894372E-06	5.7894372E-06
7.5999992	1.2995802E-03	1.6754708E-02	3.6904180E-06	3.6904180E-06
7.7999992	9.7799071E-04	1.2979068E-02	2.3540257E-06	2.3540257E-06
7.9999992	7.3592195E-04	1.0049920E-02	1.5025522E-06	1.5025522E-06
8.1999992	5.5373597E-04	7.7792279E-03	9.5966017E-07	9.5966017E-07
8.3999991	4.1663346E-04	6.0200213E-03	6.1328548E-07	6.1328548E-07
8.5999991	3.1346628E-04	4.6577113E-03	3.9215102E-07	3.9215102E-07
8.7999990	2.3583943E-04	3.6031290E-03	2.5088716E-07	2.5088716E-07
8.9999989	1.7743269E-04	2.7869873E-03	1.6059334E-07	1.6059334E-07
9.1999989	1.3348871E-04	2.1555093E-03	1.0284684E-07	1.0284684E-07
9.3999988	1.0042706E-04	1.6669925E-03	6.5896065E-08	6.5896065E-08
9.5999987	7.5553298E-05	1.2891200E-03	4.2240065E-08	4.2240065E-08
9.7999986	5.6839914E-05	9.9686047E-04	2.7088075E-08	2.7088075E-08
9.9999986	4.2761348E-05	7.7083432E-04	1.7378512E-08	1.7378512E-08
10.199998	3.2169758E-05	5.9604154E-04	1.1153746E-08	1.1153746E-08
10.399998	2.4201547E-05	4.6087531E-04	7.1613673E-09	7.1613673E-09
10.599998	1.8206966E-05	3.5635566E-04	4.5997231E-09	4.5997231E-09
10.799998	1.3697188E-05	2.7553626E-04	2.9554400E-09	2.9554400E-09
10.999998	1.0304448E-05	2.1304427E-04	1.8995974E-09	1.8995974E-09
11.199998	7.7520704E-06	1.6472437E-04	1.2213622E-09	1.2213622E-09
11.399998	5.8319045E-06	1.2736307E-04	7.8553579E-10	7.8553579E-10
11.599998	4.3873556E-06	9.8475296E-05	5.0538352E-10	5.0538352E-10
11.799998	3.3006173E-06	7.6139446E-05	3.2524108E-10	3.2524108E-10
11.999998	2.4830610E-06	5.8869584E-05	2.0936997E-10	2.0936997E-10
12.199998	1.8680114E-06	4.5516769E-05	1.3481684E-10	1.3481684E-10
12.399998	1.4053080E-06	3.5192586E-05	8.6834143E-11	8.6834143E-11
12.599998	1.0572155E-06	2.7210121E-05	5.5943534E-11	5.5943534E-11
12.799998	7.9534493E-07	2.1038235E-05	3.6051124E-11	3.6051124E-11
12.999997	5.9833920E-07	1.6266265E-05	2.3237728E-11	2.3237728E-11
13.199997	4.5013148E-07	1.2576686E-05	1.4982056E-11	1.4982056E-11
13.399997	3.3863453E-07	9.7239863E-06	9.6615942E-12	9.6615942E-12
13.599997	2.5475525E-07	7.5183473E-06	6.2319365E-12	6.2319365E-12
13.799997	1.9165274E-07	5.8129991E-06	4.0206018E-12	4.0206018E-12
13.999997	1.4418063E-07	4.4944660E-06	2.5944808E-12	2.5944808E-12
14.199997	1.0846729E-07	3.4750082E-06	1.6745510E-12	1.6745510E-12
14.399997	8.1600083E-08	2.6867889E-06	1.0810171E-12	1.0810171E-12
14.599997	6.1387864E-08	2.0773573E-06	6.9799198E-13	6.9799198E-13
14.799997	4.6182171E-08	1.6061600E-06	4.5076471E-13	4.5076471E-13
15.000000	3.4742750E-08	1.2418371E-06	2.9115590E-13	2.9115590E-13

PLOT OF UCRB VS RHO

FLPT= 0.



PLOT OF FFSR, FFSI, FFCR, AND FFCI VS RHO

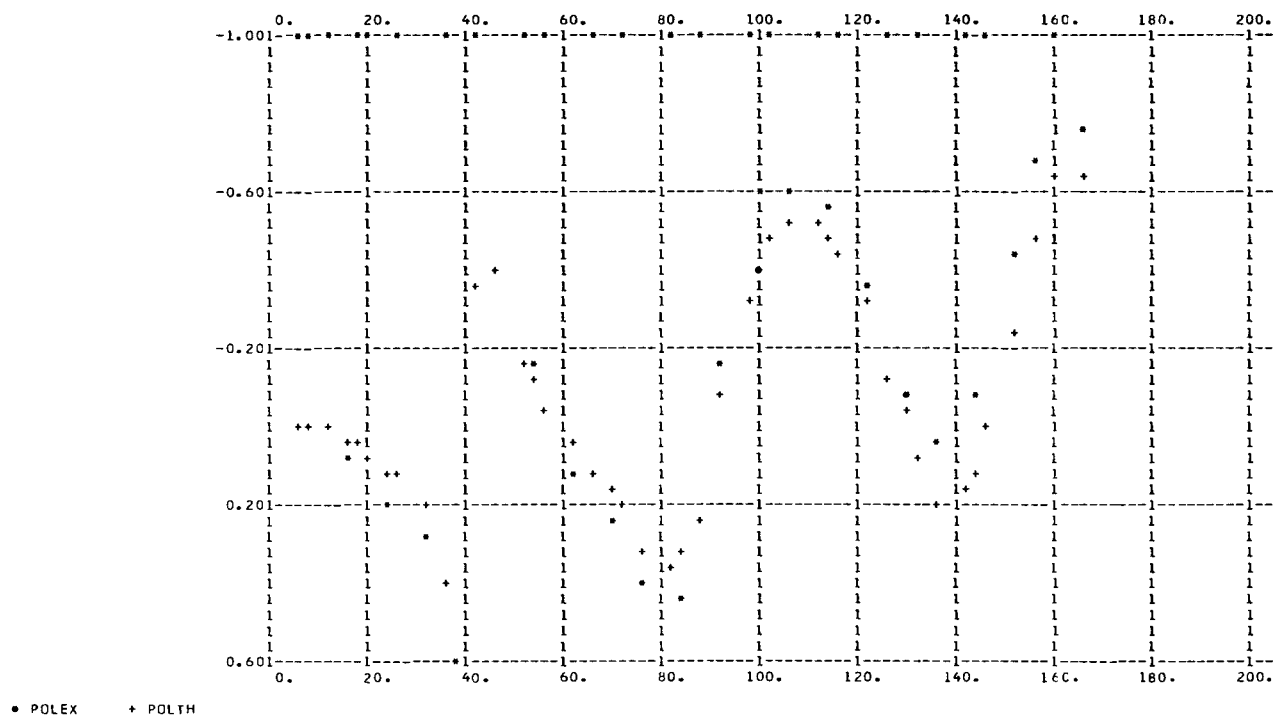


RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE	CHI SQUARE POL	CHI SQUARE TOTAL
THETA	SIGMA EX	DPOL EX	CHI SQUARE SIGMA			
5.1800000	1570.0000	1.0000000E 30	1.6701521E-04	0	1.6701521E-04	
7.7700000	235.00000	1.0000000E 30	1.8094685	0	1.8094685	
12.950000	26.237000	1.0000000E 30	8.5491178	0	8.5491178	
15.530000	13.502000	2.0000000E-02	18.451677	5.2245340	23.676211	
18.120000	8.7079999	1.0000000E 30	20.228483	0	20.228483	
20.710000	6.4939999	1.0000000E 30	11.210165	0	11.210165	
23.300000	9.9999999E 28	2.5000000E-02	0	11.735032	11.735032	
25.870000	2.0410000	1.0000000E 30	84.387260	0	84.387260	
31.030000	0.9090000	2.0000000E-02	26.904341	5.3543460	32.258686	
36.180000	0.3710000	1.0000000E 30	6.7721179	0	6.7721179	
38.800000	9.9999999E 28	2.8000000E-02	0	1.5527248	1.5527248	
41.330000	5.4999999E-02	1.0000000E 30	29.633835	0	29.633835	
46.460000	0.1010000	3.9000000E-02	26.285394	1.7292219E-04	26.285567	
51.580000	0.2510000	1.0000000E 30	12.785007	0	12.785007	
54.100000	9.9999999E 28	2.1000000E-02	0	6.4691650	6.4691650	
56.690000	0.3630000	1.0000000E 30	4.5297294	0	4.5297294	
61.790000	0.3740000	4.0000000E-02	2.1303302	4.8295689	6.9598990	
66.870000	0.3210000	1.0000000E 30	0.5194812	0	0.5194812	
69.400000	9.9999999E 28	2.2000000E-02	0	11.223739	11.223739	
71.940000	0.2310000	1.0000000E 30	0.1262237	0	0.1262237	
76.990000	0.1360000	4.9000000E-02	0.8141308	3.71934C9	4.5334716	
82.030000	7.5999999E-02	1.0000000E 30	3.2148749	0	3.2148749	
84.500000	9.9999999E 28	2.7000000E-02	0	22.892849	22.892849	
87.060000	4.7999999E-02	1.0000000E 30	5.8095114	0	5.8095114	
92.060000	4.4999999E-02	3.6000000E-02	0.9741228	4.0234771	4.9975998	
97.060000	5.1999999E-02	1.0000000E 30	0.1659592	0	0.1659592	
99.500000	9.9999999E 28	3.8000000E-02	0	17.7485C3	17.748503	
102.03000	5.7999999E-02	1.0000000E 30	1.3828310	0	1.3828310	
106.99000	6.0999999E-02	3.4000000E-02	2.6432534	5.1873049	7.8305584	
111.94000	5.1999999E-02	1.0000000E 30	0.9485278	0	0.9485278	
114.40000	9.9999999E 28	2.8000000E-02	0	9.0660667	9.0660667	
116.87000	4.3000000E-02	1.0000000E 30	3.9958048E-02	0	3.9958048E-02	
121.79000	3.3999999E-02	4.0000000E-02	0.5344959	0.5723782	1.1068741	
126.69000	2.8999999E-02	1.0000000E 30	1.5125345	0	1.5125345	
129.10000	9.9999999E 28	4.8000000E-02	0	1.5345369	1.5345369	
131.58000	2.7000000E-02	1.0000000E 30	0.4425374	0	0.4425374	
136.46000	2.7000000E-02	5.1000000E-02	2.4103834E-02	8.5065722	8.5306760	
141.33000	2.8000000E-02	1.0000000E 30	1.0702793	0	1.0702793	
143.80000	9.9999999E 28	4.4000000E-02	0	20.936991	20.936991	
146.18000	2.8000000E-02	1.0000000E 30	2.1657975	0	2.1657975	
151.03000	2.8599999E-02	3.9000000E-02	3.2561616	29.575546	32.431707	
155.87000	2.7000000E-02	4.9999999E-02	0.9643456	18.734368	19.698714	
160.71000	2.5000000E-02	1.0000000E 30	0.1866749	0	0.1866749	
165.53000	2.6000000E-02	4.9999999E-02	5.4837246E-02	3.5232337	3.5780709	

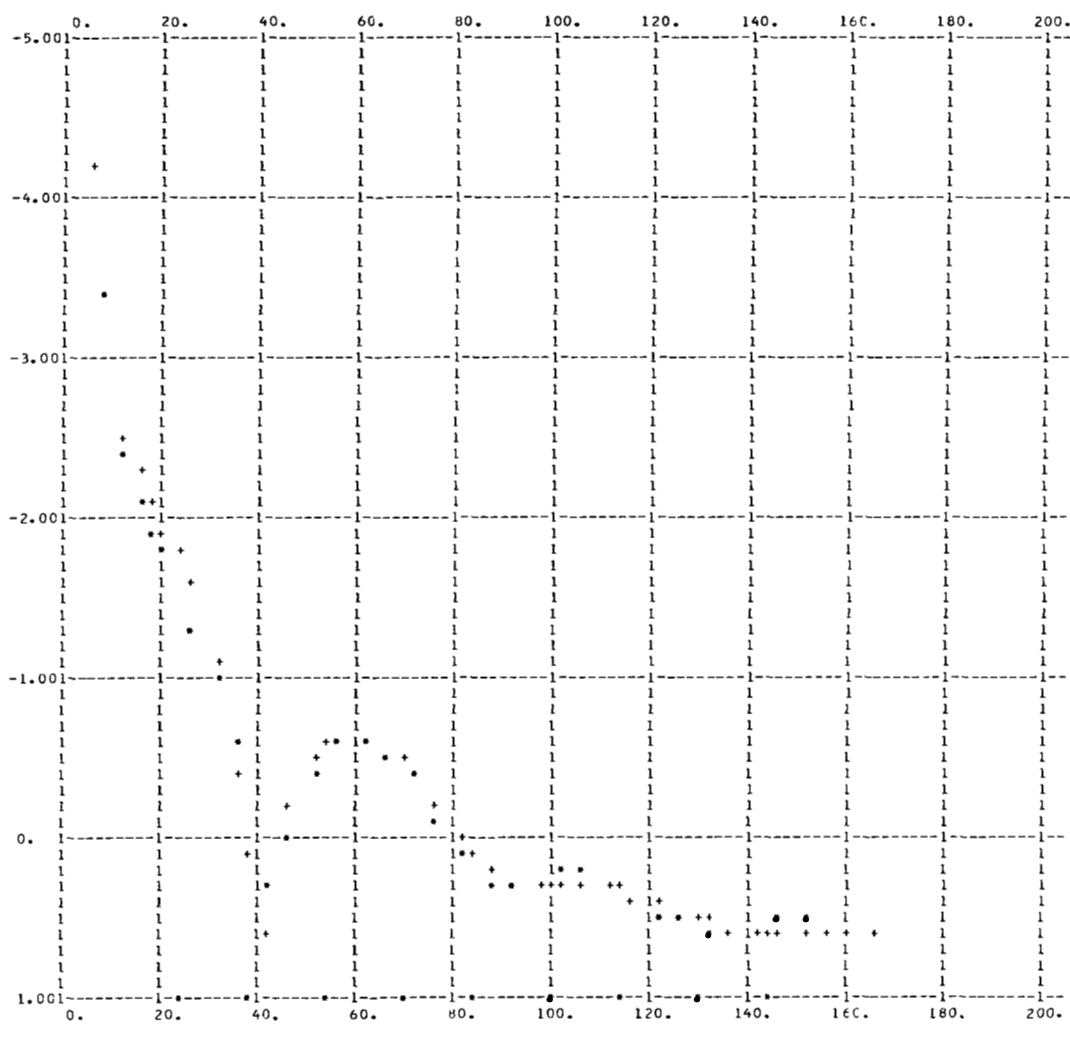
RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE	REAL C(L-1/2)	IMAG C(L-1/2)
L	REAL C(L+1/2)	IMAG C(L+1/2)				
0	0.1797416	0.6337050	0.1993897	0.4643705		
1	0.2075140	0.4301398	0.1424520	0.3554857		
2	-2.0074445E-02	0.323131	-0.1707857	0.3570086		
3	-0.2027441	0.3759233	-6.9572725E-02	0.5679760		
4	5.3130092E-02	0.3786884	0.1061343	0.2836448		
5	6.7871674E-02	0.1004405	5.8032002E-02	8.8889167E-02		
6	2.1710433E-02	2.7823952E-02	1.9809761E-02	2.7445244E-02		
7	6.2823109E-03	8.4491352E-03	5.9807702E-03	8.3943006E-03		
8	1.7717289E-03	2.6271696E-03	1.7235118E-03	2.6231314E-03		
9	4.9349798E-04	8.1922075E-04	4.8564087E-04	8.1891522E-04		
10	1.3623820E-04	2.5487865E-04	1.3494133E-04	2.5485352E-04		
11	3.6857079E-05	7.8806739E-05	3.6632877E-05	7.8803394E-05		
12	9.6379640E-06	2.3940782E-05	9.5954361E-06	2.3939455E-05		
13	2.5497706E-06	6.9950169E-06	2.5415491E-06	6.9958642E-06		
14	7.9680026E-07	1.9177817E-06	7.9584671E-07	1.9186472E-06		
15	3.2539769E-07	4.8349122E-07	3.2022431E-07	4.8272232E-07		

RUN NUMBER	1	EXAMPLE 3	SILICON 28 (P,P) E=18.82	SINGLE CASE	DEL R2-DELMR	DELM I
L	ETA1	ETA2	DEL R1-DELP R	DEL P I		
0	0.4480361	0.4501087	1.1051825	0.4014407	1.0265136	0.3991330
1	0.4379155	0.4058420	0.6230305	0.4128646	0.3891C59	0.4508957
2	0.3556473	0.3988733	3.0850273	0.5169078	2.6275221	0.4595557
3	0.4753954	0.1945364	2.6307878	0.3718042	1.9692993	0.8185679
4	0.2648722	0.4819713	0.2063998	0.6642540	0.2280319	0.3649354
5	0.8105661	0.8303732	8.4130075E-02	0.1050112	7.0116233E-02	9.2946025E-02
6	0.9453498	0.9467389	2.2973585E-02	2.8100132E-02	2.0530320E-02	2.7365980E-02
7	0.9831820	0.9832842	6.3899479E-03	8.4805076E-03	6.0825934E-03	8.4285667E-03
8	0.9947520	0.9947597	1.7810798E-03	2.6309259E-03	1.7325945E-03	2.6270387E-03
9	0.9983620	0.9983626	4.9430771E-04	8.1965046E-04	4.8643740E-04	8.1935194E-04
10	0.9994903	0.9994903	1.3630768E-04	2.5493071E-04	1.3501014E-04	2.5490462E-04
11	0.9998424	0.9998424	3.6862889E-05	7.8814727E-05	3.6638651E-05	7.8811001E-05
12	0.9999521	0.9999521	9.6384255E-06	2.3943013E-05	9.5958955E-06	2.3943013E-05
13	0.9999860	0.9999860	2.5498063E-06	6.9961441E-06	2.5415847E-06	6.9961441E-06
14	0.9999962	0.9999962	7.9680331E-07	1.9185281E-06	7.9584977E-07	1.9222535E-06
15	0.9999990	0.9999990	3.2539800E-07	4.8428797E-07	3.2022462E-07	4.8428797E-07

PLOT OF POLEX AND POLTH VS THETA (DEG)



PLOT OF SGMAEX AND SGMATH VS THETA (DEG)



SCATLE FORTRAN Listing

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$IBFIC CTRL4   LUST,DECK                                01--0010
C.....PAGE TITLING INFORMATION                          01--0020
COMMON/PTI/NUMRUN, TITLE(13)                            01--0030
C.....INDICATORS FOR INCREASES IN RHOMAX AND LMAXM      01--0040
COMMON/PCH/ NADL, NADR, NTOT                             01--0050
C.....SCATLE CONTROLS                                   01--0060
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)  01--0070
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM          01--0080
COMMON/AGN/L(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB, 01--0090
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,       01--0100
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RSS,S(12), SL, T(12), TO, 01--0110
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12),Z      01--0120
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA 01--0130
COMMON/TH1/DPOLEX(150), DSGMEX(150), JMAX, POLEX(150), POLTH(150), 01--0140
ISGMAEX(150), SGMATH(150), THETA(150), THETAD(150)      01--0150
C.....GRID VARIABLES                                   01--0160
COMMON/GDV/TRI, TRS, TVO, TWI, TAS, TVS, TWS, TAI, TWVI, TAO, TRO, 01--0170
ITVSODD,NRI, NRS, NVU, NWI, NAS, NVS, NWS, NAI, NWVI, NAO, NRO, 01--0180
2NVSODD,DRI, DRS, DVU, DWI, DAS, DVS, DWS, DAI, DWVI, DAO, DRU, 01--0190
3DVSODD                                                01--0200
C.....SCATLE PARAMETERS                                01--0210
COMMON/PARA/RI, RS, VU, WI, AS, VS, WS, AI, WVI, AO, RO, VSODD, 01--0220
INAME(12)                                              01--0230
COMMON/LIND/LMAX, LMAXM                              01--0240
C.....VARIABLES TO BE PLOTTED IN PTETDL                01--0250
COMMON/PTPL/AETA1(51), AETA2(51), DELR1(51), DELR2(51)  01--0260
DIMENSION SER(12), TSER(12),TPAR(12)                 01--0270
EQUIVALENCE (RI,SER), (TRI,TPAR)                     01--0280
CALL SAND(IX)                                          01--0290
NUMRUN=C                                              01--0300
KTRL(13)=1                                             01--0310
C.....SET UP INPUT DATA                                01--0320
3 CALL INPT4($38)                                       01--0330
C.....COMPUTE QUANTITIES NOT DEPENDENT ON NUCLEAR POTENTIAL PARAMETERS 01--0340
CALL SIGZKD                                           01--0350
CALL FSLBC                                           01--0360
CALL RFUTB                                           01--0370
NADL=1                                                01--0380
NADR=1                                                01--0390
NUMRUN= NUMRUN+1                                       01--0400
CALL SKIP                                           01--0410
C.....CHECK RHU AND L IN NUCLEAR POTENTIAL              01--0420
CALL PCTICH($38)                                       01--0430
IF(NTOT.GT.2)CALL SKIP                                01--0440
KOUT=0                                                01--0450
KSAVE= KSTEP                                           01--0460
IF(KSEND.EQ.1) GO TO 8                                 01--0470
C.....INITIAL OUTPUT                                    01--0480
CALL OUTPT4                                           01--0490
IF(KSEND.NE.3)CALL SKIP                                01--0500
8 CONTINUE                                           01--0510
C.....SET UP DO LOOPS FOR GRID ON NUCLEAR POTENTIAL PARAMETERS 01--0520
RI= TRI                                              01--0530
DO 33 IRI=1,NRI                                       01--0540
IF(IRI.GT.1) RI= RI+DRI                               01--0550
RS= TRS                                              01--0560
DO 33 IRS=1,NRS                                       01--0570
IF(IRS.GT.1)RS= RS+DRS                               01--0580
VO= TVO                                              01--0590
DO 33 IVU=1,NVU                                       01--0600
IF(IVU.GT.1) VO= VO+DVU                               01--0610
WI= TWI                                              01--0620
DO 33 IWI= 1,NWI                                       01--0630

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IF(IWI.GT.1) WI= WI+DWI	01--0640
AS= TAS	01--0650
DO 33 IAS= 1,NAS	01--0660
IF(IAS.GT.1) AS= AS+DAS	01--0670
VS= TVS	01--0680
DO 33 IVS=1,NVS	01--0690
IF(IVS.GT.1) VS= VS+DVS	01--0700
WS= TWS	01--0710
DO 33 IWS=1,NWS	01--0720
IF(IWS.GT.1) WS= WS+DWS	01--0730
AI= TAI	01--0740
DO 33 IAI= 1,NAI	01--0750
IF(IAI.GT.1) AI=AI+DAI	01--0760
WVI= TWVI	01--0770
DO 33 IWVI= 1,NWVI	01--0780
IF(IWVI.GT.1)WVI= wVI+DWVI	01--0790
AU= TAU	01--0800
DO 33 IAU=1,NAC	01--0810
IF(IAU.GT.1) AU= AU+DAU	01--0820
RU= TRU	01--0830
DO 33 IRU=1,NRU	01--0840
IF(IRU.GT.1) RU= RU+DRU	01--0850
VSODD= TVSODD	01--0860
DO 33 IVSODD=1,NVSODD	01--0870
IF(IVSODD.GT.1) VSODD = VSODD+DVSODD	01--0880
GO TO (18,17,13,15), KSEND	01--0890
C.....OUTPUT PARAMETERS FOR COMBINATION GRID AND SEARCH	01--0900
13 WRITE(6,20)	01--0910
20 FORMAT(1H1)	01--0920
CALL POUT	01--0930
DO 14 I=1,12	01--0940
14 TSER(I)=SER(I)	01--0950
15 KSTEP= KSAVE	01--0960
C.....ENTER SEARCH SUBROUTINES	01--0970
CALL ARGN	01--0980
17 CALL PUTICH(\$33)	01--0990
C.....COMPUTE NUCLEAR POTENTIALS	01--1000
18 CALL PCEN4	01--1010
C.....INTEGRATE RADIAL EQUATIONS	01--1020
CALL INTCTR(\$33)	01--1030
C.....COMPUTE VARIOUS SCATTERING AMPLITUDES	01--1040
CALL CSUBL	01--1050
CALL AB	01--1060
C.....COMPUTE CROSS SECTIONS AND POLARIZATIONS	01--1070
CALL SGSGCP	01--1080
CALL SIGMAR	01--1090
IF(KTRL(2).NE.0) CALL CHISQ	01--1100
GO TO (28,33,21,25),KSEND	01--1110
21 DO 23 I=1,12	01--1120
23 SER(I)=TSER(I)	01--1130
25 KOUT=1	01--1140
C.....FINAL OUTPUT	01--1150
28 CALL ULPT4	01--1160
C.....COMPUTE, OUTPUT, AND PLOT TRIPLE SCATTERING PARAMETERS	01--1170
IF(KTRLX(11).NE.0) CALL TRIPS	01--1180
C.....PLOT PHASE SHIFTS	01--1190
IF(KTRLX(2).NE.C.AND.KTRL(6).NE.1)CALL PTETDL(AETA1,AETA2,DELRI,	01--1200
1DELK2,LMAX)	01--1210
C.....PLOT CROSS SECTIONS AND POLARIZATIONS	01--1220
CALL PTSCAT	01--1230
33 CONTINUE	01--1240
DO 35 I=1,12	01--1250

35 SER(I)=TPAR(I)	01—1260
38 GO TO 3	01—1270
END	01—1280
\$IBFIC POUT LOST,DECK	02—0010
SUBROUTINE POUT	02—0020
C.....SCATLE PARAMETERS	02—0030
COMMON/PARA/PAR(12), NAME(12)	02—0040
DIMENSION IPU(12), NAMU(12), PARO(12)	02—0050
DATA (IPU(I),I=1,12)/3,4,10,11,9,8,1,6,7,5,2,12/	02—0060
DATA (NAMU(I),I=1,12)/6H VG,6H WI,6H AQ,6H RO,6H WVI	02—0070
1,6H AI,6H KI,6H VS,6H WS,6H AS,6H RS,6H VSODD/	02—0080
C.....OUTPUT SCATLE PARAMETERS	02—0090
DO 15 I=1,12	02—0100
J=IPU(I)	02—0110
15 PARO(I)=PAR(J)	02—0120
WRITE(6,10) (NAMU(I),PARO(I),I=1,12)	02—0130
10 FORMAT(1HK,A6,1H=1PG14.7,3(4X,A6,1H=G14.7),	02—0140
1/1HJ,21X,3(4X,A6,1H=G14.7),2(/1HJ,A6,1H=G14.7,3(4X,A6,1H=G14.7))	02—0150
RETURN	02—0160
END	02—0170
\$IBFIC INPT4 LOST,DECK	03—0010
SUBROUTINE INPT4(*)	03—0020
C.....PAGE TITLING INFORMATION	03—0030
COMMON/PTI/NUMRUN, TITLE(13)	03—0040
C.....SCATLE CONTROLS	03—0050
COMMON/CNTR/KULT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	03—0060
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	03—0070
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	03—0080
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	03—0090
ZM, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RSS,S(12), SL, T(12), TO,	03—0100
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12),Z	03—0110
C.....AUXILIARY SEARCH VARIABLES	03—0120
COMMON/ASV/DEL(12), ID(12), IIN, KULMAX, LABEL(13), NHP, NMLR,	03—0130
INPCT, NPCTP, PCT	03—0140
C.....ENERGY, MASS, AND CHARGE INPUT VALUES	03—0150
COMMON/EMCV/ELAB, FMB, FMI, FMU, RC, ZZ	03—0160
C.....OTHER SCATLE VARIABLES	03—0170
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHOBN,	03—0180
IRHOBN, SIGMA0, SIGMA1, TEMP	03—0190
COMMON/LIND/LMAX, LMAXM	03—0200
C.....GRID VARIABLES	03—0210
COMMON/GDV/TRI, TRS, TVO, TWI, TAS, TVS, TWS, TAI, TWVI, TAO, TRO,	03—0220
ITVSODD,NRI, NRS, NVO, NWI, NAS, NVS, NWS, NAI, NWVI, NAO, NRO,	03—0230
ZNVSODD,DKI, DKS, DVO, DWI, DAS, DVS, DWS, DAI, DWVI, DAO, DRO,	03—0240
3DVSODD	03—0250
C.....SCATLE PARAMETERS	03—0260
COMMON/PARA/RI, RS, VU, WI, AS, VS, WS, AI, WVI, AQ, RO, VSODD,	03—0270
INAME(12)	03—0280
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA	03—0290
COMMON/THI/DPULEX(150), DSGMEX(150), JMAX, POLEX(150), POLTH(150),	03—0300
1SGMAEX(150), SGMAH(150), THETA(150), THETAD(150)	03—0310

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C.....VARIABLES USED IN RHDTB                                03--0320
COMMON/RHU/DRHUIN( 9), NMAX, RHUIN(10)                        03--0330
C.....VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS)  03--0340
COMMON/PGU/FLPT,UGRB(250), UCIB(250), UCRM(250), UCIM(250),  03--0350
IUSRB(250), USIB(250), USRM(250), USIM(250)                  03--0360
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS    03--0370
COMMON/SACS/AAI(150),AR(150), BI(150), BR(150), FCI(150), FCR(150) 03--0380
L,SGMAC(150), SIGTEM(150), SRATIC(150)                        03--0390
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION 03--0400
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),        03--0410
LCHI2P(150), C HI2(150), ENORM, SGMRTN, SNORM, XNORM,NP,CSNRM,NCSN 03--0420
INTEGER SRCH                                                    03--0430
LOGICAL CSIG                                                    03--0440
DIMENSION DELI(12), DPAR(12), HD(12), KL(13), KT(13), KX(13),  03--0450
INPAR(12), PAR(12), SRCH(12), TPAR(12)                        03--0460
EQUIVALENCE (KL,KTRL), (KT,KTRLT), (KX,KTRLX),               03--0470
I(PAR,RI), (TPAR,TRI), (NPAR,NRI), (DPAR,DRI)                 03--0480
DATA(HD(1),I=1,12)/2*.00001,2*.005,.00001,2*.001,.00001,.001, 03--0490
12*.00001,.001/                                                03--0500
DATA(DELI(1),I=1,12)/2*.0001,2*.001,.0001,2*.001,.0001,.001, 03--0510
12*.0001,.001/                                                03--0520
NAMELIST/KTR/KL, KT, KX, XNORM, NP                           03--0530
NAMELIST/PEI/FMI, FMB, ELAB, ZZ, RC, VO, AU, RU, WI, WVI, AI, RI, 03--0540
IVS, WS, AS, RS, VSODD                                         03--0550
NAMELIST/GRI/DRI, DRS, DVO, DWI, DAS, DVS, DWS, DAI, DWVI, DAO, 03--0560
LURU, DVSODD,NRI, NRS, NVU, NWI, NAS, NVS, NWS, NAI, NWVI, NAO, 03--0570
ZNRO, NVSODD                                                    03--0580
NAMELIST/RHI/NMAX, LMAXM, RHUIN, DRHUIN                       03--0590
NAMELIST/SCHI/C, DELTA, E, FAC, H, KSTEP, N, NC, NHP, NSSW1, NMLR, 03--0600
INPUT, PCT, SRCH, VP                                           03--0610
NAMELIST/TSP/CSIG, DPOLEX, DSGMEX, DTH, JMAX, JCPT, POLEX, SGMAEX, 03--0620
LTHETA0, THI, THF                                              03--0630
IF(KL(13).EQ.0) GO TO 11                                       03--0640
C.....INITIALIZE INPUT VARIABLES                             03--0650
DO 5 I=1,13                                                    03--0660
KL(I)=C.                                                         03--0670
KT(I)=C.                                                         03--0680
KX(I)=C.                                                         03--0690
5 CONTINUE                                                      03--0700
KL(1)=1                                                         03--0710
KL(2)=1                                                         03--0720
KL(3)=1                                                         03--0730
KT(1)=1                                                         03--0740
KX(4)=3                                                         03--0750
KX(7)=1                                                         03--0760
DO 8 I=1,12                                                     03--0770
PAR(I)=0.                                                         03--0780
NPAR(I)=1                                                         03--0790
DPAR(I)=0.                                                       03--0800
8 CONTINUE                                                      03--0810
JUP=0                                                           03--0820
CSIG=.FALSE.                                                    03--0830
XNORM=1.                                                         03--0840
NP=0                                                             03--0850
NMAX= 3                                                         03--0860
LMAXM=25                                                         03--0870
RHUIN(1)=.05                                                     03--0880
RHUIN(2)=.5                                                      03--0890
RHUIN(3)=25.                                                     03--0900
DRHUIN(1)=.05                                                    03--0910
DRHUIN(2)=.5                                                     03--0920
DTH=0.                                                           03--0930

```

C.....READ TITLE AND CONTROLS	03--0940
11 READ(5,10) TITLE	03--0950
10 FORMAT(13A6)	03--0960
READ(5,KTR)	03--0970
C.....ELIMINATE INCONSISTENT USE OF KX(7)	03--0980
IF(KL(1).EQ.2.AND.KX(7).EQ.2)KX(7)=1	03--0990
C.....REMOVE POSSIBILITY OF NORMALIZING SGMAC	03--1000
IF(KX(3).EQ.1) KX(5)=0	03--1010
C.....SET UP SIGMA NORMALIZATION	03--1020
SNORM=1.	03--1030
IF(KX(5).EQ.1) SNORM=XNORM	03--1040
C.....SET UP INTERNAL PROGRAM CONTROLS	03--1050
KSEND= KT(1)	03--1060
FLPT = KX(9)	03--1070
KDLMAX=1	03--1080
KDLM=0	03--1090
NCSN=3	03--1100
DO 13 K=4,13	03--1110
13 KDLM=KDLM+KT(K)	03--1120
IF(KDLM.EQ.0) GO TO 18	03--1130
KDLMAX=2	03--1140
NCSN=15	03--1150
KDLM=KT(6)+KT(8)+KT(10)+KT(12)	03--1160
IF(KDLM.EQ.0) KDLMAX=3	03--1170
18 CONTINUE	03--1180
C.....READ SCATLE PARAMETERS AND ENERGY, MASS, AND CHARGE VALUES	03--1190
READ(5,PEI)	03--1200
CO2 = FM1+FMB	03--1210
FMU= (FM1*FMB)/CO2	03--1220
ECM= ELAB*(FMB/CO2)	03--1230
FKAY=.218739 *SQRT(FMU*ECM)	03--1240
TEMP = FKAY*(FMB**0.33333333)	03--1250
ETA=.157481 *ZZ*SQRT(FM1/ELAB)	03--1260
ETA2= ETA**2	03--1270
RHUBC= TEMP*KC	03--1280
DO 23 I=1,12	03--1290
TPAR(I)= PAR(I)	03--1300
23 CONTINUE	03--1310
C.....READ GRID VARIABLES	03--1320
IF(KSEND.EQ.2.OR.KSEND.EQ.3) READ(5,GRI)	03--1330
C.....READ INTEGRATION DATA	03--1340
READ(5,RHI)	03--1350
C.....INPUT FOR KNEE AND TAIL VARIATIONS	03--1360
CALL PGNIN	03--1370
C.....INITIALIZE AND READ IN SEARCH VARIABLES	03--1380
KDR=0	03--1390
IF(KSEND.LT.3) GO TO 48	03--1400
KSTEP=C	03--1410
NC=0	03--1420
NSSW1=1	03--1430
NHP=5	03--1440
NMLR=5	03--1450
NPCT=5	03--1460
PCT=.5	03--1470
E=.1	03--1480
VP =0.	03--1490
FAC= -1.	03--1500
DELTA=1.	03--1510
READ(5, SCHI)	03--1520
DO 45 I=1,N	03--1530
DO 33 K=1,12	03--1540
IF(NAME(K).EQ.SRCH(I)) GO TO 35	03--1550

33 CONTINUE	03--1560
WRITE(6,20) SRCH(I)	03--1570
20 FORMAT(1HKA6,44H IS NOT A SCATLE PARAMETER. GO TO NEXT CASE)	03--1580
KDR=1	03--1590
GO TO 48	03--1600
35 ID(I)=K	03--1610
Label(I)=NAME(K)	03--1620
DEL(I)= DEL1(K)	03--1630
DO 38 J=I,N	03--1640
IF(FAC.NE.0.) H(I,J)=0.	03--1650
38 H(J,I)= H(I,J)	03--1660
IF(FAC) 41,45,43	03--1670
41 H(1,1)=HD(K)	03--1680
GO TO 44	03--1690
43 H(1,1)=FAC	03--1700
44 DELTA=DELTA*H(1,1)	03--1710
45 CONTINUE	03--1720
IF(NPCT.GT.10)NPCT=10	03--1730
NPCTP=NPCT+1	03--1740
48 CONTINUE	03--1750
C.....READ EXPERIMENTAL DATA	03--1760
IF(KL(3).EQ.0) GO TO 63	03--1770
KL(3)=C	03--1780
READ(5,TSP)	03--1790
IF(DTH.EQ.0.)GO TO 53	03--1800
J=0	03--1810
51 J=J+1	03--1820
AJ=J-1	03--1830
THETAD(J)=THI+DTH*AJ	03--1840
IF(THETAD(J).LT.TH1.AND.J.LT.175)GO TO 51	03--1850
JMAX=J	03--1860
53 DO 58 J=1,JMAX	03--1870
IF(JOPT.NE.0)READ(5,50) THETAD(J), SGMAEX(J), DSGMEX(J), POLEX(J),	03--1880
IDPOLEX(J)	03--1890
50 FORMAT(8E10.0)	03--1900
THETA(J)=.0174532925*THETAD(J)	03--1910
C.....CONVERT FROM MILLIBARNS TO SQUARE FERMIS/STERAD	03--1920
IF(.NOT.CSIG) GO TO 58	03--1930
SGMAEX(J)=.1*SGMAEX(J)	03--1940
DSGMEX(J)= .1*DSGMEX(J)	03--1950
58 CONTINUE	03--1960
CSNRM=JMAX-NP	03--1970
CSIG= .FALSE.	03--1980
63 IF(KX(3).NE.0)GO TO 68	03--1990
DO 65 J=1,JMAX	03--2000
65 SIGTEM(J)=DSGMEX(J)	03--2010
68 IF(KDR.EQ.1)RETURN 1	03--2020
RETURN	03--2030
END	03--2040
\$IBFTC SIGZRC LUST,DECK	04--0010
SUBROUTINE SIGZRJ	04--0020
C.....OTHER SCATLE VARIABLES	04--0030
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHOBN,	04--0040
IRHOBN, SIGMA0, SIGMA1, TEMP	04--0050
C.....COMPUTE COULOMB PHASE SHIFT FOR L=0,1	04--0060
SIGMA0=-(ETA/(12.0*(ETA**2+16.0)))*(1.0+(ETA**2-48.0)/(30.0*((ETA**4-16.0*(ETA**2+16.0)*2)+16.0*(ETA**2)+1280.0)/(((16.0+ETA**2)**4)*104--0080	04--0070
	04--0080

```

205.0))
SIGMA0=SIGMA0-ETA+(ETA/2.0)*ALOG(ETA**2+16.0)+(7.0/2.0)*ATAN(ETA/
14.0))- (ATAN(ETA)+ATAN(ETA/2.0)+ATAN(ETA/3.0))
SIGMA1=SIGMA0+ATAN(ETA)
11 RETURN
END
04--0090
04--0100
04--0110
04--0120
04--0130
04--0140

$IBFTC FSUBC LOST,DECK
SUBROUTINE FSUBC
C.....OTHER SCATLE VARIABLES
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHOBN,
IRHOBNG, SIGMA0, SIGMA1, TEMP
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA
COMMON/TH1/POLEX(150), DSgMEX(150), JMAX, POLEX(150), POLTH(150),
ISGMAEX(150), SGMATH(150), THETA(150), THETAD(150)
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS
COMMON/SACS/A1(150), AK(150), BI(150), BK(150), FCI(150), FCR(150)
1,SGMAC(150), SIGTEM(150), SRATIO(150)
C.....COMPUTE COULUMB SCATTERING AMPLITUDES
DO 10 J=1,JMAX
SN=(SIN(THETA(J)/2.0))**2
FLN=ETA*(ALOG(SN))-2.0*SIGMA0
FNU=ETA/(2.0*FKAY*(SN))
23 FCR(J)=(-FNU*COS(FLN))
10 FCI(J)=(FNU*SIN(FLN))
27 RETURN
END
05--0C10
05--0C20
05--0C30
05--0040
05--0C50
05--0C60
05--0070
05--0C80
05--0090
05--0100
05--0110
05--0120
05--0130
05--0140
05--0150
05--0160
05--0170
05--0180
05--0190
05--0200

$IBFTC RHOTB LOST,DECK
SUBROUTINE RHOTB
C.....VARIABLES USED IN RHOTB
COMMON/RHU/DRHUIN( 9), NMAX, RHUIN(10)
C.....VARIABLES COMPUTED IN RHOTB
COMMON/RHT/DRHUL, DRHU(249), IFIRST, ILAST, RHU(250), RHOMAX
C.....GENERATE ARRAY OF RHU VALUES
DRHU(1)=DRHUIN(1)
RHU(1)=RHUIN(1)
NN=1
1=1
20 RHU(I+1)=RHU(I)+DRHUIN(NN)
IF (RHU(I+1)-RHUIN(NMAX))30,50,70
30 IF (ABS(RHU(I+1)-RHUIN(NN+1))-.5*DRHUIN(NN))35,35,40
35 NN=MINC(NN+1,NMAX-1)
40 DRHU(I+1)=DRHUIN(NN)
1=1+1
GO TO 20
50 ILAST=1+1
60 RHU(ILAST)=RHUIN(NMAX)
DRHU(ILAST-1)=RHU(ILAST)-RHU(ILAST-1)
RHOMAX=RHUIN(NMAX)
DRHUL=DRHUIN(NMAX-1)
83 RETURN
06--0010
06--0020
06--0030
06--0040
06--0050
06--0060
06--0070
06--0080
06--0090
06--0100
06--0110
06--0120
06--0130
06--0140
06--0150
06--0160
06--0170
06--0180
06--0190
06--0200
06--0210
06--0220
06--0230
06--0240

```

```

7C IF( (RHC(1+1)-RHUIN(NMAX))-.5*DRHCIN(NN))50,50,75
75 ILAST=1
GO TO 60
END

```

```

06--0250
06--0260
06--0270
06--0280

```

```

$IBFTC SKIP      LOST,DECK
SUBROUTINE SKIP
C.....PAGE TITLING INFORMATION
COMMON/PFI/NUMRUN, TITLE(13)
C.....SKIP TO NEXT PAGE, WRITE RUN NUMBER AND TITLE
WRITE(6,650)NUMRUN,TITLE
650 FORMAT(1H1,10HRUN NUMBERI3,10X,13A6)
RETURN
END

```

```

07--0010
07--0020
07--0030
07--0040
07--0050
07--0060
07--0070
07--0080
07--0090

```

```

$IBFTC PUTICH    LOST,DECK
SUBROUTINE PUTICH(*)
C.....VARIABLES COMPUTED IN RHOTB
COMMON/RHT/DRHUL, DRHU(249), IFIRST, ILAST, RHO(250), RHOMAX
C.....CONVERGENCE CRITERIA
COMMON/CONV/EPS1, EPS2, EPS3, EPS4
COMMON/LIND/LMAX, LMAXM
C.....OTHER SCATLE VARIABLES
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHUBN,
IRHUBNG, SIGMA0, SIGMA1, TEMP
C.....SCATLE PARAMETERS
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)
C.....INDICATORS FOR INCREASES IN RHOMAX AND LMAXM
COMMON/PCN/ NAUL, NAOR, NTUT
RHUBN=TEMP*RO
RHUBNG=TEMP*RG
FKAYA=FKAY*A
FKAYB=FKAY*BG
8 LMAX=LMAXM+1
FLMAX=LMAXM
C.....COMPUTE MAGNITUDE OF POTENTIALS AS A FUNCTION OF LMAXM
CALL PGNCK(FLMAX,TCR,TCI,TSR,TSI)
C.....IF MAGNITUDE OF CENTRAL POTENTIAL TOO LARGE, INCREASE LMAXM
IF(TCR.LT.EPS4.AND.TCI.LT.EPS4)GO TO 18
WRITE(6,10) LMAXM
10 FORMAT(7HJLMAXM=I5,3H +1,45H LMAXM TOO SMALL BECAUSE OF CENTRAL P
ENTIAL)
C.....LMAXM GT 50 CAUSES DIMENSIONS TO BE EXCEEDED
13 IF(LMAXM.EQ.50)GO TO 65
LMAXM=LMAXM+1
NAUL=NAUL+1
GO TO 8
16 TL=LMAX
C.....IF MAGNITUDE OF SPIN-ORBIT POTENTIAL TOO LARGE, INCREASE LMAXM
IF(TL*TSR.LT.EPS4.AND.TL*TSI.LT.EPS4)GO TO 23
WRITE(6,20) LMAXM

```

```

08--0010
08--0020
08--0030
08--0040
08--0050
08--0060
08--0070
08--0080
08--0090
08--0100
08--0110
08--0120
08--0130
08--0140
08--0150
08--0160
08--0170
08--0180
08--0190
08--0200
08--0210
08--0220
08--0230
08--0240
08--0250
08--0260
08--0270
08--0280
08--0290
08--0300
08--0310
08--0320
08--0330
08--0340
08--0350
08--0360

```



```

20 FORMAT(7HJLMAXM=I5,3H +1,48H LMAXM TOO SMALL BECAUSE OF SPIN ORBIT08--0370
1 POTENTIAL)08--0380
GO TO 1308--0390
23 IF(RHUMAX .GE.FLMAX)GO TO 4808--0400
C.....COMPUTE MAGNITUDE OF POTENTIAL AS A FUNCTION OF RHOMAX08--0410
28 CALL PGNCK(RHUMAX,TCR,TCI,ISR,TSI)08--0420
C.....IF MAGNITUDE OF CENTRAL POTENTIAL TOO LARGE, INCREASE RHOMAX08--0430
IF(TCR.LT.EPS4.AND.TCI.LT.EPS4)GO TO 3808--0440
WRITE(6,30) RHOMAX, DRHOL08--0450
30 FORMAT(8HJKRHOMAX=E16.9,2H+ E16.9,41H RHOMAX IS TOO SMALL IN NUCLEA08--0460
1R POTENTIAL)08--0470
C.....IF ILAST GT 250, RHO DIMENSIONS ARE EXCEEDED08--0480
33 IF(ILAST.EQ.250) GO TO 6508--0490
RHUMAX=RHUMAX+DRHOL08--0500
ILAST=ILAST+108--0510
RHU(ILAST)=RHU(ILAST-1)+DRHOL08--0520
DRHU(ILAST-1)=DRHOL08--0530
NADR=NADR+108--0540
GO TO 2808--0550
C.....IF MAGNITUDE OF SPIN-ORBIT POTENTIAL TOO LARGE, INCREASE RHOMAX08--0560
38 IF(TL*ISR.LT.EPS4.AND.TL*TSI.LT.EPS4)GO TO 4808--0570
WRITE(6,40) RHUMAX,DRHOL08--0580
40 FORMAT(8HJRHOMAX=E16.9,2H+ E16.9,44H RHOMAX IS TOO SMALL IN SPIN08--0590
ORBIT POTENTIAL)08--0600
GO TO 3308--0610
C.....IF LMAXM HAS BEEN INCREASED, RECOMPUTE COULOMB FUNCTIONS, PHASES08--0620
48 IF(NADL.EQ.0)GO TO 5308--0630
CALL EXSGML08--0640
CALL COULFN($65)08--0650
GO TO 5808--0660
C.....IF RHOMAX HAS BEEN INCREASED, RECOMPUTE COULOMB FUNCTIONS08--0670
53 IF(NADR.GT.0)CALL COULFN($65)08--0680
58 CONTINUE08--0690
NTUT=NADL+NADR08--0700
NADL=008--0710
NADR=008--0720
RETURN08--0730
65 WRITE(6,70)08--0740
70 FORMAT(48HKDIMENSIONS HAVE BEEN EXCEEDED. GO TO NEXT CASE)08--0750
RETURN 108--0760
END08--0770

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$IBFTC EXSGML LOST,DECK09--0010
SUBROUTINE EXSGML09--0020
C.....VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L09--0030
COMMON/VARL/C11(51), C12(51), CR1(51), CR2(51), EXSGMI(51),09--0040
1EXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)09--0050
COMMON/LIND/LMAX, LMAXM09--0060
C.....OTHER SCATLE VARIABLES09--0070
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOB, RHOBN,09--0080
1RHUBNG, SIGMA0, SIGMA1, TEMP09--0090
C.....COMPUTE COULOMB PHASE SHIFTS09--0100
1 FL=0.009--0110
EXSGMR(1)=COS(2.0*SIGMA0)09--0120
EXSGMI(1)=SIN(2.0*SIGMA0)09--0130
ETA2A=2.0*ETA09--0140
DO 20 L=2,LMAX09--0150
FL=FL+1.009--0160

```

TER 0=FL** 2	09--0170
TER 1=TER 0+ETA 2	09--0180
TER 2=(TER 0-ETA 2)/TER 1	09--0190
TER 3=(ETA 2A*FL)/TER 1	09--0200
13 EXSGMR(L)=(TER 2*EXSGMR(L-1))-(TER 3*EXSGMI(L-1))	09--0210
20 EXSGMI(L)=(TER 2*EXSGMI(L-1))+(TER 3*EXSGMR(L-1))	09--0220
17 RETURN	09--0230
END	09--0240

\$IBFTC COULFN LOST,DECK	10--0010
SUBROUTINE COULFN(*)	10--0020
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS	10--0030
COMMON/SACS/AI(150), AR(150), BI(150), BR(150), FCI(150), FCR(150)	10--0040
I,SGMAC(150), SIGTEM(150), SRATIO(150)	10--0050
C.....OTHER SCATLE VARIABLES	10--0060
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHQBC, RHQBN,	10--0070
IRHQBNG, SIGMA0, SIGMA1, TEMP	10--0080
C.....SCATLE CONTROLS	10--0090
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	10--0100
C.....CONVERGENCE CRITERIA	10--0110
COMMON/CONV/EPS1, EPS2, EPS3, EPS4	10--0120
COMMON/LIND/LMAX, LMAXM	10--0130
C.....VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L	10--0140
COMMON/VARL/CI1(51), CI2(51), CR1(51), CR2(51), EXSGMI(51),	10--0150
LEXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)	10--0160
C.....VARIABLES COMPUTED IN RHUTB	10--0170
COMMON/RHT/DRHOL, DRHO(249), IFIRST, ILAST, RHO(250), RHOMAX	10--0180
C.....COMPUTE COULUMB FUNCTIONS	10--0190
SQ=SQR I(1.0+ETA 2)	10--0200
1 IJ=1	10--0210
AR(1)=-ETA	10--0220
AI(1)=0.0	10--0230
AR(2)=-.5*ETA 2	10--0240
AI(2)=.5*ETA	10--0250
2 SI=0.0	10--0260
SR=0.0	10--0270
PR= RHOMAX	10--0280
DO 10 K=2,49	10--0290
TEM=PR*FLUAT(1-K)	10--0300
TR=AR(K)/TEM	10--0310
TI=AI(K)/TEM	10--0320
53 SQN=TR**2+TI**2	10--0330
IF(K-2) 4,4,3	10--0340
3 IF(SQN-SQ0) 4,4,11	10--0350
4 TR=SR+TR	10--0360
TI=SI+TI	10--0370
IF(TR-SR) 6,5,6	10--0380
5 IF(TI-SI) 6,13,6	10--0390
6 SR=TR	10--0400
SI=TI	10--0410
AR(K+1)=0.0	10--0420
AI(K+1)=0.0	10--0430
KP=K/2	10--0440
DU 7 MM=1,KP	10--0450
KM=K+1-MM	10--0460
AR(K+1)=AR(K+1)-AR(MM)*AR(KM)+AI(MM)*AI(KM)	10--0470
7 AI(K+1)=AI(K+1)-AI(KM)*AK(MM)-AI(MM)*AR(KM)	10--0480
IF(K-2*KP) 8,5,8	10--0490

8	AR(K+1)=AR(K+1)-.5*(AR(KP+1)**2-AI(KP+1)**2)	10--0500
	AI(K+1)=AI(K+1)-AR(KP+1)*AI(KP+1)	10--0510
9	FK=.5*FLUAT(K)	10--0520
	AI(K+1)=AI(K+1)-FK*AR(K)	10--0530
	AR(K+1)=AR(K+1)+FK*AI(K)	10--0540
	PR=PR*RHUMAX	10--0550
10	SQO=SQN	10--0560
	GO TO 101	10--0570
11	TEM=SR**2+SI**2	10--0580
	IF(TEM)105,105,12	10--0590
12	IF(ABS(SQO/TEM)-EPS3)13,13,106	10--0600
13	GO TO (14,15),IJ	10--0610
14	PAR=KHCUMAX-ETA*ALUG(2.0*KHUMAX)	10--0620
	PHIOR=PAR+SIGMA0+SR	10--0630
	PHIOI=SI	10--0640
	AR(2)=-1.0+AR(2)	10--0650
	IJ=2	10--0660
	GO TO 2	10--0670
15	PHIIR=PAR+SIGMA1-.157079632E+01+SR	10--0680
	PHIIL=SI	10--0690
25	T1=EXP(-PHIOI)	10--0700
	T2=EXP(-PHIIL)	10--0710
	G(1)=T1*COS(PHIOR)	10--0720
	G(2)=T2*COS(PHIIR)	10--0730
	F1=T1*SIN(PHIOR)	10--0740
	F2=T2*SIN(PHIIR)	10--0750
	IF(ABS(F1*G(2)-F2*G(1)-1.0/SQ)-EPS1) 31,31,102	10--0760
31	IDEC=11	10--0770
32	I=LMAX+IDEC	10--0780
	FBAR(I)=.1	10--0790
	FBAR(I+1)=0.0	10--0800
	LIMIT=LMAXM+IDEC	10--0810
	FL=LMAX+IDEC	10--0820
	T1=SQRT((FL+1.0)**2+ETA2)	10--0830
133	DO 33 I=1,LIMIT	10--0840
	L=LMAX+IDEC-I	10--0850
	FL=L	10--0860
	T2=SQRT(FL**2+ETA2)	10--0870
	FBAR(L)=((2.0*FL+1.0)*(ETA+FL*(FL+1.0)/RHUMAX)*FBAR(L+1)-FL*T1*FBA	10--0880
	IR(L+2))/((FL+1.0)*T2)	10--0890
600	IF(ABS(FBAR(L))-1.E+30)33,33,601	10--0900
601	K=LMAX+IDEC	10--0910
	FBAR(K)=FBAR(K)*0.1	10--0920
	GO TO 133	10--0930
33	T1=T2	10--0940
	ALPHA=1.0/((FBAR(1)*G(2)-FBAR(2)*G(1))*SQ)	10--0950
43	LMAXP=LMAX+1	10--0960
	DO 34 I=1,LMAXP	10--0970
34	FBAR(I)=ALPHA*FBAR(1)	10--0980
	IF(IDEC-11) 371,35,371	10--0990
371	IF(ABS(F1/FBAR(1)-1.0)-EPS2) 37,37,35	10--1000
35	DO 36 I=1,LMAXP	10--1010
36	F(I)=FBAR(I)	10--1020
	IDEC=IDEC+5	10--1030
	IF(IDEC-40) 32,32,103	10--1040
37	DO 38 I=1,LMAXP	10--1050
	IF(ABS(F(I)/FBAR(I)-1.0)-EPS2) 38,38,35	10--1060
38	CONTINUE	10--1070
	DO 381 I=1,LMAXP	10--1080
381	F(I)=FBAR(I)	10--1090
382	T1=SQ	10--1100
	DO 40 L=1,LMAXM	10--1110

```

      FL=L                                     10--1120
      T2=SQRT((FL+1.0)**2+ETA2)               10--1130
      G(L+2)=((2.0*FL+1.0)*(ETA+FL*(FL+1.0)/RHOMAX)*G(L+1)-(FL+1.0)*T1*G
1(L))/ (FL*T2)                               10--1150
      TS=FL/T1                                 10--1160
45  IF(ABS(F(L)*G(L+1)-F(L+1)*G(L)-TS)-EPS1) 40,40,104 10--1170
40  T1=T2                                       10--1180
41  DO 42 L=1,LMAX                             10--1190
      FL=L                                     10--1200
      TEM=FL**2                               10--1210
      T1=TEM/RHOMAX+ETA                       10--1220
46  T2=SQRT(TEM+ETA2)                         10--1230
      FP(L)=(T1*F(L)-T2*F(L+1))/FL            10--1240
42  GP(L)=(T1*G(L)-T2*G(L+1))/FL             10--1250
63  RETURN                                     10--1260
101 WRITE (6,121)RHOMAX,DRHUL                 10--1270
    GO TO 110                                  10--1280
102 WRITE (6,122)RHOMAX,DRHOL                 10--1290
    GO TO 110                                  10--1300
103 WRITE (6,123)RHOMAX,DRHUL                 10--1310
    GO TO 110                                  10--1320
104 WRITE (6,124)RHOMAX,DRHUL ,L              10--1330
    GO TO 110                                  10--1340
105 WRITE (6,125)RHOMAX,DRHUL                 10--1350
    GO TO 110                                  10--1360
106 WRITE (6,126)RHOMAX,DRHUL                 10--1370
110 IF (ILAST.EQ.250) RETURN 1                 10--1380
      RHOMAX=RHOMAX+DRHUL                     10--1390
      ILAST=ILAST+1                           10--1400
      RHO(ILAST)=RHO(ILAST-1)+DRHOL           10--1410
      DRHO(ILAST-1)=DRHOL                     10--1420
      GO TO 1                                  10--1430
121 FORMAT(18H INCREASE RHO MAX=E11.4,2H+ E11.4,35H A OR B SERIES CONV 10--1440
122 FORMAT(18H INCREASE RHO MAX=E11.4,2H+ E11.4,22H BAD INITIAL WRONSK 10--1460
123 FORMAT(18H INCREASE RHO MAX=E11.4,2H+ E11.4,24H L TOO LARGE IN FBA 10--1480
124 FORMAT(18H INCREASE RHO MAX=E11.4,2H+ E11.4,21H BAD WRONSKIAN FOR 10--1500
125 FORMAT(67H SERIES IN PHIO OR PHII IS ZERO, CHECK DATA, IF OK INCRE 10--1520
126 FORMAT(52H A OR B SERIES DIVERGES TOO QUICKLY INCREASE RHOMAX=E11. 10--1540
      END                                     10--1560

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$IBFTC OUTPT4  LUST,DECK                     11--0010
      SUBROUTINE OUTPT4                       11--0020
C.....SCATLE PARAMETERS                     11--0030
      COMMON/PARA/R0, R0, V, W, A, VS, WS, BG, DUMMY(4), NAME(12) 11--0040
C.....ENERGY,MASS, AND CHARGE INPUT VALUES 11--0050
      COMMON/EMCV/ELAB, FMB, FMI, FMO, RC, ZZ 11--0060
C.....CHI SQUARES, NUKMALIZATION CONSTANT, AND SIGMA REACTION 11--0070
      COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150), 11--0080
      ICHI2P(150), CHI2(150), ENORM, SGMRT, SNORM, XNORM, NP, CSNRM, NCSN 11--0090
C.....SCATLE INPUT AND OUTPUT VARUABLES WHICH ARE FUNCTIONS OF THETA 11--0100
      COMMON/THI/DOLEX(150), DSGMEX(150), JMAX, POLEX(150), POLTH(150), 11--0110
      ISGMAEX(150), SGMATH(150), THETA(150), THETAD(150) 11--0120

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C.....VARIABLES COMPUTED IN PGEN4 (FORM FACTORS) 11--0130
COMMON/PGF/FFCI(250), FFCIM(250), FFCR(250), FFCRM(250), FFSI(250) 11--0140
1,FFSIM(250), FFSR(250), FFSRM(250) 11--0150
C.....VARIABLES USED IN RHOTB 11--0160
COMMON/RHU/DRHOIN( 9), NMAX, RHUIN(10) 11--0170
C.....VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L 11--0180
COMMON/VARL/CI1(51), CI2(51), CR1(51), CR2(51), EXSGMI(51), 11--0190
1EXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51) 11--0200
COMMON/LIND/LMAX, LMAXM 11--0210
C.....VARIABLES TO BE PLOTTED IN PTETDL 11--0220
COMMON/PTPL/AETA1(51), AETA2(51), DELR1(51), DELR2(51) 11--0230
C.....SCATLE CONTROLS 11--0240
COMMON/CNIR/KGUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13) 11--0250
C.....OTHER SCATLE VARIABLES 11--0260
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHUBN, 11--0270
1RHUBNG, SIGMA0, SIGMA1, TEMP 11--0280
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS 11--0290
COMMON/SACS/A1(150), AR(150), B1(150), BR(150), FCI(150), FCR(150) 11--0300
1,SGMAC(150), SIGTEM(150), SRATIO(150) 11--0310
C.....VARIABLES COMPUTED IN RHOTB 11--0320
COMMON/RHT/DRHOL, DRHU(249), IFIRST, ILAST, RHO(250), RHOMAX 11--0330
C.....AUXILIARY SEARCH VARIABLES 11--0340
COMMON/ASV/DEL(12), ID(12), IIN, KOLMAX, LABEL(13), NHP, NMLR, 11--0350
INPT, NPCIP, PCT 11--0360
DIMENSION DELP1(51), DELM1(51) 11--0370
DIMENSION IDK(4), SNID(3), CHIQS(19) 11--0380
EQUIVALENCE (CHIQS(1),CHI2ST) 11--0390
DATA (IDK(1),I=1,4)/6H N =,6HKL(N)=,6HKT(N)=,6HKK(N)=/ 11--0400
DATA (SNID(1),I=1,3)/6H 1. ,6H XNORM,6H ENORM/ 11--0410
C.....SCATLE OUTPUT 11--0420
C.....INITIAL PAGE OUTPUT 11--0430
IF(KOUT.EQ.1)GO TO 11 11--0440
WRITE(6,10) IDK(1), (I,I=1,13),IDK(2), KTRL, IDK(3), KTRLT, 11--0450
1IDK(4), KTRLX 11--0460
10 FORMAT(1HK,46X,8HCONTROLS/1HJ,14X,A6,13I5/1HK,14X,A6,13I5, 11--0470
12(/1HJ,14X,A6,13I5)) 11--0480
NKM=KTRLX(5) + 1 11--0490
WRITE(6,20) FMI, FMB, ELAB, ZZ,XNORM,SNID(NRM), JMAX, NP 11--0500
20 FORMAT(1HL,42X,16HBASIC INPUT DATA/8HK FMI=F10.5,9X, 11--0510
16H FMB=F10.5,9X,6H ELAB=F8.3,11X,6H ZZ=F5.0/ 11--0520
28HK XNORM=F10.7,9X,6HSNORM=A6,13X,6H JMAX=14,15X,6H NP=13) 11--0530
WRITE(6,30) 11--0540
30 FORMAT(1HL,36X,28HNUCLEAR POTENTIAL PARAMETERS) 11--0550
CALL POUT 11--0560
WRITE(6,40) RL 11--0570
40 FORMAT(1H+,79X,3HRC=1PG14.7) 11--0580
RHOKU=TEMP*DUMMY(3) 11--0590
WRITE(6,50) RHOU, RHUBNG, RHUBN, RHOBC, ECM, FKAY, FKAYA, 11--0600
1FKAYB, ETA 11--0610
50 FORMAT(1HK,37X,25HBASIC COMPUTED QUANTITIES/7HRRHORO=1PG14.7,5X, 11--0620
16HRRHORI=G14.7,5X,6HRRHORS=G14.7,5X,6HRRHORC=G14.7/ 11--0630
27HK ECM=G14.7,5X,6H K=G14.7,5X,6H KAS=G14.7,5X,6H KAI=G14.7/ 11--0640
37HK ETA=G14.7) 11--0650
WRITE(6,60) RHOMAX, LMAXM, NMAX, (RHUIN(I),I=1,NMAX) 11--0660
60 FORMAT(1HJ,42X,16HINTEGRATION DATA/8HRRHOMAX=1PG14.7,12X, 11--0670
16HLMAXM=12,25X,5HNMAX=12/7HRRHOIN=OP10F12.4) 11--0680
NMAXM=NMAX-1 11--0690
WRITE(6,70) (DRHUIN(I),I=1,NMAXM) 11--0700
70 FORMAT(8HDKRHUIN=6X,9F12.4) 11--0710
CALL PGNOUT 11--0720
IF(KSEND.GT.1)GO TO 121 11--0730
11 GO TO (15,121,21,21),KSEND 11--0740

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C.....INITIAL PAGE OUTPUT, SINGLE CASE ONLY
15 IF(KTRL(2).NE.1)GO TO 35
WRITE(6,80) CHI2ST, CHI2PT, CHI2T
80 FORMAT(1HL,41X,18HSUM OF CHI SQUARES/13HKCHISQ SIGMA=1PG14.7,7X,
110HCHISQ PUL=G14.7,9X,12HCHISQ TOTAL=G14.7)
IF(KDLMAX.EQ.1)GO TO 16
WRITE(6,90)
90 FORMAT(1HJ)
CALL SUUF
16 DO 17 KK=1,NC SN
17 CHIQS(KK)=CHIQS(KK)/CSNRM
WRITE(6,280) CSNRM, CHI2ST, CHI2PT, CHI2T
280 FORMAT(1HK,36X,20HSUM OF CHI SQUARES /F5.0/13HKCHISQ SIGMA=1PG14.7
1,7X,10HCHISQ PUL=G14.7,9X,12HCHISQ TOTAL=G14.7)
IF(KDLMAX.EQ.1)GO TO 18
WRITE(6,90)
CALL SUUF
18 WRITE(6,100) SGMATH, ENORM
100 FORMAT(1HL,24X,52HREACTION CROSS SECTION AND DATA NORMALIZATION FA
ICTUR/1HK,20X,11HSIGMAR(TH)=1PG14.7,19X,6HENORM=G14.7)
C.....OUTPUT EXPERIMENTAL,THEORETICAL CROSS SECTION, POLARIZATION
21 CALL SKIP
WRITE(6,110)
110 FORMAT(1HJ,2X,5HTHETA,6X,8HSIGMA TH,8X,10HSIGTH/SIGC,9X,6HPOL TH,
110X,8HSIGMA EX,8X,10HSIGEX/SIGC,9X,6HPOL EX)
IF(KTRLX(5).NE.C)WRITE(6,120) SNID(NRM)
120 FORMAT(1H+,111X,A6,7H*SGMAEX)
DO 28 J=1,JMAX
SIGXOC=SGMAEX(J)/SGMAC(J)
WRITE(6,220) THETA(J), SGMATH(J), SRATIO(J), POLTH(J), SGMAEX(J),
1SIGXOC, POLEX(J)
220 FORMAT(1HJ,F8.3,1PG17.7)
IF(KTRLX(5).EQ.C)GO TO 28
SGMEXN=SNORM*SGMAEX(J)
WRITE(6,130) SGMEXN
130 FORMAT(1H+,110X,1PG17.7)
28 CONTINUE
GO TO 41
C.....OUTPUT THEORETICAL CROSS SECTION, POLARIZATION ONLY
35 CALL SKIP
WRITE(6,140)
140 FORMAT(1HJ,9X,5HTHETA,19X,7HSIGMATH,18X,8HSIG/SIGC,18X,6HPOL TH)
DO 38 J=1,JMAX
38 WRITE(6,150) THETA(J), SGMATH(J), SRATIO(J), POLTH(J)
150 FORMAT(1HJ,1PG20.7,4G25.7)
41 IF(KTRL(6).EQ.1)GO TO 121
IF(KTRL(6).NE.2)GO TO 48
C.....OUTPUT SCATTERING AMPLITUDES A,B
CALL SKIP
WRITE(6,160)
160 FORMAT(1HJ,11X,2HAR,23X,2HAI,23X,2HBR,23X,2HBI)
DO 43 J=1,JMAX
43 WRITE(6,150) AR(J), AI(J), BR(J), BI(J)
48 IF(KTRL(12).NE.1)GO TO 53
C.....OUTPUT AND PLOT FORM FACTORS
CALL SKIP
WRITE(6,170)
170 FORMAT(1HJ,9X,6HKKHU(1),15X,4HFFCR,16X,4HFFCI,16X,4HFFSR,16X,4HFFSI
1)
DO 51 I=1,ILAST
51 WRITE(6,180) RHU(1), FFCR(1), FFCI(1), FFSR(1), FFSI(1)

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18C FORMAT(1HJ,1P6G20.7)	11--1360
CALL PIFFRI	11--1370
53 IF(KTRL(2).NE.1)GO TO 61	11--1380
C.....OUTPUT CHISQ AND ERRORS FOR SIGMA AND POLARIZATION	11--1390
CALL SKIP	11--1400
WRITE(6,190)	11--1410
190 FORMAT(1HJ, 9X,5HTHETA,13X,9HDSIGMA EX,13X,7HDPOL EX, 8X,	11--1420
116HCHI SQUARE SIGMA,5X,14HCHI SQUARE POL,5X,16HCHI SQUARE TOTAL)	11--1430
DO 58 J=1,JMAX	11--1440
58 WRITE(6,180) THETAD(J), DSGMEX(J), DPOLEX(J), CHI2S(J), CHI2P(J),	11--1450
ICHI2(J)	11--1460
C.....OUTPUT REAL AND IMAG PARTS OF C-COEFFICIENTS	11--1470
61 CALL SKIP	11--1480
WRITE(6,200)	11--1490
200 FORMAT(1HJ,11X,1HL,14X,13HREAL C(L+1/2),12X,13HIMAG C(L+1/2),12X,	11--1500
113HREAL C(L-1/2),12X,13HIMAG C(L-1/2))	11--1510
DO 63 L=1,LMAX	11--1520
L1=L-1	11--1530
63 WRITE(6,210) L1, CR1(L), CI1(L), CR2(L), CI2(L)	11--1540
210 FORMAT(1HJ,111,1P630.7,3G25.7)	11--1550
C.....COMPUTE AND OUTPUT SCATTERING PHASE SHIFTS	11--1560
CALL SKIP	11--1570
WRITE (6,1399)	11--1580
DO 400 L=1,LMAX	11--1590
L1=L-1	11--1600
AETA1(L)=2.0*SQRT(CR1(L)**2+(.5-CI1(L))**2)	11--1610
AETA2(L)=2.0*SQRT(CR2(L)**2+(.5-CI2(L))**2)	11--1620
DELPI(L)=-.5*ALOG(AETA1(L))	11--1630
DELM1(L)=-.5*ALOG(AETA2(L))	11--1640
TEM=CI1(L)-.5	11--1650
IF(CR1(L)) 402,401,401	11--1660
401 IF(TEM) 403,403,404	11--1670
403 DELR1(L)=.5*ATAN(-CR1(L)/TEM)	11--1680
GO TO 410	11--1690
404 DELR1(L)=.5*(3.1415927 + ATAN(-CR1(L)/TEM))	11--1700
GO TO 410	11--1710
402 IF(TEM) 405,405,406	11--1720
405 DELR1(L)=3.1415927+.5*ATAN(-CR1(L)/TEM)	11--1730
GO TO 410	11--1740
406 DELR1(L)=.5*(3.1415927+ATAN(-CR1(L)/TEM))	11--1750
410 TEM=CI2(L)-.5	11--1760
IF(CR2(L))1402,1401,1401	11--1770
1401 IF(TEM) 1403,1403,1404	11--1780
1403 DELR2(L)=.5*ATAN(-CR2(L)/TEM)	11--1790
GO TO 1410	11--1800
1404 DELR2(L)=.5*(3.1415927+ATAN(-CR2(L)/TEM))	11--1810
GO TO 1410	11--1820
1402 IF(TEM) 1405,1405,1406	11--1830
1405 DELR2(L)=3.1415927+.5*ATAN(-CR2(L)/TEM)	11--1840
GO TO 1410	11--1850
1406 DELR2(L)=.5*(3.1415927+ATAN(-CR2(L)/TEM))	11--1860
1410 WRITE (6,1400)L1, AETA1(L),AETA2(L),DELRI(L),	11--1870
IDELPI(L),DELR2(L),DELM1(L)	11--1880
400 CONTINUE	11--1890
IF(KTRLX(2)-2)121,1415,121	11--1900
1415 WRITE(6,1420)	11--1910
1420 FORMAT(1HL)	11--1920
1425 WRITE(6,1430) (DELR1(I),DELPI(I),DELR2(I),DELM1(I),I=1,LMAX)	11--1930
1430 FORMAT(2H* 8F10.5)	11--1940
1399 FORMAT(5H L, 9X,4HETA1,16X,4HETA2,13X,11HDELR1-DELP1,11X,	11--1950
15HDELP1,13X,11HDELR2-DELM1,11X,5HDELM1)	11--1960
1400 FORMAT(15,1P6G20.7)	11--1970

121 RETURN
END

11--1980
11--1990

\$IBFTC PGEN	LOST,DECK	12--0010
	SUBROUTINE PGEN4	12--0020
C.....	VARIABLES USED FOR KNEE AND TAIL VARIATIONS	12--0030
	COMMON/SCNFF/TH(2), TN1(2), TN2(2), TRM(2),PMA, PMB	12--0040
C.....	SCATLE PARAMETERS	12--0050
	COMMON/PAKA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	12--0060
C.....	SCATLE CONTROLS	12--0070
	COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	12--0080
C.....	OTHER SCATLE VARIABLES	12--0090
	COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOB, RHOB2, RHOB3, SIGMA0, SIGMA1, TEMP	12--0100
C.....	VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS)	12--0120
	COMMON/PGU/FLPT,UCRB(250), UCIB(250), UCRM(250), UCIM(250),	12--0130
	USRB(250), USIB(250), USRM(250), USIM(250)	12--0140
C.....	VARIABLES COMPUTED IN PGEN4 (FORM FACTORS)	12--0150
	COMMON/PGF/FFC1(250), FFC1M(250), FFCR(250), FFCRM(250), FFSI(250)	12--0160
	IF, FFSIM(250), FFSR(250), FFSRM(250)	12--0170
C.....	VARIABLES COMPUTED IN RHUTB	12--0180
	COMMON/RHT/DRHOL, DRHU(249), IFIRST, ILAST, RHO(250), RHOMAX	12--0190
C.....	MM=1 DURING CALCULATIONS AT THE BEGINNINGS OF INTEGRATION INTERVAL	12--0200
C.....	MM=2 DURING CALCULATIONS AT THE MIDPOINTS OF INTEGRATION INTERVALS	12--0210
C.....	MM=3 DURING PUTICH CALCULATIONS	12--0220
	MM=1	12--0230
1	T1= V/ECM	12--0240
	T2= W/ECM	12--0250
	T3= 2.*FKAY/A	12--0260
	T10=-VS/ECM	12--0270
	T11=-WS/ECM	12--0280
	T4= T3*T10	12--0290
	T5 = T3*T11	12--0300
	T6 = FKAYA	12--0310
	IF(ABS(T6).LT.1.E-10) T6= SIGN(1.E-10,T6)	12--0320
	T7 = ETA/RHOB	12--0330
	T8 = RHOB**2	12--0340
	T9 = 2.*ETA	12--0350
	T12 = FKAYB	12--0360
	IF(ABS(T12).LT.1.E-10) T12= SIGN(1.E-10,T12)	12--0370
	IF(KNTV.NE.0) TEMX=TFI(A)	12--0380
	TTWV=DUMMY(1)	12--0390
	IF(KTRL(1).NE.1.OR.KTRLX(1).LT.2)TTWV=0.	12--0400
	KDCI=0	12--0410
	UCIX=0.	12--0420
	FFCIX=C.	12--0430
	IF(W.EQ.0..AND.TTWV.EQ.0.)KDCI=1	12--0440
	IF(KTRLX(7).NE.2) GO TO 2	12--0450
	RHUBKL = TEMP*DUMMY(3)	12--0460
	T26 = FKAY*DUMMY(2)	12--0470
	IF(ABS(T26).LT.1.E-10) T26=SIGN(1.E-10,T26)	12--0480
2	CONTINUE	12--0490
	IF(MM.EQ.3)GO TO 4	12--0500
C.....	SET UP LOOP ON I	12--0510
	I=0	12--0520
3	I=I+1	12--0530
	RHUX = RHU(I)	12--0540

4 TEMX= (RHUX-RHOBX)/T6	12--0550
TEMX= AMIN1(TEMX,80.)	12--0560
EX= EXP(TEMX)	12--0570
IF(KTRL(1).NE.2) GO TO 7	12--0580
S1= 0.	12--0590
IF(RHUX.LT.RHOBX) S1=1.	12--0600
GO TO 6	12--0610
7 S1 = 1./(1.+EX)	12--0620
8 S2 = EX*S1**2	12--0630
IF(RHUX.GT.RHOBX) GO TO 9	12--0640
S3 = T/(3.-RHUX**2/T8)	12--0650
GO TO 11	12--0660
9 S3 = T9/RHUX	12--0670
11 S4 = S2/RHUX	12--0680
C.....COMPUTE FFCRX AND UCRX	12--0690
IF(KTRL(7).NE.0) GO TO 33	12--0700
IF(KTRLX(7).EQ.2) GO TO 19	12--0710
FFCRX= S1	12--0720
GO TO 58	12--0730
19 TEMX = (RHUX-RHOBRL)/T26	12--0740
TEMX = AMIN1(TEMX,80.)	12--0750
FFCRX= 1./(1.+EXP(TEMX))	12--0760
GO TO 58	12--0770
33 FFCRX = TF(1,KTRL(7),RHUX)	12--0780
58 TCRX=T1*FFCRX	12--0790
UCRX=-1.-TCRX+S3	12--0800
C.....COMPUTE FFCIX AND UCIX	12--0810
IF(KTRL(8).NE.0) GO TO 83	12--0820
IF(KDC1.EQ.1)GO TO 88	12--0830
IF(KTRL(1).NE.1) GO TO 75	12--0840
TEM1= (RHUX-RHOBNG)/T12	12--0850
TEM1= AMIN1(TEM1,55.)	12--0860
IF(KTRLX(1).EQ.1.OR.KTRLX(1).EQ.3) GO TO 63	12--0870
S1= EXP(-TEM1**2)	12--0880
IF(KTRLX(1).EQ.0) GO TO 75	12--0890
S1V= 1./(1.+EXP(TEM1/.69))	12--0900
GO TO 75	12--0910
63 EX1 = EXP(TEM1)	12--0920
S1 =(4./(1.+EX1))*(EX1/(1.+EX1))	12--0930
IF(KTRLX(1).EQ.1)GO TO 75	12--0940
S1V = 1./(1.+EX1)	12--0950
75 UCIX = -T2*S1-S1V*TTWV/ECM	12--0960
FFCIX=(S1*w+S1V*TTWV)/(w+TTWV)	12--0970
GO TO 88	12--0980
83 FFCIX= TF(1,KTRL(8),RHUX)	12--0990
UCIX=-T2*FFCIX	12--1000
88 TCIX=-UCIX	12--1010
C.....COMPUTE FFSRX AND USRX	12--1020
IF(KTRL(9).NE.0)GO TO 93	12--1030
FFSRX = S4	12--1040
USRX=T4*FFSRX	12--1050
GO TO 98	12--1060
93 FFSRX= TF(2,KTRL(9),RHUX)	12--1070
CN1 = .5	12--1080
IF(ITQ.EQ.2) CN1 = FKAYA	12--1090
USRX = CN1*T4*FFSRX	12--1100
98 TSRX=LSRX	12--1110
IF(KTRL(11).EQ.0) GO TO 108	12--1120
T30 = .004927*ETA*ECM	12--1130
RHUY= AMAX1(RHUX,RHOBLC)	12--1140
USRX=LSRX+T30/RHUY**3	12--1150

C.....COMPUTE FFSIX AND USIX	12--1160
108 IF(KTRL(10).NE.0) GO TO 113	12--1170
FFSIX = 54	12--1180
USIX=T5*FFSIX	12--1190
GO TO 113	12--1200
113 FFSIX = TF(2,KTRL(10),RHUX)	12--1210
CN1 = .5	12--1220
IF(17Q.EQ.2) CN1=FKAYA	12--1230
USIX = CN1*T5*FFSIX	12--1240
118 TSIX=USIX	12--1250
GO TO (123,133,195),MM	12--1260
123 FFCR(I)= FFCRX	12--1270
UCRB(I)= UCRX	12--1280
FFCI(I)= FFCIX	12--1290
UCIB(I)= UCIX	12--1300
FFSR(I)= FFSRX	12--1310
USRB(I)= USRX	12--1320
FFSI(I)= FFSIX	12--1330
USIB(I)= USIX	12--1340
IF(1.EQ.1LAST)GO TO 175	12--1350
MM=2	12--1360
RHUX = RHUX+.5*DRHU(1)	12--1370
GO TO 4	12--1380
133 FFCRM(I)= FFCRX	12--1390
UCRM(I)= UCRX	12--1400
FFCIM(I)= FFCIX	12--1410
UCIM(I)= UCIX	12--1420
FFSRM(I)= FFSRX	12--1430
USRM(I)= USRX	12--1440
FFSIM(I)= FFSIX	12--1450
USIM(I)= USIX	12--1460
MM=1	12--1470
GO TO 3	12--1480
175 RETURN	12--1490
C.....ENTRY FOR PUTICH CALCULATIONS	12--1500
ENTRY PGNCK(RHOT,TCR,TCI,TSR,TSI)	12--1510
RHUX=RHUT	12--1520
MM=3	12--1530
GO TO 1	12--1540
195 TCR=TCRX	12--1550
TCI=TCIX	12--1560
TSR=TSRX	12--1570
TSI=TSIX	12--1580
GO TO 175	12--1590
C.....ENTRY TO INITIALIZE PGEN4	12--1600
ENTRY PGNIN	12--1610
KNTV=KTRL(7)+KTRL(8)+KTRL(9)+KTRL(10)	12--1620
IF(KNTV.NE.0)READ(5,200)TH, TN1, TN2, PMA, PMB	12--1630
200 FORMAT(8E10.0)	12--1640
GO TO 175	12--1650
C.....ENTRY FOR TFX INITIAL OUTPUT	12--1660
ENTRY PGNOU	12--1670
IF(KNTV.NE.0)WRITE(6,250) TH(1), TRM(1), TN1(1), TN2(1), PMA,	12--1680
1TH(2), TRM(2), TN1(2), TN2(2), PMB	12--1690
250 FORMAT(7HL HA=E16.9,7H RMA=E16.9,7H N1A=E16.9,7H N2A=E16.9	12--1700
1,7H PMA=E16.9/7H HB=E16.9,7H RMB=E16.9,7H N1B=E16.9,7H	12--1710
2N2B=E16.9,7H PMB=E16.9)	12--1720
GO TO 175	12--1730
END	12--1740

\$IBFTC TFX	LOST,DECK	13--0010
	FUNCTION TF(JTQ,KOD,RHOX)	13--0020
C.....	SPECIAL CENTRAL NUCLEAR FORM FACTOR	13--0030
C.....	VARIABLES USED FOR KNEE AND TAIL VARIATIONS	13--0040
	COMMON/SCNFF/TH(2), TN1(2), TN2(2), TRM(2),PMA, PMB	13--0050
C.....	OTHER SCATLE VARIABLES	13--0060
	COMMON/MI SC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHUBC, RHUBN,	13--0070
	IRHUBNG, SIGMA0, SIGMA1, TEMP	13--0080
C.....	SCATLE PARAMETERS	13--0090
	COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	13--0100
	ITQ=JTQ	13--0110
	GO TO (3,6),ITQ	13--0120
3	IX=2	13--0130
	IF(KOD.EQ.1) IX=1	13--0140
	GO TO 5	13--0150
6	IX=1	13--0160
	IF(KOD.LE.1)GO TO 9	13--0170
	ITQ=1	13--0180
	IX=2	13--0190
9	TIN= TN1(IX)	13--0200
	IF(RHOX.GT.RHUBN) TIN= TN2(IX)	13--0210
	T20= RHOX/RHUBN	13--0220
	TF=0.	13--0230
	IF(TIN*ALOG(T20).GT.80.) GO TO 35	13--0240
	TEM= TIN*FKAY*A	13--0250
	IF(TEM.NE.0.) GO TO 12	13--0260
	TG = T20** (RHUBN/FKAY*A)	13--0270
	GO TO 18	13--0280
12	TQ=(T20**TIN-1.)*RHUBN/TEM	13--0290
	IF(TQ.GT.80.) GO TO 35	13--0300
	TG = EXP(TQ)	13--0310
18	TF= 1./(1.+TG)	13--0320
	IF(RHOX.GT.TRM(IX))GO TO (35,28),ITQ	13--0330
	T21= RHOX/TRM(IX)	13--0340
	THH = TH(IX)*(1.+2.*T21)*(1.-T21)**2	13--0350
	IF(ITQ.EQ.2) GO TO 28	13--0360
	TF = TF*(1.+THH)	13--0370
	GO TO 35	13--0380
28	TEN = TF	13--0390
	TF= RHUBN*T20**TIN*TG*(TEN/RHOX)**2/(FKAY*A)	13--0400
	IF(RHOX.GT.TRM(IX))GO TO 35	13--0410
	T24= 6.*TH(IX)*(1.-T21)/TRM(IX)**2	13--0420
	TF = T24*TEN+ (1.+THH)*TF	13--0430
35	RETURN	13--0440
	ENTRY TF(DUM)	13--0450
	TRM(1)=PMA*RHUBN	13--0460
	TRM(2)=PMB*RHUBN	13--0470
	TF=DUM	13--0480
	GO TO 35	13--0490
	END	13--0500

\$IBFTC INTCTR	LOST,DECK	14--0010
	SUBROUTINE INTCTR(*)	14--0020
C.....	RADIAL WAVE FUNCTIONS AND THEIR FIRST DERIVATIVES DURING INTEGRATI	14--0030
	COMMON/RWF/L, XC1, XCP1, XD1, XDP1, YC1, YCP1, YD1, YDP1	14--0040
C.....	FINAL RADIAL WAVE FUNCTIONS AND FIRST DERIVATIVES	14--0050
	COMMON/RWFF/X1(51), X1P(51), X2(51), X2P(51), Y1(51), Y1P(51),	14--0060
	Y2(51), Y2P(51)	14--0070

C.....SCATLE PARAMETERS	14--0080
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	14--0090
COMMON/LIND/LMAX, LMAXM	14--0100
C.....VARIABLES COMPUTED IN RHUTB	14--0110
COMMON/RHT/DRHUL, DRHU(249), IFIRST, ILAST, RHO(250), RHOMAX	14--0120
C.....SCATLE CONTROLS	14--0130
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	14--0140
C.....CONTROL INTEGRATION OF RADIAL EQUATIONS	14--0150
IFIRST=1	14--0160
IDX=1	14--0170
C.....KTRLX(6)=1 FOR EXCHANGE FORM IN SPIN-ORBIT POTENTIAL	14--0180
IF(KTRLX(6).EQ.1)IDX=2	14--0190
DO 2 KK=1,IDX	14--0200
DO 1 L=KK,LMAX,IDX	14--0210
TEM=RHO(IFIRST)**(L-1)	14--0220
XC1=TEM*RHO(IFIRST)	14--0230
XD1=XC1	14--0240
FL=L	14--0250
XCP1=FL*TEM	14--0260
XDP1=XCP1	14--0270
YC1=0.0	14--0280
YD1=0.0	14--0290
YCP1=0.0	14--0300
YDP1=0.0	14--0310
CALL RKINT	14--0320
X1(L)=XC1	14--0330
X2(L)=XD1	14--0340
Y1(L)=YC1	14--0350
Y2(L)=YD1	14--0360
X1P(L)=XCP1	14--0370
X2P(L)=XDP1	14--0380
Y1P(L)=YCP1	14--0390
1 Y2P(L)=YDP1	14--0400
IF(IDX.EQ.1)GO TO 2	14--0410
IF(KK.EQ.2)GO TO 2	14--0420
VSSAV=VS	14--0430
VS=DUMMY(4)	14--0440
CALL POTICH(15)	14--0450
C.....GENERATE POTENTIAL FOR EXCHANGE TERM	14--0460
CALL PGEN4	14--0470
2 CONTINUE	14--0480
IF(IDX.EQ.2)VS=VSSAV	14--0490
RETURN	14--0500
15 RETURN 1	14--0510
END	14--0520

\$IBFTC RKINT LOST,DECK	15--0010
SUBROUTINE RKINT	15--0020
C.....SCATLE CONTROLS	15--0030
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	15--0040
C.....RADIAL WAVE FUNCTIONS AND THEIR FIRST DERIVATIVES DURING INTEGRATION	15--0050
COMMON/RWF/L, XC1, XCP1, XD1, XDP1, YC1, YCP1, YD1, YDP1	15--0060
C.....SCATLE PARAMETERS	15--0070
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	15--0080
C.....VARIABLES COMPUTED IN RHUTB	15--0090
COMMON/RHT/DRHUL, DRHU(249), IFIRST, ILAST, RHO(250), RHOMAX	15--0100
C.....VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS)	15--0110
COMMON/PGU/FLPT,UCRB(250), UCIB(250), UCRM(250), UCIM(250),	15--0120
IUSR(250), USIB(250), USRM(250), USIM(250)	15--0130

1	FL=L-1	15--0140
	F2L=-1.0-FL	15--0150
	F3L=FL*(FL+1.0)	15--0160
	TB=UCRB(1FIRST)+F3L/(RHU(1FIRST)**2)	15--0170
C.....	IF VS=WS=0, OMIT REDUNDANT INTEGRATION STEPS	15--0180
	IF(KTRL(11).NE.C)GO TO 13	15--0190
	IF(VS.EQ.0..AND.WS.EQ.0.)GO TO 413	15--0200
13	PCB=TB+USRB(1FIRST)*FL	15--0210
	PDB=TB+USRB(1FIRST)*F2L	15--0220
	QCB=UC1B(1FIRST)+US1B(1FIRST)*FL	15--0230
	QDB=UC1B(1FIRST)+US1B(1FIRST)*F2L	15--0240
	IK=1LAST-1	15--0250
	DO 6 I=1FIRST,IK	15--0260
2	HDRHU=.5*DRHU(I)	15--0270
	DRHU2=(DRHU(I)**2)*.5	15--0280
	RHUM=RHO(I)+HDRHU	15--0290
	TM=UCRM(I)+F3L/(RHOM**2)	15--0300
15	PCM=TM+USKM(1)*FL	15--0310
	PDM=TM+USRM(1)*F2L	15--0320
	QCM=UC1M(1)+US1M(1)*FL	15--0330
	QDM=UC1M(1)+US1M(1)*F2L	15--0340
	XCPP1=PCB*XC1-QCB*YC1	15--0350
	YCPP1=QCB*XC1+PCB*YC1	15--0360
	XOPP1=PDB*XU1-QDB*YU1	15--0370
	YOPP1=QDB*XU1+PDB*YU1	15--0380
	XC2=XC1+XCPP1*HDRHU	15--0390
	YC2=YC1+YCPP1*HDRHU	15--0400
	XU2=XU1+XOPP1*HDRHU	15--0410
	YU2=YU1+YOPP1*HDRHU	15--0420
	XCPP2=PCM*XC2-QCM*YC2	15--0430
	YCPP2=QCM*XC2+PCM*YC2	15--0440
	XOPP2=PDM*XU2-QDM*YU2	15--0450
	YOPP2=QDM*XU2+PDM*YU2	15--0460
	DRHU4=.5*DRHU2	15--0470
	SDRHU=.33333333*HDRHU	15--0480
	XC3=XC2+XCPP1*DRHU4	15--0490
	YC3=YC2+YCPP1*DRHU4	15--0500
	XU3=XU2+XOPP1*DRHU4	15--0510
	YU3=YU2+YOPP1*DRHU4	15--0520
	XCPP3=PCM*XC3-QCM*YC3	15--0530
	YCPP3=QCM*XC3+PCM*YC3	15--0540
	XOPP3=PDM*XU3-QDM*YU3	15--0550
	YOPP3=QDM*XU3+PDM*YU3	15--0560
	XC4=XC2+XCPP2*DRHU2+XCPP1*HDRHU	15--0570
	YC4=YC2+YCPP2*DRHU2+YCPP1*HDRHU	15--0580
	XU4=XU2+XOPP2*DRHU2+XOPP1*HDRHU	15--0590
	YU4=YU2+YOPP2*DRHU2+YOPP1*HDRHU	15--0600
	TB=UCRB(1+1)+F3L/(RHU(1+1)**2)	15--0610
17	PCB=TB+USRB(1+1)*FL	15--0620
	PDB=TB+USRB(1+1)*F2L	15--0630
	QCB=UC1B(1+1)+US1B(1+1)*FL	15--0640
	QDB=UC1B(1+1)+US1B(1+1)*F2L	15--0650
	XCPP4=PCB*XC4-QCB*YC4	15--0660
	YCPP4=QCB*XC4+PCB*YC4	15--0670
	XOPP4=PDB*XU4-QDB*YU4	15--0680
	YOPP4=QDB*XU4+PDB*YU4	15--0690
	SXC=XCPP2+XCPP3	15--0700
	SYC=YCPP2+YCPP3	15--0710
	SXD=XOPP2+XOPP3	15--0720
	SYU=YOPP2+YOPP3	15--0730
	TXC=SXC+XCPP1	15--0740
	TYC=SYC+YCPP1	15--0750

TXD=SD+XDPP1	15--0760
TYD=SYD+YDPP1	15--0770
TXC1=XC1+DRHU(1)*(XCP1+SDRHU*TXC)	15--0780
TYC1=YC1+DRHU(1)*(YCP1+SDRHU*TYC)	15--0790
TXD1=XD1+DRHU(1)*(XDP1+SDRHU*TXD)	15--0800
TYD1=YD1+DRHU(1)*(YDP1+SDRHU*TYD)	15--0810
TXCP1=XCP1+SDRHU*(TXC+SXC+XCPP4)	15--0820
TYCP1=YCP1+SDRHU*(TYC+SYC+YCPP4)	15--0830
TXDP1=XDP1+SDRHU*(TXD+SXD+XDPP4)	15--0840
TYDP1=YDP1+SDRHU*(TYD+SYD+YDPP4)	15--0850
TEM=AMAX1(ABS(XC1),ABS(YC1),ABS(XCP1),ABS(YCP1),	15--0860
1ABS(XD1),ABS(YD1),ABS(XDP1),ABS(YDP1))	15--0870
IF(TEM-1.E+30)21,21,316	15--0880
316 RENORM=TEM	15--0890
320 XC1=XC1/RENORM	15--0900
YC1=YC1/RENORM	15--0910
XCP1=XCP1/RENORM	15--0920
YCP1=YCP1/RENORM	15--0930
XD1=XD1/RENORM	15--0940
YD1=YD1/RENORM	15--0950
XDP1=XDP1/RENORM	15--0960
YDP1=YDP1/RENORM	15--0970
WRITE(6,200)RENORM,L,RHU(1)	15--0980
200 FORMAT(24H RENORMALIZATION FACTOR=E16.9,22H IN RKINT FOR CODED L=I	15--0990
13,9H AND RHU=E16.9)	15--1000
JSPILL=0	15--1010
GO TU2	15--1020
21 XC1=TXC1	15--1030
YC1=TYC1	15--1040
XD1=TXD1	15--1050
YD1=TYD1	15--1060
XCP1=TXCP1	15--1070
YCP1=TYCP1	15--1080
XDP1=TXDP1	15--1090
YDP1=TYDP1	15--1100
6 CONTINUE	15--1110
4 RETURN	15--1120
C.....INTEGRATION STEPS FOR VS=WS=0, OMTS REDUNDANT EQUATIONS	15--1130
413 PCB=TB	15--1140
QCB=UC1B(1FIRST)	15--1150
IK=ILAST-1	15--1160
DO 46 I=1FIRST,IK	15--1170
42 HDRHU=.5*DRHU(1)	15--1180
DRHU2=(DRHU(1)**2)*.5	15--1190
RHUM=RHU(1)+HDRHU	15--1200
TM=UCRM(1)+F3L/(RHUM**2)	15--1210
415 PCM=FM	15--1220
QCM=UCIM(1)	15--1230
XCPP1=PCB*XC1-QCB*YC1	15--1240
YCPP1=QCB*XC1+PCB*YC1	15--1250
XC2=XC1+XCP1*HDRHU	15--1260
YC2=YC1+YCP1*HDRHU	15--1270
XCPP2=PCM*XC2-QCM*YC2	15--1280
YCPP2=QCM*XC2+PCM*YC2	15--1290
DRHU4=.5*DRHU2	15--1300
SDRHU=.33333333*HDRHU	15--1310
XC3=XC2+XCPP1*SDRHU4	15--1320
YC3=YC2+YCPP1*SDRHU4	15--1330
XCPP3=PCM*XC3-QCM*YC3	15--1340
YCPP3=QCM*XC3+PCM*YC3	15--1350
XC4=XC2+XCPP2*DRHU2+XCP1*HDRHU	15--1360
YC4=YC2+YCPP2*DRHU2+YCP1*HDRHU	15--1370
TB=UCRB(I+1)+F3L/(RHU(I+1)**2)	15--1380

417	PCB=TB	15--1390
	QCB=UC IB(I+1)	15--1400
	XC PP4=PCB*XC4-QCB*YC4	15--1410
	YCPP4=QCB*XC4+PCB*YC4	15--1420
	SXL=XC PP2+XC PP3	15--1430
	SYC=YCPP2+YCPP3	15--1440
	TXC=SXC+XC PP1	15--1450
	TYC=SYC+YCPP1	15--1460
	TXC1=XC1+DRHO(I)*(XC P1+SDRHO*TXC)	15--1470
	TYC1=YC1+DRHO(I)*(YC P1+SDRHO*TYC)	15--1480
	TXCP1=XC P1+SDRHO*(TXC+SXC+XC PP4)	15--1490
	TYCP1=YC P1+SDRHO*(TYC+SYC+YCPP4)	15--1500
	TEM=AMAX1(ABS(XC1),ABS(YC1),ABS(XC P1),ABS(YC P1))	15--1510
	IF(TEM-1.E+30)421,421,4316	15--1520
4316	RENORM=TEM	15--1530
4320	XC1=XC1/RENORM	15--1540
	YC1=YC1/RENORM	15--1550
	XC P1=XC P1/RENORM	15--1560
	YC P1=YC P1/RENORM	15--1570
	WRITE (6,4200)RENORM,L,RHO(I)	15--1580
4200	FORMAT(24H RENORMALIZATION FACTOR=E16.9,22H IN RKINT FOR CODED L=I	15--1590
	13,9H AND RHO=E16.9)	15--1600
	GO TO 42	15--1610
421	XC1=TXC1	15--1620
	YC1=TYC1	15--1630
	XD1=XC1	15--1640
	YD1=YC1	15--1650
	XC P1=TXCP1	15--1660
	YC P1=TYCP1	15--1670
	XD P1=XC P1	15--1680
	YD P1=YC P1	15--1690
46	CUNTINUE	15--1700
44	RETURN	15--1710
	END	15--1720

\$IBFTC	CSUBL	16--0010
	SUBROUTINE CSUBL	16--0020
C.....	FINAL RADIAL WAVE FUNCTIONS AND FIRST DERIVATIVES	16--0030
	COMMON/RWFF/X1(51), X1P(51), X2(51), X2P(51), Y1(51), Y1P(51),	16--0040
	Y2(51), Y2P(51)	16--0050
	COMMON/LIND/LMAX, LMAXM	16--0060
C.....	VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L	16--0070
	COMMON/VARL/G11(51), G12(51), CR1(51), CR2(51), EXSGM1(51),	16--0080
	LEXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)	16--0090
C.....	COMPUTE C-COEFFICIENTS	16--0100
	DO 40 L=1,LMAX	16--0110
	XNORM1=AMAX1(ABS(X1(L)),ABS(Y1(L)),ABS(X1P(L)),ABS(Y1P(L)))	16--0120
	TX1L=X1(L)/XNORM1	16--0130
	TY1L=Y1(L)/XNORM1	16--0140
	TX1PL=X1P(L)/XNORM1	16--0150
	TY1PL=Y1P(L)/XNORM1	16--0160
	FNORM=AMAX1(F(L),G(L),FP(L),GP(L))	16--0170
	TFL=F(L)/FNORM	16--0180
	TGL=G(L)/FNORM	16--0190
	TFPL=FP(L)/FNORM	16--0200
	TGPL=GP(L)/FNORM	16--0210
	CO1=TFL*TY1PL-TFPL*TY1L	16--0220
	CO2=TFPL*TX1L-TFL*TX1PL	16--0230

	CO3=TY1L*TGPL-TY1PL*TGL+TX1L*TFPL-TX1PL*TFL	16--0240
	CO4=TX1PL*TGL-TX1L*TGPL+TY1L*TFPL-TY1PL*TFL	16--0250
	CO7=1.C/(CO3**2+CO4**2)	16--0260
53	CR1(L)=(CO1*CO3+CO2*CO4)*CO7	16--0270
	CI1(L)=(CO2*CO3-CO1*CO4)*CO7	16--0280
	XNORM2=AMAX1(ABS(X2(L)),ABS(Y2(L)),ABS(X2P(L)),ABS(Y2P(L)))	16--0290
	TX2L=X2(L)/XNORM2	16--0300
	TY2L=Y2(L)/XNORM2	16--0310
	TX2PL=X2P(L)/XNORM2	16--0320
	TY2PL=Y2P(L)/XNORM2	16--0330
	CO1=TFPL*TY2PL-TFPL*TY2L	16--0340
	CO2=TFPL*TX2L-TFL*TX2PL	16--0350
	CO3=TY2L*TGPL-TY2PL*TGL+TX2L*TFPL-TX2PL*TFL	16--0360
	CO4=TX2PL*TGL-TX2L*TGPL+TY2L*TFPL-TY2PL*TFL	16--0370
	CO7=1.C/(CO3**2+CO4**2)	16--0380
55	CR2(L)=(CO1*CO3+CO2*CO4)*CO7	16--0390
40	CI2(L)=(CO2*CO3-CO1*CO4)*CO7	16--0400
59	RETURN	16--0410
	END	16--0420
\$IBFTC AB	LOST,DECK	17--0010
	SUBROUTINE AB	17--0020
C.....	SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA	17--0030
	COMMON/TH1/DPULEX(150), DSGMEX(150), JMAX, PULEX(150), POLTH(150),	17--0040
	ISGMAEX(150), SGMAH(150), THETA(150), THETAU(150)	17--0050
	COMMON/LIND/LMAX, LMAXM	17--0060
C.....	VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L	17--0070
	COMMON/VARL/CI1(51), CI2(51), CR1(51), CR2(51), EXSGMI(51),	17--0080
	LEXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)	17--0090
C.....	OTHER SCATLE VARIABLES	17--0100
	COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHOBN,	17--0110
	IRHUBNG, SIGMAO, SIGMA1, TEMP	17--0120
C.....	SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS	17--0130
	COMMON/SACS/AL(150), AR(150), BI(150), BR(150), FCI(150), FCR(150)	17--0140
	I,SGMAC(150), SIGTEM(150), SRATIO(150)	17--0150
	DIMENSION P(52),PP(51)	17--0160
C.....	COMPUTE SCATTERING AMPLITUDES A, B	17--0170
	FKAYD=1.0/FKAY	17--0180
4	DO 20 J=1,JMAX	17--0190
	ASUMR=C.0	17--0200
	ASUMI=C.0	17--0210
	BSUMR=C.0	17--0220
	BSUMI=C.0	17--0230
C.....	COMPUTES LEGENDRE POLYNOMIALS	17--0240
	SI2=1.C/SIN(THETA(J))	17--0250
	CU=COS(THETA(J))	17--0260
	P(1)=1.0	17--0270
	P(2)=CU	17--0280
	PP(1)=C.0	17--0290
	TWULP1=3.0	17--0300
	FL=1.0	17--0310
	DO 2008 L=1,LMAXM	17--0320
	TL=FL+1.0	17--0330
	P(L+2)=(TWULP1*CU*P(L+1)-FL*P(L))/TL	17--0340
	PP(L+1)=TL*SI2*(CU*P(L+1)-P(L+2))	17--0350
	TWULP1=TWULP1+2.0	17--0360
2008	FL=TL	17--0370
	DO 10 L=1,LMAX	17--0380

FL=L	17--0390
ATR1=FL*CR1(L)+(FL-1.0)*CR2(L)	17--0400
ATI1=FL*CI1(L)+(FL-1.0)*CI2(L)	17--0410
BTR1=CR1(L)-CR2(L)	17--0420
BTI1=CI1(L)-CI2(L)	17--0430
ATR2=ATR1*EXSGMR(L)-(ATI1*EXSGMI(L))	17--0440
ATI2=ATR1*EXSGMI(L)+(ATI1*EXSGMR(L))	17--0450
BTR2=BTR1*EXSGMR(L)-(BTI1*EXSGMI(L))	17--0460
BTI2=BTR1*EXSGMI(L)+(BTI1*EXSGMR(L))	17--0470
ASUMR=ASUMR+(ATR2*P(L))	17--0480
ASUMI=ASUMI+(ATI2*P(L))	17--0490
BSUMR=BSUMR+(BTR2*PP(L))	17--0500
10 BSUMI=BSUMI+(BTI2*PP(L))	17--0510
AR(J)= FCR(J)+(FKAYD*ASUMR)	17--0520
AI(J)=FCI(J)+(FKAYD*ASUMI)	17--0530
BR(J)= FKAYD*BSUMI	17--0540
20 BI(J)= -FKAYD*BSUMR	17--0550
33 RETURN	17--0560
END	17--0570

\$IBFTC SGSGCP LOST,DECK	18--0010
SUBROUTINE SGSGCP	18--0020
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS	18--0030
COMMON/SACS/AI(150), AR(150), BI(150), BR(150), FCI(150), FCR(150)	18--0040
1,SGMAC(150), SIGTEM(150), SRATIO(150)	18--0050
C.....OTHER SCATLE VARIABLES	18--0060
COMMON/MS/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOB, RHOB2, RHOB3,	18--0070
IRHUBG, SIGMA0, SIGMA1, TEMP	18--0080
C.....SCATLE CONTROLS	18--0090
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	18--0100
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA	18--0110
COMMON/TH1/DPULEX(150), DSGMEX(150), JMAX, PULEX(150), POLTH(150),	18--0120
1SGMAEX(150), SGMAH(150), THETA(150), THETAD(150)	18--0130
C.....COMPUTE CROSS SECTION, POLARIZATION, RATIO(SIGMA/SIGMA-COUL)	18--0140
DO 50 J=1,JMAX	18--0150
SGMATH(J) = AR(J)*AR(J)+AI(J)*AI(J) + BR(J)*BR(J)+BI(J)*BI(J)	18--0160
POLTH(J)= -(2.0*(AR(J)*BR(J)+AI(J)*BI(J)))/SGMATH(J)	18--0170
13 SGMAC(J) = FCR(J)*FCR(J) + FCI(J)*FCI(J)	18--0180
IF(ETA) 7,7,8	18--0190
8 SRATIO(J)=SGMATH(J)/SGMAC(J)	18--0200
15 GO TO 5	18--0210
7 SRATIO(J)=0.0	18--0220
5 IF(KTRLX(J))1,50,1	18--0230
1 IF(DSGMEX(J)-1.E+27)2,2,3	18--0240
2 SIGTEM(J)=SGMAC(J)	18--0250
GO TO 50	18--0260
3 SIGTEM(J)=DSGMEX(J)	18--0270
50 CONTINUE	18--0280
15 RETURN	18--0290
END	18--0300

\$IBFTC SIGMAR LOST,DECK	19--0010
SUBROUTINE SIGMAR	19--0020

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C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION          19--0030
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),                19--0040
ICH12P(150), CHI2(150), ENORM, SGMRTTH, SNORM, XNORM, NP, CSNRM, NCSN    19--0050
C.....VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L                  19--0060
COMMON/VARL/CI1(51), CI2(51), CR1(51), CR2(51), EXSGMI(51),           19--0070
IEXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)                    19--0080
COMMON/LIND/LMAX, LMAXM                                                19--0090
C.....OTHER SCATLE VARIABLES                                           19--0100
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOB, RHOBN,           19--0110
IRHUBNG, SIGMA0, SIGMA1, TEMP                                         19--0120
C.....COMPUTE REACTION CROSS SECTIONS                                  19--0130
FL=0.0                                                                  19--0140
SGMRTTH=0.0                                                            19--0150
CP1=(.125663/C6E+02)/(FKAY**2)                                       19--0160
DO 20 L=1,LMAX                                                         19--0170
SGMRTTH=SGMRTTH+FL*(CI2(L)-(CI2(L))**2-(CR2(L))**2)                  19--0180
FL=FL+1.0                                                              19--0190
20 SGMRTTH=SGMRTTH+FL*(CI1(L)-(CI1(L))**2-(CR1(L))**2)                19--0200
SGMRTTH=CP1*SGMRTTH                                                  19--0210
13 RETURN                                                              19--0220
END                                                                    19--0230

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$IBFTC CHISQ LUST,DECK                                                20--0010
SUBROUTINE CHISQ                                                       20--0020
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA    20--0030
COMMON/TH1/DPOLEX(150), DSGMEX(150), JMAX, POLEX(150), POLTH(150),    20--0040
ISGMAEX(150), SGMAETH(150), THETA(150), THETAD(150)                  20--0050
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION          20--0060
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),             20--0070
ICH12P(150), CHI2(150), ENORM, SGMRTTH, SNORM, XNORM, NP, CSNRM, NCSN 20--0080
C.....SCATLE CONTROLS                                                  20--0090
COMMON/CNTR/KULT, KSEND, KTRL(13), KTRLT(3), NF, NR, NI, IN1,         20--0100
IN2, IN3, IN4, IN5, IN6, KTRLX(13)                                    20--0110
C.....AUXILIARY SEARCH VARIABLES                                       20--0120
COMMON/ASV/DEL(12), ID(12), IIN, KOLMAX, LABEL(13), NHP, NMLR,       20--0130
INPCT, NPCTP, PCT                                                    20--0140
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS              20--0150
COMMON/SACS/AI(150), AR(150), BI(150), BR(150), FCI(150), FCR(150) 20--0160
1,SGMAC(150), SIGTEM(150), SRATIO(150)                                20--0170
DIMENSION CHIQS(19)                                                  20--0180
EQUIVALENCE                                                            20--0190
1(CHIQS(1),CHI2ST), (SUMS(1),SUM1S), (SUMS(2),SUM1P),                20--0200
2(SUMS(3),SUM2S), (SUMS(4),SUM2P), (SUMS(5),SUM3S), (SUMS(6),SUM3P), 20--0210
3(SUMS(7),SUM4S), (SUMS(8),SUM4P), (SUMS(9),SUMFS), (SUMS(10),SUMFP), 20--0220
4(SUMS(11),SUMMS), (SUMS(12),SUMMP), (SUMS(13),SUMRS),               20--0230
5(SUMS(14),SUMKP), (SUMS(15),SUM34S), (SUMS(16),SUM34P)              20--0240
ANUM=0.                                                                20--0250
DEN=0.                                                                20--0260
DO 20 J=1,JMAX                                                         20--0270
TEM=SGMAETH(J)/DSGMEX(J)                                              20--0280
ANUM=ANUM+TEM**2                                                       20--0290
20 DEN=DEN+TEM*SGMAEX(J)/DSGMEX(J)                                    20--0300
ENORM=ANUM/DEN                                                         20--0310
IF(KTRLX(5).EQ.2) SNORM=ENORM                                         20--0320
CHI2PT=0.                                                              20--0330
CHI2ST=0.                                                              20--0340
DO 28 J=1,JMAX                                                         20--0350
CHI2P(J)=((POLTH(J)-POLEX(J))/DPOLEX(J))**2                          20--0360
CHI2PT=CHI2PT+CHI2P(J)                                                20--0370

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CHI2S(J)=SGMATH(J)-SNORM*SGMAEX(J)	20--0380
CHI2S(J)=(CHI2S(J)/(SNORM*SIGTEM(J)))*2	20--0390
CHI2(J)=CHI2S(J)+CHI2P(J)	20--0400
28 CHI2ST=CHI2ST+CHI2S(J)	20--0410
CHI2T=CHI2ST+CHI2PT	20--0420
32 GO TO (19,26,26),KDLMAX	20--0430
26 DO 40 I=1,14	20--0440
40 SUMS(I)=0.0	20--0450
C.....CALCULATE SPECIAL CHI SQUARES	20--0460
IF(KDLMAX-3)1,16,1	20--0470
1 IF (N1) 2,3,2	20--0480
2 LIM = N1+IN1	20--0490
DO 101 J=N1,LIM	20--0500
SUM1S = SUM1S+CHI2S(J)	20--0510
101 SUM1P = SUM1P+CHI2P(J)	20--0520
3 IF (N2) 4,5,4	20--0530
4 LIM = N2+IN2	20--0540
DO 102 J=N2,LIM	20--0550
SUM2S = SUM2S+CHI2S(J)	20--0560
102 SUM2P=SUM2P+CHI2P(J)	20--0570
5 IF (N3) 6,7,6	20--0580
6 LIM = N3+IN3	20--0590
DO 103 J=N3,LIM	20--0600
SUM3S = SUM3S+CHI2S(J)	20--0610
103 SUM3P = SUM3P + CHI2P(J)	20--0620
7 IF(N4)14,15,14	20--0630
14 LIM = N4+IN4	20--0640
DO 104 J=N4,LIM	20--0650
SUM4S = SUM4S + CHI2S(J)	20--0660
104 SUM4P = SUM4P + CHI2P(J)	20--0670
15 SUM34S = SUM3S+SUM4S	20--0680
SUM34P = SUM3P+SUM4P	20--0690
16 DO 105 J=1,NF	20--0700
SUMFS = SUMFS+CHI2S(J)	20--0710
105 SUMFP=SUMFP+CHI2P(J)	20--0720
I = NF+1	20--0730
DO 106 J=1,NR	20--0740
SUMMS = SUMMS+CHI2S(J)	20--0750
106 SUMMP = SUMMP+CHI2P(J)	20--0760
I = NR+1	20--0770
DO 107 J=I,JMAX	20--0780
SUMRS = SUMRS+CHI2S(J)	20--0790
107 SUMRP=SUMRP+CHI2P(J)	20--0800
19 IF(KSEND.NE.2)GO TO 43	20--0810
C.....OUTPUT SCATLE PARAMETERS	20--0820
30 CALL POUT	20--0830
WRITE(6,60) ENORM,CHI2ST,CHI2PT,CHI2T	20--0840
60 FORMAT(1H+,26X,6HENORM=1PG14.7,4X,7HCHI2ST=G14.7,4X,7HCHI2PT=G14.720--0850	
1,5X,6HCHI2T=G14.7)	20--0860
CALL SOUF	20--0870
DO 38 KK=1, NC SN	20--0880
38 CHIQS(KK)=CHIQS(KK)/CSNRM	20--0890
WRITE(6,80) CSNRM, CHI2ST, CHI2PT, CHI2T	20--0900
80 FORMAT(1HK,10X,20HSUM OF CHI SQUARES /F5.0,15X,7HCHI2ST=G14.7,4X,720--0910	
1HCHI2PT=G14.7,5X,6HCHI2T=G14.7)	20--0920
CALL SOLF	20--0930
WRITE(6,70)	20--0940
70 FORMAT(1HK,10(2H-))	20--0950
43 RETURN	20--0960
END	20--0970

\$IBFTC PTFERR1 LOST,DECK	21--0010
SUBROUTINE PTFERR1	21--0020
C.....VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS)	21--0030
COMMON/PGU/FLPT,UCRB(250), UCIB(250), UCRM(250), UCIM(250),	21--0040
1,USRB(250), USIB(250), USRM(250), USIM(250)	21--0050
C.....VARIABLES COMPUTED IN PGEN4 (FORM FACTORS)	21--0060
COMMON/PGF/FFC1(250), FFCIM(250), FFCR(250), FFCRM(250), FFSI(250)	21--0070
1,FFSIM(250), FFSR(250), FFSRM(250)	21--0080
C.....VARIABLES COMPUTED IN RHOTB	21--0090
COMMON/RH1/DRHUL, DRHO(249), IFIRST, ILAST, RHO(250), RHOMAX	21--0100
C.....SCATLE PARAMETERS	21--0110
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	21--0120
C.....OTHER SCATLE VARIABLES	21--0130
COMMON/MS/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOB, RHOBX,	21--0140
IRHUBNG, SIGMAO, SIGMA1, TEMP	21--0150
C.....SCATLE CONTROLS	21--0160
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	21--0170
DIMENSION KK(14), PT(11), YPLUT(1000), XPLUT(1000)	21--0180
EQUIVALENCE (UCRB,XPLUT),(USRB,YPLUT)	21--0190
C.....PLOT FORM FACTORS	21--0200
C.....SET UP PLOT OF UCRB	21--0210
TESTA=1.50*V/ECM	21--0220
ANUM = FLPT*(FLPT + 1.)	21--0230
IF(FLPT) 7,6,7	21--0240
6 BN=8.	21--0250
CN=8.	21--0260
GO TO 5	21--0270
7 CN=0.	21--0280
8 CN=CN+1.	21--0290
DEN1=RHOBX-CN*FKAYA	21--0300
DEN1=DEN1*DEN1	21--0310
DEN2=RHOBX+CN*FKAYA	21--0320
DEN2=DEN2*DEN2	21--0330
TERM=ANUM/DEN1-ANUM/DEN2	21--0340
IF(TERM-TESTA) 8,8,19	21--0350
19 BN=AMIN1(8.,CN)	21--0360
9 TESTB=RHOBX+BN*FKAYA	21--0370
TESTC=RHOBX-CN*FKAYA	21--0380
KNT=0	21--0390
DO 2 I=1,ILAST	21--0400
IF(TESTC-RHO(I)) 1,1,2	21--0410
1 IF(RHO(I)-TESTB) 3,3,2	21--0420
3 TERM=ANUM/(RHO(I)*RHO(I))	21--0430
4 KNT=KNT+1	21--0440
UCRB(KNT)=UCRB(I)+TERM+1.	21--0450
UCRB(KNT)=-UCRB(KNT)	21--0460
YPLUT(KNT)=RHO(I)	21--0470
2 CONTINUE	21--0480
PT(1)=KNT	21--0490
KUDE=48	21--0500
IX1=ABS(UCRB(1))	21--0510
X1=IX1+1	21--0520
JX1=SIGN(X1,UCRB(1))	21--0530
IXL=ABS(UCRB(KNT))	21--0540
XL=IXL+1	21--0550
JXL=SIGN(XL,UCRB(KNT))	21--0560
IXBEG=MIN0(JX1,JXL)	21--0570
XBEU=100*IXBEG	21--0580
IDELX=ABS(JXL-JX1)	21--0590
DELX=IDELX*2	21--0600
IRU1=YPLUT(1)	21--0610
RU1=100*IRU1	21--0620

IRDF=YPLUT(KNT)	21--0630
IDELY=IRDF-IRU1	21--0640
DELY=IDELY+1	21--0650
PT(6)=4.	21--0660
PT(7)=XBEG	21--0670
PT(8)=DELX	21--0680
PT(9)=4.	21--0690
PT(10)=RU1	21--0700
PT(11)=DELY	21--0710
CALL SORTXY(UCRB,YPLUT,KNT)	21--0720
WRITE(6,100)FLPT	21--0730
CALL PLUTXY(UCRB,YPLUT,KODE,PT)	21--0740
WRITE(6,101)	21--0750
100 FORMAT(35HPT PLOT OF UCRB VS RHG FLPT=F4.0)	21--0760
101 FORMAT(2HPL)	21--0770
C.....SET UP PLOT OF FFSR, FFSI, FFGR, FFCL	21--0780
TEST=RHU0N+7.5*FKAYA	21--0790
CNSR=4.*KHU0N	21--0800
CNSI=CNSR	21--0810
IF(KTRL(9).EQ.2)CNSR=1.	21--0820
IF(KTRL(10).EQ.2)CNSI=1.	21--0830
KNT=0	21--0840
DO 28 I=1,ILAST	21--0850
IF(RHU(I)-TEST)29,29,28	21--0860
29 KNT=KNT+1	21--0870
28 CONTINUE	21--0880
NPTS=KNT	21--0890
KNT=0	21--0900
DO 12 I=1,ILAST	21--0910
IF(RHU(I)-TEST)11,11,12	21--0920
11 KNT=KNT+1	21--0930
12=NPTS+KNT	21--0940
13=NPTS+12	21--0950
14=NPTS+13	21--0960
XPLUT(KNT)=CNSR*FFSR(1)	21--0970
XPLUT(12)=CNSI*FFSI(1)	21--0980
XPLUT(13)=FFGR(1)	21--0990
XPLUT(14)=FFCL(1)	21--1000
YPLUT(KNT)=KHU(1)	21--1010
12 CONTINUE	21--1020
KDEL=YPLUT(NPTS)	21--1030
DELF=KDEL+1	21--1040
KK(1)=48	21--1050
KK(2)=4	21--1060
KK(3)=NPTS	21--1070
PT(1)=3.	21--1080
PT(6)=3.	21--1090
PT(7)=0.	21--1100
PT(8)=25.	21--1110
PT(9)=4.	21--1120
PT(10)=0.	21--1130
PT(11)=DELF	21--1140
WRITE(6,200)	21--1150
CALL PLUTMY(XPLUT,YPLUT,KK,PT)	21--1160
WRITE(6,201)	21--1170
RETURN	21--1180
200 FORMAT(44HPT PLOT OF FFSR, FFSI, FFGR, AND FFCL VS RHU)	21--1190
201 FORMAT(42HPL * FFSR + FFSI & FFGR X FFCL)	21--1200
END	21--1210

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*IBFTC TRIPS   LOST,DECK                                22--0010
      SUBROUTINE TRIPS                                    22--0020
C.....COMPUTE, OUTPUT, AND PLOT TRIPLE SCATTERING PARAMETERS 22--0030
C.....SCAT-4 DIMENSIONS AND COMMON                        22--0040
C.....VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS) 22--0050
      COMMON/PGU/FLPT,UCRB(250), UC16(250), UCRM(250), UCIM(250), 22--0060
      IUSRB(250), US16(250), USRM(250), USIM(250)          22--0070
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA 22--0080
      COMMON/TH1/DPULEX(150), DSGMEX(150), JMAX, PULEX(150), POLTH(150), 22--0090
      ISGMAEX(150), SGMA TH(150), THETA(150), THETAD(150) 22--0100
      COMMON/LIND/LMAX, LMAXM                                22--0110
C.....PAGE TITLING INFORMATION                            22--0120
      COMMON/PTI/NUMRUN, TITLE(13)                          22--0130
C.....SCATLE CONTROLS                                     22--0140
      COMMON/CNTR/KOUT, KSEND, KIRL(13), KTRLT(13), KTRLX(13) 22--0150
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS 22--0160
      COMMON/SACS/A1(150), AR(150), B1(150), BR(150), FCI(150), FCR(150) 22--0170
      I,SGMAC(150), SIGTEM(150), SRATIO(150)                22--0180
C.....VARIABLES WHICH ARE CALCULATED AS FUNCTIONS OF L     22--0190
      COMMON/VARL/C11(51), C12(51), CR1(51), CR2(51), EXSGMI(51), 22--0200
      IEXSGMR(51), F(52), FBAR(91), FP(51), G(52), GP(51)   22--0210
C.....ENERGY, MASS, AND CHARGE INPUT VALUES              22--0220
      COMMON/EMCV/ELAB, FMB, FMI, FMU, RC, ZZ                22--0230
      DIMENSION PT(11),K(14),XSAV(150),YPLUT(150)           22--0240
      EQUIVALENCE (UCRB,XSAV), (USRB,YPLUT)                  22--0250
      IF(KTRLX(11)-2) 355,309,355                            22--0260
309 CALL SKIP                                                22--0270
      WRITE(6,310)                                           22--0280
310 FORMAT(1H0,6X,5HTHETA,13X,3HFCR,17X,3HFC1,16X,6HAR-FCR,14X, 22--0290
      16HAI-FC1,14X,5HSGMAC)                                22--0300
      DO 325 J=1,JMAX                                         22--0310
      XSAV(J)=AR(J)-FCR(J)                                     22--0320
      YPLUT(J)=A1(J)-FC1(J)                                   22--0330
C.....OUTPUT REAL AND IMAG PARTS OF F, COULOMB SCATTERING AMPLITUDE 22--0340
325 WRITE(6,320) THETAD(J),FCR(J),FC1(J),XSAV(J),YPLUT(J),SGMAC(J) 22--0350
320 FORMAT(1H ,G15.3,5G20.8)                                22--0360
      CALL SKIP                                                22--0370
      WRITE(6,330)                                           22--0380
330 FORMAT(1H0,6X,5HTHETA,13X,4HCAMP,16X,4HCPHA,16X,4HNAMP,16X, 22--0390
      14HNPHA,9X,1HL,8X,6HSGCOUL)                            22--0400
C.....COMPUTE AND OUTPUT MAGNITUDES OF F, A-F              22--0410
      DO 335 J=1,JMAX                                         22--0420
      CAMP=SQRT(FCR(J)*FCR(J)+FC1(J)*FC1(J))                 22--0430
      CPHA=ATAN2(FC1(J),FCR(J))                               22--0440
      ANAMP=SQRT(XSAV(J)*XSAV(J)+YPLUT(J)*YPLUT(J))           22--0450
      ANPHA=ATAN2(YPLUT(J),XSAV(J))                           22--0460
      IF(J-LMAX) 332,332,331                                  22--0470
331 WRITE(6,340) THETAD(J),CAMP,CPHA,ANAMP,ANPHA            22--0480
      GO TO 335                                                22--0490
332 SGCOUL=.5*ATAN2(EXSGMI(J),EXSGMR(J))                     22--0500
      WRITE(6,340) THETAD(J),CAMP,CPHA,ANAMP,ANPHA,J,SGCOUL 22--0510
340 FORMAT(1H ,G15.3,4G20.8,13,G20.8)                       22--0520
335 CONTINUE                                                  22--0530
      IF(LMAX-JMAX) 355,355,352                                22--0540
352 LIN=JMAX+1                                                22--0550
      DO 353 L=LIN,LMAX                                         22--0560
      SGCOUL=.5*ATAN2(EXSGMI(L),EXSGMR(L))                   22--0570
353 WRITE(6,354) L,SGCOUL                                     22--0580
354 FORMAT(1H ,95X,13,G20.8)                                  22--0590
355 WRITE(6,1000) NUMRUN,TITLE                                22--0600
1000 FORMAT(11H1RUN NUMBER13,10X,13A6 ///8X,5HTHETA15X,6HTANBET 22--0610

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1      15X,4HBE TA12X,10H THETA,LAB14X,3HROT18X,3H-R') 22--0620
DO 5 J=1,JMAX 22--0630
YPLUT(J)=THETAD(J) 22--0640
ASQ= AR(J)*AR(J) + AI(J)*AI(J) 22--0650
BSQ= BR(J)*BR(J) + BI(J)*BI(J) 22--0660
TANBET=-2.*(AI(J)*BR(J) - AR(J)*BI(J))/(ASQ-BSQ) 22--0670
C.....CALCULATE LAB ANGLE IN TERMS OF TAN AND COS 22--0680
TNTHU= SIN(THETA(J))/(COS(THETA(J))+ FMI/FMB) 22--0690
SCTHO= SQRT(1. + TNTHU*TNTHU) 22--0700
IF(TNTHU)20,21,21 22--0710
20 CSTHO= -1./SCTHO 22--0720
GO TO 22 22--0730
21 CSTHO= 1./SCTHO 22--0740
C.....COMPUTE ROTATION OF POLARIZATION 22--0750
22 XXX= (ASQ-BSQ)/SGMATH(J) 22--0760
ROT= XXX*CSTHO*(1.+TANBET*TNTHU) 22--0770
CC=XXX*CSTHO*(TANBET-TNTHU) 22--0780
BETA= ATAN(TANBET) 22--0790
IF(TANBET)30,31,31 22--0800
30 BETA= 180.+BETA/.01745329252 22--0810
GO TO 32 22--0820
31 BETA= BETA/.01745329252 22--0830
32 THO= ATAN(TNTHU) 22--0840
IF(TNTHU)23,24,24 22--0850
23 THO= 180.+THO/.01745329252 22--0860
GO TO 25 22--0870
24 THO= THO/.01745329252 22--0880
25 CONTINUE 22--0890
C.....OUTPUT TRIPLE SCATTERING PARAMETERS 22--0900
WRITE (6,1001) THETAD(J),TANBET,BETA,THO,ROT,CC 22--0910
XSAV(J)=-CC 22--0920
JJ=J+JMAX 22--0930
XSAV(JJ)=-ROT 22--0940
5 CONTINUE 22--0950
C.....SET UP FOR PLOT OF ROT AND R-PRIME 22--0960
19 K(1)=48 22--0970
K(2)=2 22--0980
K(3)=JMAX 22--0990
PT(1)=3. 22--1000
PT(6)=4. 22--1010
PT(7)=-100. 22--1020
PT(8)=4. 22--1030
PT(9)=6. 22--1040
PT(10)=0. 22--1050
PT(11)=2. 22--1060
WRITE (6,100) 22--1070
CALL PLOTMY(XSAV,YPLUT ,K,PT) 22--1080
WRITE (6,101) 22--1090
100 FORMAT(23HPT PLOT OF -R' AND ROT) 22--1100
101 FORMAT(27HPL * -R' + ROT) 22--1110
1001 FORMAT(6G20.8) 22--1120
RETURN 22--1130
END 22--1140

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$IBFTC PTETDL LOST,DECK 23--0010
SUBROUTINE PTETDL 23--0020
C.....VARIABLES COMPUTED IN PGEN4 (NUCLEAR POTENTIAL TERMS) 23--0030
COMMON/PGU/FLPT,UCRB(250), UCIB(250), UCRM(250), UCIM(250), 23--0040

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1 USRB(250), USIB(250), USKM(250), USIM(250)	23--0050
COMMON/LIND/LMAX, %LMAXM	23--0060
C.....VARIABLES TO BE PLOTTED IN PTETDL	23--0070
COMMON/PTPL/AETA1(51), AETA2(51), DELR1(51), DELR2(51)	23--0080
DIMENSION KK(14), PT(11)	23--0090
DIMENSION XPLUT(408), YPLOT(408)	23--0100
EQUIVALENCE (UCRB,XPLUT), (USRB,YPLOT)	23--0110
C.....PLOTS ETA1,ETA2,DELP, DELM	23--0120
C.....SET UP ABSCISSA FOR BOTH PLOTS	23--0130
1 DO 2 I=1,5	23--0150
IF((LMAX-1)-10*I)3,3,2	23--0160
2 CONTINUE	23--0170
3 IF(I-3)5,4,5	23--0180
4 I=4	23--0190
5 PT(9)=5.0	23--0200
PT(10)=0.0	23--0210
PT(11)=I	23--0220
YPLOT(1)=0.	23--0230
DO 6 I=2,LMAX	23--0240
6 YPLOT(I)=YPLOT(I-1)+1.0	23--0250
C.....SET UP PLOT OF ETA	23--0260
7 KK(1)=48	23--0270
KK(2)=2	23--0280
KK(3)=LMAX	23--0290
PT(1)=3.0	23--0300
PT(6)=4.0	23--0310
PT(7)=-100.0	23--0320
PT(8)=2.0	23--0330
DO 8 I=1,LMAX	23--0340
XPLUT(I)=-AETA1(I)	23--0350
IP=I+LMAX	23--0360
8 XPLUT(IP)=-AETA2(I)	23--0370
WRITE (6,100)	23--0380
CALL PLOTMY(XPLUT,YPLOT,KK,PT)	23--0390
WRITE (6,101)	23--0400
C.....SET UP PLOT OF DELTA, DELTA-PI, DELTA+PI, DELTA+2PI	23--0410
9 KK(1)=48	23--0420
KK(2)=2	23--0430
KK(3)=4*LMAX	23--0440
PT(1)=3.0	23--0450
PT(6)=5.0	23--0460
PT(7)=-100.0	23--0470
PT(8)=1.0	23--0480
C.....COMPUTE NEGATIVE VALUES TO BE PLOTTED	23--0490
DO 10 J=1,4	23--0500
IN=(J-1)*LMAX	23--0510
IND=(J+3)*LMAX	23--0520
CON=FLOAT(J-2)*PI	23--0530
DO 10 I=1,LMAX	23--0540
II=IN+I	23--0550
XPLUT(II)=-(DELR1(I)+CON)	23--0560
IP=IND+I	23--0570
XPLUT(IP)=-(DELR2(I)+CON)	23--0580
10 YPLOT(II)=YPLOT(I)	23--0590
WRITE (6,102)	23--0600
CALL PLOTMY(XPLUT,YPLOT,KK,PT)	23--0610
WRITE (6,103)	23--0620
11 RETURN	23--0630
100 FORMAT(29HPT PLOT OF ETA1 AND ETA2 VS L)	23--0640
101 FORMAT(20HPL * ETA1 + ETA2)	23--0650
102 FORMAT(31HPT PLOT OF DELR1 AND DELR2 VS L)	23--0660
103 FORMAT(20HPL * DELR1 + DELR2)	23--0670
END	23--0680


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$IBFTC PTSCAT LUST,DECK                                24--0010
SUBROUTINE PTSCAT                                        24--0020
C.....SCATLE INPUT AND OUTPUT VARIABLES WHICH ARE FUNCTIONS OF THETA 24--0030
COMMON/TH1/UPOLEX(150), DSGMEX(150), JMAX, POLEX(150), POLTH(150), 24--0040
ISGMAEX(150), SGMATH(150), THETA(150), THETAD(150) 24--0050
C.....SCATLE CONTROLS                                24--0060
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13) 24--0070
C.....SCATTERING AMPLITUDES AND ADDITIONAL CROSS SECTIONS 24--0080
COMMON/SACS/A1(150), AR(150), BI(150), BR(150), FCI(150), FCR(150) 24--0090
1,SGMAC(150), SIGTEM(150), SRATIO(150) 24--0100
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION 24--0110
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150), 24--0120
1CHI2P(150), CHI2(150), ENORM, SGMATH, SNORM, XNORM, NP, CSNRM, NCSN 24--0130
DIMENSION PT(11), KK(14), PSAV(6) 24--0140
DIMENSION XPLUT(150), YPLUT(150) 24--0150
EQUIVALENCE (AR,XPLUT), (BR,YPLUT) 24--0160
DIMENSION FMTA(10), FMTA1(8), FMTA2(10), FMTB(6), FMTB1(5), 24--0170
1FMTB2(6) 24--0180
DATA FMTA1(1)/48H(43HPT PLOT OF SGMAEX AND SGMATH VS THETA (DEG))/24--0190
DATA FMTA2(1)/56H(51HPT PLOT OF (SNORM*SGMAEX) AND SGMATH VS THETA 24--0200
1 (DEG))/ 24--0210
DATA FMTB1(1)/28H(23HPL * SGMAEX + SGMATH)/ 24--0220
DATA FMTB2(1)/36H(31HPL * (ENORM*SGMAEX) + SGMATH)/ 24--0230
C.....KTRL(4)=0 NO PLOT 24--0240
C.....KTRL(4)=1 PLOT OF POLEX AND POLTH VS THETAD 24--0250
C.....KTRL(4)=2 PLOT OF SGMAEX AND SGMATH VS THETAD 24--0260
C.....KTRL(4)=3 PLOT POLARIZATIONS AND CROSS SECTIONS 24--0270
C.....KTRLX(5).NE.0 IF CROSS SECTIONS ARE PLOTTED, ALSO PLOT SGMAEX*END 24--0280
C..... AND SGMATH VS THETAD 24--0290
IF(KTRL(4).EQ.C)GO TO 48 24--0300
C.....SET UP YPLUT FOR ALL PLOTS 24--0310
TMAX=0. 24--0320
DO 7 J=1,JMAX 24--0330
IF(THETAD(J).GT.TMAX) TMAX=THETAD(J) 24--0340
YPLUT(J)=THETAD(J) 24--0350
KK(1)=48 24--0360
KK(2)=2 24--0370
KK(3)=JMAX 24--0380
PT(1)=3. 24--0390
PT(9)=5. 24--0400
PT(10)=0. 24--0410
I=1 24--0420
13 AI=I 24--0430
IF(TMAX.LE.50.*AI)GO TO 18 24--0440
I=I+1 24--0450
GO TO 13 24--0460
18 PT(11)=5*I 24--0470
IF(KTRL(4).EQ.2)GO TO 28 24--0480
.....PLOT POLEX AND POLTH VS THETAD 24--0490
PT(6)=4. 24--0500
PT(7)=-100. 24--0510
PT(8)=4. 24--0520
DO 21 J=1,JMAX 24--0530
XPLUT(J)=-POLEX(J) 24--0540
JJ=J+JMAX 24--0550
21 XPLUT(JJ)=-POLTH(J) 24--0560
WRITE(6,100) 24--0570
100 FORMAT(41HPT PLOT OF POLEX AND POLTH VS THETA (DEG)) 24--0580
CALL PLUTMY(XPLUT,YPLUT,KK,PT) 24--0590
WRITE(6,101) 24--0600
101 FORMAT(22HPL * POLEX + POLTH) 24--0610
IF(KTRL(4).EQ.1)GO TO 48 24--0620

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C.....PLOT SGMAEX AND SGMATH VS THETAD	24--0630
28 XMIN=1.E10	24--0640
XMAX=1.E-10	24--0650
DO 31 J=1,JMAX	24--0660
XPL0T(J)=-AL0G10(SGMAEX(J))	24--0670
JJ=J+JMAX	24--0680
XPL0T(JJ)=-AL0G10(SGMATH(JJ))	24--0690
IF(XPL0T(J).LT.XMIN)XMIN=XPL0T(J)	24--0700
IF(XPL0T(JJ).LT.XMIN)XMIN=XPL0T(JJ)	24--0710
IF(XPL0T(J).GT.XMAX)XMAX=XPL0T(J)	24--0720
IF(XPL0T(JJ).GT.XMAX)XMAX=XPL0T(JJ)	24--0730
31 CONTINUE	24--0740
K0D=1	24--0750
DO 33 I=1,8	24--0760
FMTA(I)=FMTA1(I)	24--0770
IF(1.GT.5)GO TO 33	24--0780
FMTB(I)=FMTB1(I)	24--0790
33 CONTINUE	24--0800
35 MIN=XMIN	24--0810
MIN=MIN-1	24--0820
MAX=XMAX	24--0830
MAX=MAX+1	24--0840
IF(MAX-MIN.LT.4)GO TO 36	24--0850
PT(6)=5.	24--0860
PT(7)=10*MIN	24--0870
PT(8)=1.	24--0880
GO TO 38	24--0890
36 PT(6)=4.	24--0900
PT(7)=100*MIN	24--0910
PT(8)=5.	24--0920
38 WRITE(6,FMTA)	24--0930
CALL PLOTMY(XPL0T,YPL0T,KK,PT)	24--0940
WRITE(6,FMTB)	24--0950
IF(K0D.EQ.2)GO TO 48	24--0960
IF(KFRLX(5).EQ.0)GO TO 48	24--0970
C.....PLOT SNORM * SGMAEX AND SGMATH VS THETAD	24--0980
DO 43 J=1,JMAX	24--0990
XPL0T(J)=-AL0G10(SNORM*SGMAEX(J))	24--1000
IF(XPL0T(J).LT.XMIN)XMIN=XPL0T(J)	24--1010
IF(XPL0T(J).GT.XMAX)XMAX=XPL0T(J)	24--1020
JJ=J+JMAX	24--1030
XPL0T(JJ)=-AL0G10(SGMATH(JJ))	24--1040
43 CONTINUE	24--1050
DO 45 I=1,10	24--1060
FMTA(I)=FMTA2(I)	24--1070
IF(1.GT.6)GO TO 45	24--1080
FMTB(I)=FMTB2(I)	24--1090
45 CONTINUE	24--1100
K0D=2	24--1110
GO TO 35	24--1120
48 RETURN	24--1130
END	24--1140

\$IBFTC ARGN	25--0010
SUBROUTINE ARGN	25--0020
C.....VARIABLE METRIC MINIMIZATION (MCNITUR ADAPTATION)	25--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	25--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	25--0050

IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	25--0060
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	25--0070
3VA, VF, VFP, VGP(12), VGP(12), VP, X(12), XP(12), Z	25--0080
C.....SCATLE PARAMETERS	25--0090
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	25--0100
C.....AUXILIARY SEARCH VARIABLES	25--0110
COMMON/ASV/DEL(12), ID(12), IIN, KOLMAX, LABEL(13), NHP, NMLR,	25--0120
NPCT, NPCTP, PCT	25--0130
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION	25--0140
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),	25--0150
1CHI2P(150), CHI2(150), ENORM, SGPRTH,SNORM,XNORM,NP,CSNRM,NCSN	25--0160
DIMENSION SER(12)	25--0170
EQUIVALENCE (RG,SER)	25--0180
DIMENSION CHIQS(19)	25--0190
EQUIVALENCE (CHIQS(1),CHI2ST)	25--0200
DO 705 I=1,N	25--0210
J=ID(I)	25--0220
705 X(I)=SER(J)	25--0230
101 MS=0	25--0240
105 WRITE (6,5)	25--0250
111 WRITE(6,6)N,KSTEP,E,VP,DELTA	25--0260
WRITE(6,7) NHP, NMLR, NPCT, PCT	25--0270
7 FORMAT(5HJNHP=I2,5X,5HNMLR=I2,5X,5HNPCT=I2,5X,4HPCT=F7.4)	25--0280
CALL SQUI	25--0290
2860 IF (NC) 113, 113, 2861	25--0300
2861 WRITE (6,2013)	25--0310
2862 DO 2863 J=1,NC	25--0320
2863 WRITE (6,2014) (C(I,J),I=1,N)	25--0330
113 WRITE (6,8)	25--0340
114 DO 115 I=1,N	25--0350
115 WRITE (6,9) (H(I,J),J=1,N)	25--0360
117 CALL FCN(N,VG(1),VF,X(1))	25--0370
M1=0	25--0380
IIN=1	25--0390
118 LV = 1	25--0400
1185 IT=0	25--0410
119 WRITE (6,14) IT,MS,VF	25--0420
CALL SQUT	25--0430
120 WRITE (6,4)	25--0440
1201 IF (NC) 121,121,1202	25--0450
1202 DO 1205 J1=1,NC	25--0460
1203 CALL MATMPY(N,N,H(1,1),C(1,J1),T(1))	25--0470
1204 CALL MATMPY(1,N,T(1),C(1,J1),TO)	25--0480
2204 IF (M1-1) 1206, 1206, 1205	25--0490
1205 IF (TO-E) 1209, 1209, 1206	25--0500
1206 DO 1208 I=1,N	25--0510
1207 DO 1208 J=1,N	25--0520
1208 H(1,J)=H(1,J)-T(1)*T(J)/TO	25--0530
1209 CONTINUE	25--0540
121 CALL READY	25--0550
122 LV = LV	25--0560
123 GO TO (139,159,137,126),LV	25--0570
124 LV = 2	25--0580
125 GO TO 121	25--0590
126 CALL AIM	25--0600
127 LV = LV	25--0610
128 GO TO (129,135,137),LV	25--0620
129 CALL FARE	25--0630
IF(M1.GE.NMLR)GO TO 1395	25--0640
130 LV = LV	25--0650
131 GO TO (135,132,126),LV	25--0660
132 LV = 1	25--0670

133 CALL DRESS(\$142)	25--0680
1335 LV = LV	25--0690
134 GU TO (124,156),LV	25--0700
135 LV = 2	25--0710
136 GU TO 133	25--0720
137 LV = 3	25--0730
138 GU TO 133	25--0740
155 LV = 4	25--0750
161 GU TO 133	25--0760
139 IF(NSSW1.LT.1)CALL SOUT	25--0770
1395 WRITE(6,8)	25--0780
DO 1096 I=1,N	25--0790
1096 WRITE(6,9) (H(I,J),J=1,N)	25--0800
CALL STUFF	25--0810
140 LV = LV	25--0820
141 GU TO (117,142),LV	25--0830
142 WRITE (6,10)	25--0840
143 WRITE (6,11)	25--0850
144 DO 145 I=1,N	25--0860
145 WRITE (6,9)(H(I,J),J=1,N)	25--0870
146 WRITE (6,13)DELTA,VF,GS	25--0880
CALL SOUT	25--0890
DO 148 KK=1,NCSN	25--0900
148 CHIQS(KK)=CHIQS(KK)/CSNKM	25--0910
WRITE(6,15) CSNKM, CHI2T, CHI2ST, CHI2PT	25--0920
15 FORMAT(1HK,13X,20HSUM OF CHI SQUARES /F5.0,15X,6HCHI2T=G13.5,	25--0930
15X,7HCHI2ST=G13.5,5X,7HCHI2PT=G13.5)	25--0940
CALL SOUT	25--0950
150 CALL FCN(N,VG(1),VF,X(1))	25--0960
156 CONTINUE	25--0970
RETURN	25--0980
2013 FORMAT(12HCONSTRAINTS)	25--0990
2014 FORMAT(3HU 1P8E14.5)	25--1000
4 FORMAT(20HO- - - - -)	25--1010
5 FORMAT(29HOVARIABLE METRIC MINIMIZATION)	25--1020
6 FORMAT(3HON=12,4H K=12,4H E=1PE14.5,4H P=E14.5,8H DELTA=E14.5)	25--1030
8 FORMAT(2HON)	25--1040
9 FORMAT(1H01P8E14.5/(1H08E14.5))	25--1050
10 FORMAT(13HOFINAL VALUES)	25--1060
11 FORMAT(13HOERROR MATRIX)	25--1070
13 FORMAT(7HDELTA=1PE14.5,4H F=E14.5,5H GS=E14.5)	25--1080
14 FORMAT(4HCIT 14,7H STEP 14,4H F=1PE14.5)	25--1090
END	25--1100

\$IBFTC SOUTT LOST,DECK	26--0010
SUBROUTINE SOUTI	26--0020
C.....SEARCH OUTPUT OF PARAMETERS DERIVATIVES AND CHI SQUARES	26--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	26--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	26--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	26--0060
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	26--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	26--0080
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION	26--0090
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),	26--0100
1CHI2P(150), CHI2(150), ENORM, SGMRTH,SNORM,XNORM,NP,CSNRM,NCSN	26--0110
C.....AUXILIARY SEARCH VARIABLES	26--0120
COMMON/ASV/DEL(12), ID(12), IIN, KDLMAX, LABEL(13), NHP, NMLR,	26--0130
INPCT, NPCTP, PCT	26--0140
DIMENSION CSID(2)	26--0150
DATA (CSID(1),I=1,2)/5HSIGMA,5H POL /	26--0160
KUD=1	26--0170

3	IA=1	26--0180
	IB=MING(N,9)	26--0190
8	WRITE(6,10) (LABEL(I),I=IA,IB)	26--0200
10	FORMAT(7X,A5,8(9X,A5))	26--0210
	WRITE(6,20) (X(I),I=IA,IB)	26--0220
20	FORMAT(3HJX=1P9G14.5)	26--0230
	IF(KUU.EQ.2)WRITE(6,30) (VG(I),I=IA,IB)	26--0240
30	FORMAT(3HJG=1P9G14.5)	26--0250
	IF(IB.EQ.N)GO TO 23	26--0260
	IA=10	26--0270
	IB=N	26--0280
	GO TO 8	26--0290
23	IF(KUU.EQ.1)GO TO 53	26--0300
	WRITE(6,40) ENORM, SGMRTH, CHI2T, CHI2ST, CHI2PT	26--0310
40	FORMAT(1HJ,6HENORM=G13.5,5X,11HSIGMAR(TH)=G13.5,5X,6HCHI2T=G13.5,	26--0320
	15X,7HCHI2ST=G13.5,5X,7HCHI2PT=G13.5)	26--0330
	ENTRY SUUF	26--0340
	GO TO (47,45,43),KOLMAX	26--0350
43	WRITE(6,50)	26--0360
50	FORMAT(1HJ,20X,4HSUMF,21X,4HSCMM,21X,4HSUMR)	26--0370
	WRITE(6,60) CSID(1), (SUMS(KK),KK=9,13,2)	26--0380
60	FORMAT(1HJA5,3G25.8)	26--0390
	WRITE(6,60) CSID(2), (SUMS(KK),KK=10,14,2)	26--0400
	GO TO 47	26--0410
45	WRITE(6,70)	26--0420
70	FORMAT(1HJ,12X,4HSUM1,11X,4HSUM2,11X,4HSUM3,11X,4HSUM4,11X,	26--0430
	14HSUMF,11X,4HSUMM,11X,4HSUMR,10X,5HSUM34)	26--0440
	WRITE(6,80) CSID(1), (SUMS(KK),KK=1,15,2)	26--0450
80	FORMAT(1HJA6,8G15.5)	26--0460
	WRITE(6,80) CSID(2), (SUMS(KK),KK=2,16,2)	26--0470
47	CONTINUE	26--0480
53	RETURN	26--0490
	ENTRY SUOT	26--0500
	KUU=2	26--0510
	GO TO 3	26--0520
	END	26--0530

\$IBFTC READY	LUST,DECK	27--0010
	SUBROUTINE READY	27--0020
C.....READY (MONITOR ADAPTATION)		27--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM		27--0040
	COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	27--0050
	IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	27--0060
	2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	27--0070
	3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	27--0080
C.....AUXILIARY SEARCH VARIABLES		27--0090
	COMMON/ASV/DEL(12), ID(12), IIN, KOLMAX, LABEL(13), NHP, NMLR,	27--0100
	INPCT, NPCTP, PCT	27--0110
	DIMENSION FEX(12)	27--0120
	LV = LV	27--0130
	GO TO (200,201),LV.	27--0140
200	IT=1	27--0150
201	CALL MATMPY (N,N,H(1,1),VG(1),S(1))	27--0160
202	DO 203 I=1,N	27--0170
203	S(I)=-S(I)	27--0180
204	M=1	27--0190
205	CALL MATMPY (M,N,S(1),VG(1),GS)	27--0200
206	IF(GS+E)207,227,227	27--0210
207	IF(IT.GT.NPCTP)GO TO 246	27--0220
	FEX(IT)=VF	27--0230
	IF(IT.EQ.NPCTP)GO TO 249	27--0240
	GO TO 255	27--0250

246 FEX(NPCT+2)=VF	27--0260
DO 248 KK=1,NPCTP	27--0270
248 FEX(KK)=FEX(KK+1)	27--0280
249 TEST=.C1*PCT*VF	27--0290
IF(FEX(1)-FEX(NPCTP).GT.TEST)GO TO 255	27--0300
WRITE(6,2)NPCT,PCT	27--0310
2 FORMAT(33H)THE CHANGE IN F DURING THE LAST 12,	27--0320
125H ITERATIONS IS LESS THAN F7.4,9H PER CENT)	27--0330
GO TO 227	27--0340
255 TP1 = -2.0*(VF/GS)	27--0350
208 EL=AMIN1(2.0,TP1)	27--0360
209 SL=-GS	27--0370
210 DO 211 I=1,N	27--0380
211 XP(I)=X(I)+EL*S(I)	27--0390
213 CALL FCN(N,VGP(1),VFP,XP(1))	27--0400
214 M=1	27--0410
215 CALL MATMPY (M,N,S(1),VGP(1),GSP)	27--0420
216 IF(GSP)217,225,229	27--0430
217 IF (VFP-VF) 218,229,229	27--0440
218 WRITE (6,1)	27--0450
231 FB = VFP	27--0460
232 DO 234 I=1,N	27--0470
233 GB(I) = VGP(I)	27--0480
234 T(I)=XP(I)	27--0490
220 IF(EL-2.0)221,223,223	27--0500
221 LV = 3	27--0510
222 RETURN	27--0520
223 DELTA=2.0*DELTA	27--0530
224 TU=1.0/SL	27--0540
225 LV = 2	27--0550
226 GO TO 222	27--0560
227 LV = 1	27--0570
228 GO TO 222	27--0580
229 LV = 4	27--0590
230 GO TO 222	27--0600
1 FORMAT(10H)UNDER SHOT)	27--0610
END	27--0620

\$IBFTC AIM LUST,DECK	28--0010
SUBROUTINE AIM	28--0020
C.....AIM (MCNITUR ADAPTATION)	28--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	28--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FU, GB(12), GS, GSB,	28--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	28--0060
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	28--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	28--0080
300 Z = GS+GSP+3.0*(VF-VFP)/EL	28--0090
301 TO=GS/Z	28--0100
T1=GSP/Z	28--0110
302 Q=SQRT(1.0-TO*T1)	28--0120
Q = ABS(Q*Z)	28--0130
VA = (GSP+Q-Z)/(GSP-GS+2.0*Q)	28--0140
303 TO = (EL*(GSP+Z+2.0*Q)*VA**2)/3.0	28--0150
304 FU = VFP-TU	28--0160
305 CALL MATMPY (N,N,H(1,1),VGP(1),T(1))	28--0170
306 TP1=GSP/SL	28--0180
307 DO 308 I=1,N	28--0190
308 T(I)=-T(I)+TP1*S(I)	28--0200
309 M=1	28--0210
310 CALL MATMPY(M,N,T(1),VGP(1),GTP)	28--0220
311 IF(2.0*TO+GTP)317,312,312	28--0230
312 TP1 = 1.0-VA	28--0240

313 DO 314 I=1,N	28--0250
314 T(I) = VA*X(I)+TP1*XP(I)	28--0260
315 LV = 1	28--0270
316 RETURN	28--0280
317 IF (VF+GTP/2.0) 312,318,318	28--0290
318 DO 319 I=1,N	28--0300
319 T(I)=T(I)+XP(I)	28--0310
321 CALL FCN(N,GB(1),FB,T(1))	28--0320
322 IF(FB-FU)323,312,312	28--0330
323 WRITE (6,1)	28--0340
324 DO 325 I=1,N	28--0350
325 S(I)=T(I)-XP(I)	28--0360
326 M=1	28--0370
327 CALL MATMPY(M,N,S(1),GB(1),GTT)	28--0380
328 GTT=GTT-GTP	28--0390
329 IF(GTT)335,330,330	28--0400
330 GSS=GTT	28--0410
331 SL=-GTP	28--0420
332 EL=1.0	28--0430
333 LV = 2	28--0440
334 GO TO 310	28--0450
335 LV = 3	28--0460
336 GO TO 316	28--0470
1 FORMAT(9H0R1C0CHET)	28--0480
END	28--0490
\$1BFTC FIRE LOST,DECK	29--0010
SUBROUTINE FIRE	29--0020
C.....FIRE (MONITOR ADAPTATION)	29--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	29--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FU, GB(12), GS, GSB,	29--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	29--0060
2M, M1, MS, N, NC, NS, NSSM1, NSSM2, Q, RS, S(12), SL, T(12), TO,	29--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	29--0080
401 CALL FCN(N,GB(1),FB,T(1))	29--0090
402 M=1	29--0100
IF(ABS(VA)-1.E-30)410,403,403	29--0110
403 CALL MATMPY(M,N,S(1),GB(1),GSB)	29--0120
404 TP1= AMIN1(VF,VFP)	29--0130
405 IF(TP1-FB+E)418,406,406	29--0140
406 TP1=VA/(1.0-VA)	29--0150
407 TP2 = (1.0-VA)/VA	29--0160
408 TO=GSB*(TP1-TP2)	29--0170
409 IF(ABS(TO)-Q)413,410,410	29--0180
410 GSS=2.0*Q	29--0190
411 LV = 1	29--0200
M1=0	29--0210
412 RETURN	29--0220
413 GSS=TO+2.0*Q	29--0230
414 DO 415 I=1,N	29--0240
415 VG(I) = (GB(I)-VG(I))*TP1+(VGP(I)-GB(I))*TP2	29--0250
416 LV = 2	29--0260
M1=0	29--0270
417 GO TO 412	29--0280
418 IF (VF-VFP) 419,428,428	29--0290
419 WRITE (6,1)	29--0300
420 EL = (1.0-VA)*EL	29--0310
421 VFP = FB	29--0320
422 GSP=GSB	29--0330
423 DO 425 I=1,N	29--0340
424 XP(I)=T(I)	29--0350
425 VGP(I) = GB(I)	29--0360

426 LV = 3	29--0370
M1=M1+1	29--0380
427 GO TO 412	29--0390
428 WRITE (6,2)	29--0400
429 EL = EL*VA	29--0410
430 VF = FB	29--0420
431 GS=GSB	29--0430
432 DO 434 I=1,N	29--0440
433 X(I)=T(I)	29--0450
434 VG(I) = GB(I)	29--0460
435 GO TO 426	29--0470
1 FORMAT(10HOMOVE LEFT)	29--0480
2 FORMAT(11HOMOVE RIGHT)	29--0490
END	29--0500
\$IBFIC DRESS LOST,DECK	30--0010
SUBROUTINE DRESS(*)	30--0020
C.....DRESS (MONITOR ADAPTATION)	30--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	30--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	30--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	30--0060
ZM, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TU,	30--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	30--0080
C.....AUXILIARY SEARCH VARIABLES	30--0090
COMMON/ASV/DEL(12), ID(12), IIN, KOLMAX, LABEL(13), NHP, NMLR,	30--0100
INPCT, NPC1P, PCT	30--0110
C.....VARIABLES NEEDED FOR POP1	30--0120
COMMON JMAX, LMAX, THETA(75)	30--0130
C..... VARIABLES NEEDED FOR AB	30--0140
COMMON AK(75), AI(75),	30--0150
1 BR(75), BI(75),	30--0160
2 CR1(51), CR2(51), CI1(51), CI2(51),	30--0170
3 EXSGMK(51), EXSGMI(51),	30--0180
4 FKAY, FCR(75), FCI(75)	30--0190
LV = LV	30--0200
GO TO (500,525,519,510),LV	30--0210
500 CALL MATMPY(N,N,H(1,1),VG(1),X(1))	30--0220
501 M=1	30--0230
502 CALL MATMPY(M,N,X(1),VG(1),TU)	30--0240
503 TP1=SL-GSS**2/TU-E	30--0250
504 IF(TP1)524,505,505	30--0260
505 DO 507 I=1,N	30--0270
506 DO 507 J=1,N	30--0280
507 H(I,J)=H(I,J)-X(1)*X(J)/TG	30--0290
508 DELTA=DELTA*(EL*GSS/TU)	30--0300
509 TU=EL/GSS	30--0310
510 DO 512 I=1,N	30--0320
511 DO 512 J=1,N	30--0330
512 H(I,J)=H(I,J)+TU*S(I)*S(J)	30--0340
515 VF = FB	30--0350
520 DO 522 I=1,N	30--0360
521 VG(I) = GB(I)	30--0370
522 X(I)=T(I)	30--0380
513 WRITE (6,1)IT,MS,VF,GS	30--0390
IF(NSSW1.LT.1)GO TO 517	30--0400
516 WRITE (6,3)DELTA	30--0410
CALL SOUT	30--0420
IF(IIN.NE.NHP)GO TO 517	30--0430
560 IIN=0	30--0440
WRITE(6,7)	30--0450
DO 534 I=1,N	30--0460
534 WRITE(6,8) (H(I,J),J=1,N)	30--0470

517 WRITE (6,4)	30--0480
CALL POT1CH(\$585)	30--0490
518 IT=IT+1	30--0500
IIN=IIN+1	30--0510
5185 LV = 1	30--0520
523 RETURN	30--0530
524 WRITE (6,5)	30--0540
525 TP1=EL*SL/GSS	30--0550
526 DELTA=DELTA*TP1	30--0560
527 TU=(TP1-1.0)/SL	30--0570
528 GO TO 510	30--0580
585 RETURN 1	30--0590
1 FORMAT(4HCIT I4,7H STEP I4,4H F=1PE14.5,5H GS=E14.5)	30--0600
3 FORMAT(7HODELTA=1PE14.5)	30--0610
4 FORMAT(20H0- - - - -)	30--0620
5 FORMAT(9HOCOLINEAR)	30--0630
7 FORMAT(13H0ERROR MATRIX)	30--0640
8 FORMAT(1H01P8E14.5/(1H08E14.5))	30--0650
END	30--0660
\$IBFTC STUFF LUST,DECK	31--0010
SUBROUTINE STUFF	31--0020
C.....STUFF(MONITOR ADAPTATION)	31--0030
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	31--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	31--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	31--0060
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	31--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	31--0080
600 KSTEP=KSTEP-1	31--0090
601 IF(KSTEP)617,602,602	31--0100
602 MS=MS+1	31--0110
620 WRITE (6,1)MS,DELTA,GS	31--0120
603 DO 604 I=1,N	31--0130
CALL RAND(Y)	31--0140
604 T(1)=Y-.5	31--0150
605 CALL MATMPY(N,N,H(1,1),T(1),S(1))	31--0160
606 M=1	31--0170
607 CALL MATMPY(M,N,S(1),T(1),TP1)	31--0180
608 TP1=SQRT(TP1)	31--0190
609 EL = VP/TP1	31--0200
610 DO 611 I=1,N	31--0210
611 X(1)=X(1)+EL*S(I)	31--0220
614 LV = 1	31--0230
616 RETURN	31--0240
617 LV = 2	31--0250
618 MS=0	31--0260
619 GO TO 610	31--0270
1 FORMAT(13HORANDOM STEP I4,8H DELTA=1PE14.5,5H GS=E14.5)	31--0280
END	31--0290
\$IBFTC MATMPY LUST,DECK	32--0010
SUBROUTINE MATMPY(M,N,H,VG,S)	32--0020
C.....MATRIX MULTIPLICATION (MONITOR ADAPTATION)	32--0030

C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	32--0040
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	32--0050
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	32--0060
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	32--0070
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	32--0080
702 DO 703 I=1,M	32--0090
700 S(I)=0.0	32--0100
DO 703 J=1,N	32--0110
703 S(I)=H(J,I)*VG(J)+S(I)	32--0120
704 RETURN	32--0130
END	32--0140
5IBFTC FCN LUST,DECK	33--0010
SUBROUTINE FCN(N,VG,VF,X)	33--0020
C.....VARIABLES USED IN ARGONNE SEARCH PROGRAM	33--0030
COMMON/AGN/C(12,10), DELTA, E, EL, FAC, FB, FO, GB(12), GS, GSB,	33--0040
IGSP, GSS, GTP, GTT, H(12,12), IT, KSTEP, LV, LS,	33--0050
2M, M1, MS, N, NC, NS, NSSW1, NSSW2, Q, RS, S(12), SL, T(12), TO,	33--0060
3VA, VF, VFP, VG(12), VGP(12), VP, X(12), XP(12), Z	33--0070
C.....AUXILIARY SEARCH VARIABLES	33--0080
COMMON/ASV/DEL(12), ID(12), IIN, KDLMAX, LABEL(13), NHP, NMLR,	33--0090
INPCT, NPCTP, PCT	33--0100
C.....SCATLE PARAMETERS	33--0110
COMMON/PARA/RG, RO, V, W, A, VS, WS, BG, DUMMY(4), NAME(12)	33--0120
C.....CHI SQUARES, NORMALIZATION CONSTANT, AND SIGMA REACTION	33--0130
COMMON/CSQ/CHI2ST, CHI2PT, CHI2T, SUMS(16), CHI2S(150),	33--0140
ICH12P(150), CHI2(150), ENORM, SGMRTN,SNORM,XNORM,NP,CSNRM,NCSN	33--0150
C.....SCATLE CONTROLS	33--0160
COMMON/CNTR/KOUT, KSEND, KTRL(13), KTRLT(13), KTRLX(13)	33--0170
C.....OTHER SCATLE VARIABLES	33--0180
COMMON/MISC/ECM, ETA, ETA2, FKAY, FKAYA, FKAYB, RHOBC, RHOBN,	33--0190
RHUBNG, SIGMAO, SIGMA1, TEMP	33--0200
DIMENSION SER(12)	33--0210
EQUIVALENCE (RG,SER)	33--0220
DIMENSION CHIQS(19), CHIQST(19)	33--0230
EQUIVALENCE (CHIQS(1),CHI2ST)	33--0240
C.....CALCULATE FUNCTION AND PARTIAL DERIVATIVES TO BE USED BY SEARCH	33--0250
XX=0.	33--0260
IND = KTRLX(4)	33--0270
DO 802 I=1,N	33--0280
J=ID(I)	33--0290
802 SER(J)=X(I)	33--0300
KODE = 1	33--0310
DO 816 I=1,N	33--0320
J=ID(I)	33--0330
IF(I.NE.1)GO TO 813	33--0340
811 CONTINUE	33--0350
RHOBN=TEMP*RO	33--0360
RHUBNG = TEMP*RG	33--0370
FKAYA=FKAY*A	33--0380
FKAYB=FKAY*BG	33--0390
CALL PGEN4	33--0400
CALL INTCR(\$825)	33--0410
CALL CSUBL	33--0420
CALL AB	33--0430
CALL SGSGCP	33--0440
CALL SIGMAR	33--0450
CALL CHISQ	33--0460

IF(KTRLX(12).EQ.1)XX=CHIQS(IND+1)	33--0470
IF(KODE.EQ.2)GO TO 815	33--0480
VF=CHIQS(IND)+XX	33--0490
DO 812 K=1,19	33--0500
812 CHIQST(K)=CHIQS(K)	33--0510
ENRMT=ENORM	33--0520
SGMT=SGMRTH	33--0530
KUDE = 2	33--0540
813 SER(J)=SER(J)+DEL(I)	33--0550
GO TO 811	33--0560
815 VG(I) = (CHIQS(IND)+XX-VF)/DEL(I)	33--0570
SER(J) = SER(J)-DEL(I)	33--0580
816 CONTINUE	33--0590
DO 818 K=1,19	33--0600
818 CHIQS(K)=CHIQST(K)	33--0610
ENORM=ENRMT	33--0620
SGMRTH=SGMT	33--0630
RETURN	33--0640
825 WRITE(6,830)	33--0650
830 FORMAT(62HK NONSTANDARD RETURN FROM INTCTR IN FCN, EXECUTION TERM	33--0660
INATED)	33--0670
STOP	33--0680
END	33--0690
\$IBFTC SCTBD LOST,DECK	34--0010
BLCK DATA	34--0020
C.....SCATLE PARAMETERS	34--0030
COMMON/PARA/RI, RS, VO, WI, AS, VS, WS, AI, WVI, AO, RO, VSODD,	34--0040
INAME(12)	34--0050
C.....CONVERGENCE CRITERIA	34--0060
COMMON/CUNV/EPS1, EPS2, EPS3, EPS4	34--0070
DATA(NAME(1),I=1,12)/2HRI,2HRS,2HVO,2HWI,2HAS,2HVS,2HWS,2HAI,	34--0080
13HWVI,2HAU,2HRO,5HVSODD/	34--0090
DATA EPS1,EPS2,EPS3,EPS4 /3*.00001, .001/	34--0100
END	34--0110

Lewis Research Center,
National Aeronautics and Space Administration,
Cleveland, Ohio, April 29, 1970,
129-02.

APPENDIX A

SYMBOLS

AI	diffuseness parameter in nuclear potential (eq. (15)), fm	\hbar	Planck constant, MeV-sec
		IN1, IN2 } IN3, IN4 }	number of angles in ranges 1 through 4 (eq. (41))
AO	diffuseness parameter in nuclear potential (eq. (12)), fm	J_{\max}	last angle in data set
		j	total angular momentum quantum number
AS	diffuseness parameter in nuclear potential (eq. (7)), fm	k	wave number in center-of- mass system, fm^{-1}
$A(\theta)$	spin-independent scattering amplitude (eq. (22a))	\vec{k}	wave vector, fm^{-1}
		\vec{L}	orbital angular momentum operator
a	diffuseness parameter in nuclear potential, fm	l	orbital angular momentum quantum number
$B(\theta)$	spin-dependent scattering amplitude (eq. (22b))	l_{lim}	see eq. (44)
C_l^{\pm}	coefficients used to compute scattering amplitudes (eq. (21))	M_{π}	mass of pion, kg
		m_b	mass of target nucleus, amu
c	velocity of light, m/sec	m_i	mass of incident nucleus, amu
E	energy in center-of-mass system, MeV	N	normalization constant for $\sigma^{\text{ex}}(\theta)$ (eq. (35))
e	electron charge, C	NF	last forward angle
$f_c(\theta)$	coulomb scattering amplitude (eq. (23))	NR	last middle angle
f_{χ^2}	chi-square function to be minimized by search	N_E	normalization constant for $\sigma^{\text{ex}}(\theta)$ which gives smallest χ^2 for a given $\sigma^{\text{th}}(\theta)$ (eq. (36))
G_j	j^{th} component of gradient of f_{χ^2} (eq. (50))	N1, N2, } N3, N4 }	first angle of ranges 1 through 4 (eq. (41))
H	matrix used as metric in search parameter space	\vec{n}	unit normal vector

$P(\theta)$	polarization at angle θ (eq. (27))	VS	strength parameter for real spin-orbit nuclear potential, MeV
$\overline{P}(\theta)$	polarization vector	VSODD	strength parameter for real spin-orbit nuclear potential, for odd values of l , MeV
$\Delta P^{\text{ex}}(\theta)$	uncertainty in experimental polarization at angle θ	V_{EFF}	dimensionless effective potential for given l (eq. (43))
$P_l(\cos \theta)$	Legendre polynomial	$V_1(r)$	spin-independent potential (eq. (2)), MeV
$P_l^1(\cos \theta)$	associated Legendre poly- nomial	$V_2(r)$	spin-dependent potential (eq. (2)), MeV
R	rotation parameter (eq. (28))	WI	strength parameter for imaginary central nuclear potential, MeV
R'	rotation parameter (eq. (29))	WS	strength parameter for imaginary spin-orbit nuclear potential, MeV
RC	coulomb charge radius param- eter	WVI	strength parameter for imaginary central nuclear potential, MeV
RI	radius parameter in nuclear potential (eq. (15)), fm	x_j	current values of j^{th} search parameter
RO	radius parameter in nuclear potential (eq. (12)), fm	Δx_j	increment for x_j in eq. (50)
RS	radius parameter in nuclear potential (eq. (7)), fm	Z	dimensionless charge number of incident nucleus
r	radial coordinate, fm	Z'	dimensionless charge number of target nucleus
\overline{S}	spin angular momentum operator	β	rotation angle (eqs. (25a) and (25b)), deg
S_l	orbital angular momentum number (eqs. (48a) and (48b))	δ_l^{\pm}	phase shifts (eq. (21))
TCI	see eq. (45b)	$\epsilon_1, \epsilon_2, \epsilon_3, \epsilon_4$	convergence parameters
TCR	see eq. (45a)		
TSI	see eq. (49b)		
TSR	see eq. (49a)		
V	scattering potential, MeV		
VO	strength parameter for real central nuclear potential, MeV		

η	coulomb parameter (eq. (5))	LAB	value as measured in laboratory system
η_l^\pm	absorption coefficients (eqs. (20a) and (20b))	l	orbital angular momentum
θ	angular coordinate in center-of-mass system, deg	M	middle angles (eq. (39))
μ	reduced mass, amu	max	maximum
ρ	dimensionless radial coordinate (eq. (3))	n	number of search parameters
$\sigma(\theta)$	elastic cross section at angle θ , fm ²	O	corresponds to input parameters AO and RO
σ_l	coulomb phase shift (eq. (24))	P	polarization
σ_0	coulomb phase shift for $l = 0$	R	backward angles (eq. (40))
$\Delta\sigma^{\text{ex}}(\theta)$	uncertainty in experimental cross section at angle θ , fm ²	R	real part of complex number
χ^2	sum of chi-squares for a range of angles	S	corresponds to input parameters AS and RS
$\chi^2(\theta)$	chi-square at angle θ	SO	spin-orbit
ψ	wave function representing scattering particle	T	total (polarization + cross section)
Subscripts:		σ	cross section
CN	central nuclear	0	incident
coul	coulomb	1	after single scattering
F	forward angles (eq. (38))	2	after double scattering
I	corresponds to input parameters AI and RI	Superscripts:	
\Im	imaginary part of complex number	ex	experimental values
j	index denoting j th parameter, 1, . . . , n	th	theoretical or calculated values
K	index denoting particular χ^2 function (eq. (41)), 1, . . . , 4	+	total angular momentum, $j = l + 1/2$
		-	total angular momentum, $j = l - 1/2$

APPENDIX B

GLOSSARY OF FORTRAN VARIABLES

The FORTRAN variables listed here are those appearing in the COMMON statements of program SCATLE. Some of the FORTRAN variables in COMMON block /AGN/ are omitted, since they are internal to the search subroutines of reference 2. When two or more FORTRAN names refer to the same variable, the alternate names are enclosed in brackets. Some of the mathematical symbols listed do not appear in appendix A. Those symbols correspond to symbols in references 1 and 2, and are defined in the last column.

FORTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
AETA1(L), AETA2(L)	51	PTPL	η_L^+, η_L^-	absorption coefficients (eqs. (20a) and (20b))
AI, [BG]		PARA	a_I	diffuseness parameter for Gaussian absorption (eqs. (14), (16), (17), (18))
AO, [DUMMY(2)]		PARA	a_O	diffuseness parameter for de-coupled potential (eq. (11))
AR(J), AI(J), [AAI(J)]	150	SACS	$A_{0I}(\theta), A_{\theta I}(\theta)$	spin-independent scattering amplitude at angle θ (eq. (22a))
AS, [A]		PARA	a_S	diffuseness parameter, (eqs. (10) and (13))
BR(J), BI(J)	150	SACS	$B_{0R}(\theta), B_{\theta R}(\theta)$	spin-dependent scattering amplitude at angle θ (eq. (22b))
C(K, M)	(12, 10)	AGN		constraint coefficients for search procedure
CHI2(J)	150	CSQ	$\chi_T^2(\theta)$	total chi-square at angle θ
CHI2T, [CHISQ(3)]		CSQ	χ_T^2	total chi-square summed over J_{\max} angles (eq. (34))
CHI2P(J)	150	CSQ	$\chi_P^2(\theta)$	chi-square for polarization at angle θ (eq. (33))
CHI2PT, [CHISQ(2)]		CSQ	χ_P^2	chi-square for polarization summed over J_{\max} angles (eq. (33))
CHI2S(J)	150	CSQ	$\chi_G^2(\theta)$	chi-square for cross section at angle θ (eqs. (35) and (37))
CHI2ST, [CHISQ(1)]		CSQ	χ_G^2	chi-square for cross section summed over J_{\max} angles (eq. (35))
CR1(L), CI1(L)	51	VARL	$C_{L,R}^+, C_{L,\theta}^+$	see eqs. (21), (22a), and (22b)
CR2(L), CI2(L)	51	VARL	$C_{L,R}^-, C_{L,\theta}^-$	see eqs. (21), (22a), and (22b)

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
CSNRM		CSQ		JMAX - NP
DAI, DAO, DAS, DRI, DRO, DRS, DVO, DVS, DVSODD, DWI, DWS, DWVI		GDV		parameter increments used for grid procedure (table IV)
DEL(K)	12	ASV	Δx_j	increment for search parameter x_j (eq. (50))
DELR1(L), DELR2(L)	51	PTPL	$\delta_{l,R}^+, \delta_{l,R}^-$	see eq. (21)
DELTA		AGN		determinant of H-matrix used in search procedure
DPOLEX(J)	150	THI	$\Delta P^{\text{ex}}(\theta)$	standard deviation in ex- perimental polarization at angle θ (eq. (33))
DRHO(I)	249	RHT	$\Delta \rho$	numerical integration step for I^{th} integration interval
DRHOL		RHT		last interval to be used in numerical integration
DRHOIN(K)	9	RHU		numerical integration step size for all DRHO(I), where $\text{RHOIN}(K) < \text{RHO}(I) \leq$ $\text{RHOIN}(K+1)$
DSGMEX(J)	150	THI	$\Delta \sigma^{\text{ex}}(\theta)$	standard deviation in ex- perimental cross section at angle θ (eq. (35))
E		AGN	ϵ	twice the fractional accuracy to which f_2 is to be mini- mized
ECM		MISC	E	incident energy in center- of-mass system
EPS1, EPS2, EPS3		CONV	$\epsilon_1, \epsilon_2, \epsilon_3$	error thresholds in calcula- tions of coulomb functions
EPS4		CONV	ϵ_4	error threshold used in POT1CH subroutine
ELAB		EMCV	E_{LAB}	energy of incident particle in laboratory system
ENORM		CSQ	N_E	normalization constant (eq. (36))
ETA, ETA2		MISC	$\eta, (\eta)^2$	coulomb parameter (eq. (5))
EXSGMR(L), EXSGMI(L)	51	VARL		real and imaginary parts of $\exp(2i\sigma_l)$

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
F(L)	52	VARL	F_l	regular coulomb function
FAC		AGN		factor which controls the form of the initial H-matrix for a search (table III)
FBAR(L)	91	VARL	$F_l^{(n)}$	n th trial value of regular coulomb function used in iterative computation of F
FCR(J), FCI(J)	150	SACS	$f_{C,R}(\theta), f_{C,I}(\theta)$	coulomb scattering amplitude (eq. (23))
FFCI(I), FFCIM(I)	250	PGF	$f_{CI}(\rho), f_{CI}\left(\rho + \frac{\Delta\rho}{2}\right)$	form factors for the imaginary central potential
FFCR(I), FFCRM(I)	250	PGF	$f_{CR}(\rho), f_{CR}\left(\rho + \frac{\Delta\rho}{2}\right)$	form factors for real central potential
FFSI(I), FFSIM(I)	250	PGF	$f_{SI}(\rho), f_{SI}\left(\rho + \frac{\Delta\rho}{2}\right)$	form factors for imaginary spin-orbit potential
FFSR(I), FFSRM(I)	250	PGF	$f_{SR}(\rho), f_{SR}\left(\rho + \frac{\Delta\rho}{2}\right)$	form factors for real spin-orbit potential
FKAY		MISC	k	wave number (eq. (4))
FKAYA		MISC	$k \cdot a_S$	wave number times diffuseness constant
FKAYB		MISC	$k \cdot a_I$	wave number times diffuseness constant
FMB		EMCV	m_b	mass number of target nucleus
FLPT		PGU	l	value of l in eq. (43)
FMI		EMCV	m_i	mass number of incident nucleus
FMU		EMCV	μ	reduced mass of incident particle
FP(L)	51	VARL	F'_l	derivative of regular coulomb function
G(L)	52	VARL	G_l	irregular coulomb function
GP(L)	51	VARL	G'_l	derivative of irregular coulomb function
H(K, M)	(12, 12)	AGN	$H_{k, m}$	element of matrix used as a metric during search procedure

FORTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
ID(K)	12	ASV		internal control used for initializing search param- eter array
IFIRST		RHT		initial value of index I re- ferring to RHO(I)
IIN		ASV		internal counter used to regulate printout of H- matrix
ILAST		RHT		final value of index I re- ferring to RHO(I)
JMAX		THI	J_{\max}	total number of angles ($JMAX \leq 150$)
KDLMAX		ASV		internal control used to initiate calculation of re- stricted χ^2 functions as given in eqs. (38) through (42)
KL(K), [KTRL(K)]	13	CNTR		input controls (table III)
KOUT		CNTR		internal control used to select proper output mode
KSEND		CNTR		KSEND set to KT(1), see description of KT(1) in table III
KSTEP		AGN		number of random changes in variables to test minimum after a search
KT(K), [KTRLT(K)]	13	CNTR		input controls (table III)
KX(K), [KTRLX(K)]	13	CNTR		input controls (table III)
L		RWF	$l + 1$	index of partial waves
LABEL(K)	13	ASV		array containing search parameter labels
LMAX		LIND	$l_{\max} + 1$	index of maximum partial wave
LMAXM		LIND	l_{\max}	maximum number of partial waves
N		AGN	n	number of search parameters
NADL		PCH		internal control which is in- creased by 1 each time l_{\max} is increased in POT1CH

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
NADR		PCH		internal control which is increased by 1 each time ρ_{\max} is increased in POT1CH
NAI, NAO, NAS, NRI, NRO, NRS, NVO, NVS, NVSODD, NWI, NWS, NWVI		GDV		number of increments used for parameters in grid (table IV)
NAME(K)	12	PARA		array of output labels for nuclear potential parameters
NC		AGN		number of constraints on search parameters
NCSN		CSQ		number of values to be divided by CSNRM
NHP		ASV		H-matrix is printed out every NHP iterations during a search
NMAX		RHU		number of RHOIN(I) values to be input
NMLR		ASV		search is cut off after NMLR move left or move right output messages
NP		CSQ		chi-square adjustment factor
NPCT		ASV		search is terminated after NPCT iterations with less than PCT percent change
NPCTP		ASV		not used
NSSW1		AGN		input variable which controls search output (table III)
NTOT		PCH		NTOT = NADL + NADR
NUMRUN		PTI		index identifying cases of a data set
PCT		ASV		search will terminate after NPCT iterations with less than PCT percent change
PMA, PMB		SCNFF	$\frac{\rho_{mA}}{\rho_S}, \frac{\rho_{mB}}{\rho_S}$	parameters for knee and tail variations (eqs. (86) and (87) of ref. 1)

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
POLEX(J)	150	THI	$P^{\text{ex}}(\theta)$	experimental value of polarization for angle θ
POLTH(J)	150	THI	$P^{\text{th}}(\theta)$	calculated value of polarization for angle θ
RC		EMCV		uniform charge radius constant used to compute ρ_{coul}
RHO(I)	250	RHT	ρ	value of ρ at I^{th} integration interval
RHOB		MISC	ρ_{coul}	value of ρ at which uniform charge density ends, $\rho_{\text{coul}} = k \cdot RC (m_b)^{1/3}$
RHOB		MISC	ρ_S	value of ρ corresponding to RS (eq. (7))
RHOBNG		MISC	ρ_I	value of ρ corresponding to RI (eq. (15))
RHOIN(K)	10	RHU		values of ρ for which integration interval changes
RHOMAX		RHT	ρ_{max}	value of ρ for last integration interval
RI, [RG]		PARA	RI	Gaussian radius constant (eq. (15))
RO, [DUMMY(3)]		PARA	RO	radius constant for decoupled potential (eq. (12))
RS, [R0]		PARA	RS	radius constant (eq. (7))
SGMAC(J)	150	SACS	$\sigma_{\text{coul}}(\theta) = f_c(\theta) ^2$	coulomb scattering cross section for angle θ
SGMAEX(J)	150	THI	$\sigma^{\text{ex}}(\theta)$	experimental value of cross section for angle θ
SGMATH(J)	150	THI	$\sigma^{\text{th}}(\theta)$	calculated value of cross section for angle θ
SGMRTH		CSQ	σ_R	calculated value of reaction cross section
SIGMA0, SIGMA1		MISC	σ_0, σ_1	coulomb phase shifts (eq. (24))
SIGTEM(J)	150	SACS		internal temporary storage for weight factors in computing $\chi_{\sigma}^2(\theta)$ (eqs. (35) and (37))

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
SNORM		CSQ	N	normalization constant for experimental cross section (eq. (35))
SRATIO(J)	150	SACS	$\sigma^{\text{th}}(\theta)/\sigma_{\text{coul}}(\theta)$	ratio of scattering cross section to coulomb cross section for angle θ
SUMS(K)	16	CSQ		χ^2 for a restricted range of angles (see next 16 variables)
SUM1S, [SUMS(1)], [CHISQ(4)]		CSQ	$\chi_{\sigma,1}^2$	see eq. (41a)
SUM1P, [SUMS(2)], [CHISQ(5)]		CSQ	$\chi_{\text{P},1}^2$	see eq. (41b)
SUM2S, [SUMS(3)], [CHISQ(6)]		CSQ	$\chi_{\sigma,2}^2$	see eq. (41a)
SUM2P, [SUMS(4)], [CHISQ(7)]		CSQ	$\chi_{\text{P},2}^2$	see eq. (41b)
SUM3S, [SUMS(5)], [CHISQ(8)]		CSQ	$\chi_{\sigma,3}^2$	see eq. (41a)
SUM3P, [SUMS(6)], [CHISQ(9)]		CSQ	$\chi_{\text{P},3}^2$	see eq. (41b)
SUM4S, [SUMS(7)], [CHISQ(10)]		CSQ	$\chi_{\sigma,4}^2$	see eq. (41a)
SUM4P, [SUMS(8)], [CHISQ(11)]		CSQ	$\chi_{\text{P},4}^2$	see eq. (41b)
SUMFS, [SUMS(9)], [CHISQ(12)]		CSQ	$\chi_{\sigma,\text{F}}^2$	see eq. (38a)
SUMFP, [SUMS(10)], [CHISQ(13)]		CSQ	$\chi_{\text{P},\text{F}}^2$	see eq. (38b)
SUMMS, [SUMS(11)], [CHISQ(14)]		CSQ	$\chi_{\sigma,\text{M}}^2$	see eq. (39a)
SUMMP, [SUMS(12)], [CHISQ(15)]		CSQ	$\chi_{\text{P},\text{M}}^2$	see eq. (39b)
SUMRS, [SUMS(13)], [CHISQ(16)]		CSQ	$\chi_{\sigma,\text{R}}^2$	see eq. (40a)
SUMRP, [SUMS(14)], [CHISQ(17)]		CSQ	$\chi_{\text{P},\text{R}}^2$	see eq. (40b)
SUM34S, [SUMS(15)], [CHISQ(18)]		CSQ	$\chi_{\sigma,34}^2$	see eq. (42a)
SUM34P, [SUMS(16)], [CHISQ(19)]		CSQ	$\chi_{\text{P},34}^2$	see eq. (42b)
TEMP		MISC	$k(m_b)^{1/3}$	auxiliary constant used in calculating various ρ values (eq. (7))
TH(K)	2	SCNFF	h_{0A}, h_{0B}	parameters for knee and tail variations (eq. (88) of ref. 1)
THETA(J)	150	THI	θ	center-of-mass scattering angle in radians
THETAD(J)	150	THI	θ	center-of-mass scattering angle in degrees

FORTTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
TITLE(K)	13	PTI		title information (78 characters)
TN1(K)	2	SCNFF	nA_1, nB_2	parameters for knee and tail variations
TN2(K)	2	SCNFF	nA_2, nB_2	(eq. (90) of ref. 1)
TAI, TAO, TAS, TRI, TRO, TRS, TVO, TVS, TVSODD, TWI, TWS, TWVI		GDV		storage for initial parameter values during grid
TRM(K)	2	SCNFF	ρ_{mA}, ρ_{mB}	parameters for knee and tail variations (eqs. (86) and (87) of ref. 1)
UCIB(I), UCIM(I)	250	PGU	$U_{CI}(\rho), U_{CI}\left(\rho + \frac{\Delta\rho}{2}\right)$	l -independent part of imaginary central potential
UCRB(I), UCRM(I)	250	PGU	$U_{CR}(\rho), U_{CR}\left(\rho + \frac{\Delta\rho}{2}\right)$	l -independent part of real central potential
USRB(I), USRM(I)	250	PGU	$U_{SR}(\rho), U_{SR}\left(\rho + \frac{\Delta\rho}{2}\right)$	l -independent part of real spin-orbit potential
USIB(I), USIM(I)	250	PGU	$U_{SI}(\rho), U_{SI}\left(\rho + \frac{\Delta\rho}{2}\right)$	l -independent part of imaginary spin-orbit potential
VO, [V]		PARA	VO	depth of real central potential
VP		AGN		input number to determine size of random step taken at end of search (see card 31--0220.)
VS		PARA	VS	depth of real spin-orbit potential
VSODD, [DUMMY(4)]		PARA	VSODD	real spin-orbit strength for odd l in exchange option
WI, [W]		PARA	WI	depth of imaginary central potential
WS		PARA	WS	depth of imaginary spin-orbit potential
WVI, [DUMMY(1)]		PARA	WVI	depth of imaginary central potential
XNORM		CSQ	N	input value of normalization constant (eq. (35))

FORTRAN symbol	Dimension	COMMON block	Mathematical symbol	Description
XC1, XCP1		RWF	$x_l^+(\rho), \dot{x}_l^+(\rho)$	real parts of radial wave function and first deriv- ative for $l + 1/2$
XD1, XDP1		RWF	$x_l^-(\rho), \dot{x}_l^-(\rho)$	as above for real part, $l - 1/2$
YC1, YCP1		RWF	$y_l^+(\rho), \dot{y}_l^+(\rho)$	as above for imaginary part, $l + 1/2$
YD1, YDP1		RWF	$y_l^-(\rho), \dot{y}_l^-(\rho)$	as above for imaginary part, $l + 1/2$
X1(L), X1P(L)	51	RWFF	$x_l^+(\rho_{\max}), \dot{x}_l^+(\rho_{\max})$	value of XC1 and XCP1 at end of numerical integration
X2(L), X2P(L)	51	RWFF	$x_l^-(\rho_{\max}), \dot{x}_l^-(\rho_{\max})$	value of XD1 and XDP1 at end of numerical integration
Y1(L), Y1P(L)	51	RWFF	$y_l^+(\rho_{\max}), \dot{y}_l^+(\rho_{\max})$	value of YC1 and YCP1 at end of numerical integration
Y2(L), Y2P(L)	51	RWFF	$y_l^-(\rho_{\max}), \dot{y}_l^-(\rho_{\max})$	value of YD1 and YDP1 at end of numerical integration
ZZ		EMCV	ZZ'	product of atomic numbers of target and incident nuclei

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